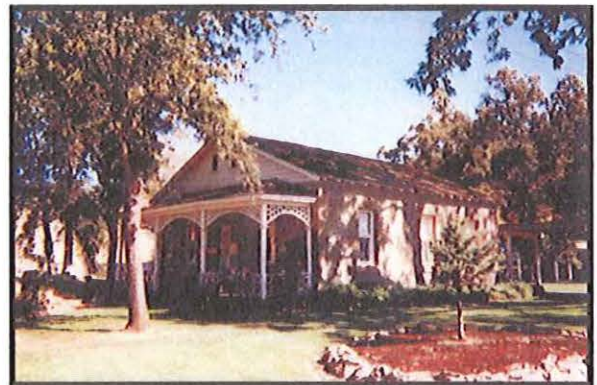


# Master Storm Drainage Plan

## Hidden Valley Lake, California



May 2000

Prepared for:

Hidden Valley Lake CSD  
Hidden Valley Lake HOA  
Lake County Flood Control  
and Water Conservation District



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- APPENDIX C BEST MANAGEMENT PRACTICES
- APPENDIX D HYDROLOGY DESIGN STANDARDS, LAKE COUNTY

# CHAPTER 1 - SUMMARY

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## I. PURPOSE

This Storm Water Master Plan has been prepared to provide a detailed overview of the adequacy of the storm drainage facilities serving the Hidden Valley Lake Subdivision. This Storm Water Master Plan provides the following review of the hydrology and hydraulics of the watershed:

- An assessment of the carrying capacity and existing facilities,
- Preliminary recommendations on upgrades required, and
- The cost of these upgrades.
- Encroachment Standards.
- Storm Water Best Management Practices.

## II. METHODOLOGY

This Storm Water Master Plan began with the development of a watershed tributary to the Hidden Valley Lake Subdivision and the design storm.

The tributary watershed and its sub-watersheds were developed using available 200-scale topographic mapping and U.S. Geological Survey 2000-scale topographic mapping. The total tributary watershed is approximately 10.5 square miles. It can be subdivided into six tributary watersheds with areas varying from .89 to 3.7 square miles.

The design storms were developed using the *Hydrology Design Standards, Lake County*. These standards allow for use of a 10-year storm for watersheds less than one square mile in area and a 25-year storm for watershed more than one square mile in area. The 100-year design storm was also routed through critical drainage systems. Chapter 3 provides a detailed discussion of the development of the design criteria.

Hydrologic modeling was performed using Haested Methods HEC-1<sup>1</sup> and Pond Pack. Hydraulic modeling of major channels was performed using Haested Methods HEC-2. Drainage culverts were evaluated using Manning's equation and design nomographs. Chapter 4 provides a detailed discussion of the hydrologic analysis. Chapter 5 provides a detailed discussion of the hydraulic analysis.

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<sup>1</sup> Haested's Graphical HEC-1, Version 1.0

### **III. IMPROVEMENTS WITHIN THE HIDDEN VALLEY LAKE SUBDIVISION**

The analysis indicates approximately 78 drainage structures within the Hidden Valley Lake Subdivision are undersized for the design flow. The total estimated cost of correcting these deficiencies is \$3,600,520. Chapter 6 provides a prioritization of the recommended improvements.

In addition to the drainage structures (culverts), a storm water pump station, located at the southeast end of the subdivision (Watershed 1), has inadequate capacity to carry the 10-year design storm. The upstream portion of Watershed 1 through the golf course could be used as a detention facility to reduce peak flows to the pump station. However, major upsizing of the station would still be required. A gravity system alternative to the pump station was analyzed that would carry flows downstream entering Putah Creek at a hydraulic grade elevation that would prevent upstream flooding. The costs for these various alternatives range from \$90,000 to \$3.7 million (excluding right-of-way).

### **IV. IMPROVEMENTS OUTSIDE THE HIDDEN VALLEY LAKE SUBDIVISION**

Coyote Creek, a major tributary of Putah Creek, passes through the Subdivision and through Hidden Valley Lake. The creek runs just outside the southern boundary of the Subdivision to its confluence with Putah Creek. Gallagher Creek splits the Subdivision into two parts and joins Coyote Creek just downstream from Mountain Meadow North. An analysis by the Federal Emergency Management Agency (FEMA) indicated that Coyote Creek and Gallagher Creek have the potential to flood portions of the Hidden Valley Lake Subdivision.

This Storm Water Master Plan confirms the FEMA analysis, both Coyote Creek and Gallagher Creek are incapable of carrying the 100-year storm without flooding. Modeling indicates that in order to carry the 100-year flow, Coyote Creek must be widened by approximately 100 feet. This channel widening can be significantly reduced if Hidden Valley Lake can be utilized to provide storm water flood control storage. The channel improvements would be based on the acceptable range of lake level fluctuation during the rainy season. This would reduce the downstream improvements (that are located outside District boundaries) necessary on Coyote Creek.

The hydraulic analysis would benefit from additional surveys of the topography of Coyote Creek and from a more detailed analysis of the operational flexibility of Hidden Valley Lake.

The cost estimates for improvements to Coyote Creek range from \$241,000 to \$713,000 and the cost estimate to improve Gallagher Creek is \$79,000.

## **V. FINANCIAL RECOMMENDATIONS**

Without clear ownership/responsibilities of the stormwater conveyance facilities within Hidden Valley Lake, a stormwater management program cannot be successfully implemented. A number of factors emerge from the review of the material.

- Determine the authority to implement and manage the stormwater facilities for Hidden Valley Lake.
- Grants and funding from FEMA and other government agencies generally require a government entity for administering the funds.
- A defined tax base must be established to dedicate funds for operation/maintenance and implementation of the recommendations.
- A user-fee approach appears to be best suited for Hidden Valley Lake.

## CHAPTER 2 – INTRODUCTION

---

### I. BACKGROUND AND PURPOSE OF STUDY

#### A. BACKGROUND

The Hidden Valley Lake Subdivision (the Subdivision) is located in southern Lake County, approximately 4 miles north of the unincorporated community of Middletown, California, along State Highway 29. The Subdivision is bordered by Putah Creek to the south, Highway 29 to the west, a subdivision of 5-acre ranchettes (known as the Ranchos) to the east, and undeveloped lands to the north. Figure 2-1 illustrates the location of the Subdivision.

The U.S. Land Company originally held title to the Subdivision; the Land Company started development of the Subdivision in 1968. The Land Company sold the property to Boise Cascade Corporation, prior to completing the subdivision improvements. Boise Cascade completed the development in 1973. In its final development certificates, Boise Cascade dedicated responsibility for some subdivision drainage to the County of Lake. Remaining drainage and all roadway responsibilities were dedicated to the Hidden Valley Lake Homeowners Association (Homeowners Association) and responsibility for water and limited sewer service were dedicated to Stonehouse Mutual Water Company (Stonehouse Mutual). Responsibility for a small stormwater pump station, located at the southeast end of the Subdivision, was also dedicated to Stonehouse Mutual.

In 1984, under the provisions of the Cortese-Knox Local Government Reorganization Act, the voters of the Subdivision elected to form a Community Services District. The Hidden Valley Lake Community Services District (the District) is an independent special district with 5 locally elected directors. Community Services Districts, by state law, have very broad latent powers. This type of special district may provide water, sewer, stormwater, recreation, police, fire and transportation services. The original formation documents of the District granted it the authority to provide sanitary sewer service throughout the whole of the subdivision. In 1992, after passage of special legislation and another election by the voters in the Subdivision, the District merged with Stonehouse Mutual. The District now provides all water and sewer service within the Subdivision. The District also has some interest in storm drainage, as it inherited the stormwater pump station originally dedicated to Stonehouse Mutual.



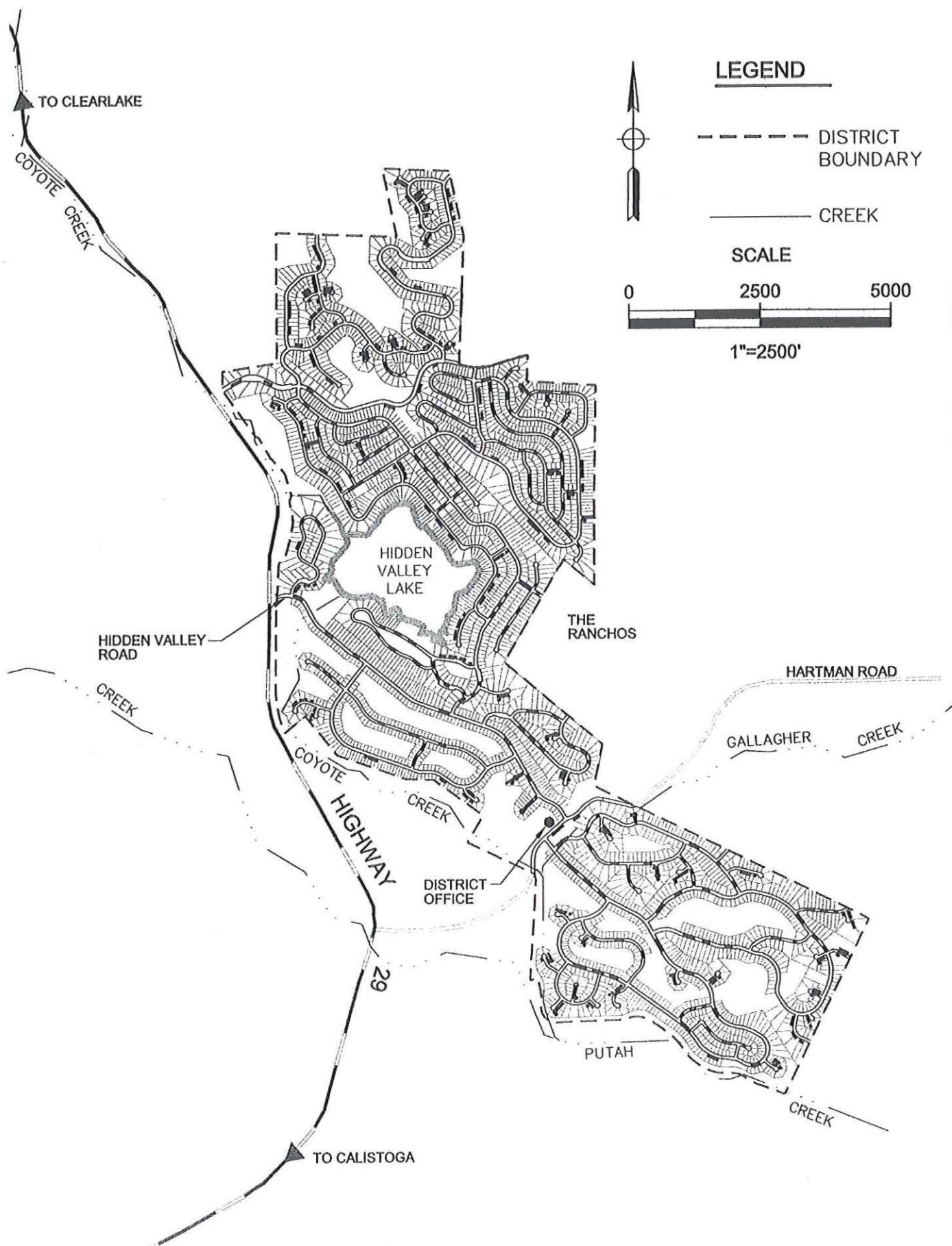


FIGURE 2-1  
LOCATION MAP

Since the merger in 1992, the District has constructed and operates sewer collection facilities, provides water system improvements, repaved roadways and made improvements to the irrigation system on the community Golf Course.

#### **B. PURPOSE**

The only comprehensive review of the drainage system in the Hidden Valley Lake area was conducted in the late 1960s and early 1970s as part of the original subdivision process. Portions of the Subdivision have experienced periodic flooding over the course of the past 25 years, with several severe flooding incidents in the late 1980s and early 1990s. This stormwater master planning effort will identify an orderly approach to correcting existing problems and identify storm run-off flows so future facilities can be integrated into the entire flood control system. The objectives of the Stormwater Master Plan include:

- Identifying the existing flow patterns and quantities of runoff that can be expected to occur.
- Evaluating the capacities of the existing stormwater facilities.
- Developing and evaluating solutions to capacity deficiencies.
- Estimating the costs of implementing the solutions.
- Prioritizing the required improvements

The Lake County Flood Control and Water Conservation District provided the funds for the Stormwater Master Plan and the District administered the funding. The District served as the project manager for this planning effort on behalf of the Lake County Flood Control and Water Conservation District. Winzler & Kelly, Consulting Engineers prepared the Stormwater Master Plan under contract to the District.

#### **C. SCOPE OF WORK**

The Scope of Work for the Stormwater Master Plan is comprised of the following tasks:

- *Data Collection.* This work included obtaining zoning maps, soil surveys and base topographical mapping and digitizing this information; also, reviewing existing data available through the Lake County Flood Control and Water Conservation District, the Division of Safety of Dams, and the Federal Emergency Management Agency's Flood Insurance Rate Mapping; obtaining Rainfall Intensity Curves; and meetings with property owners, District personnel, and Lake County staff.

- **Data Reduction.** This work included the defining of the drainage basins and developing spreadsheets to organize the data for each basin reach; determining base flows for each basin reach; evaluating the capacities of the existing stormwater facilities and identifying undersized stormwater facilities.
- **Technical Recommendations and Cost Estimates.** Comprised of developing potential solutions to identified problems, estimating the costs for the solutions, and recommending a course of action for correcting the problems.
- **Financing Alternatives.** Identify current funding sources and possible alternatives. These alternatives are for long-term funding of the proposal storm water recommendations and recommending a course of action.
- **Report Preparation.** Within this overall scope of work, the Lake County Flood Control and Water Conservation District identified specific areas of interest that needed to be included in the analysis. These specific tasks include:
  - Review the hydrology of Coyote Creek below the Hidden Valley Lake Dam. Below the dam near Fishhook Court, Coyote Creek splits and a portion of the flow goes through two culverts that pass below Highway 29 and outside the boundaries of the Subdivision. The remainder of Coyote Creek flows to a crossing on Hartmann Road that has historically been a flooding problem. The Master Plan should develop solutions that reduce the flooding in the area and allow for modifications to the Flood Insurance Rate Maps.
  - Review the hydrology of Coyote Creek at the confluence of Gallagher Creek. Prepare solutions for increasing the size of the culvert crossing Hartmann Road.
  - Develop driveway encroachment standards.
  - Prepare a set of Best Management Practices (BMP's) for property owners.

A Stormwater Master Plan that satisfies these objectives will provide the framework for developing storm drainage requirements for the Subdivision, and will satisfy Lake County Flood Control Conservation District.

## II. REPORT PREPARERS

This report was prepared under the direction of Mr. Mel Aust, General Manager, Hidden Valley Lake Community Services District.

- Mr. Robert Lossius, Deputy Director of Water Resources, County of Lake
- Mr. Tom Smythe, Water Resources Engineer of Lake County Flood Control and Water Conservation District;
- Mr. Bill Stewart of the Homeowners Association provided review comments.

Winzler & Kelly, Consulting Engineer's project staff included:

- Mr. Iver Skavdal, Principal-in-Charge
- Mr. Jim Winter, Project Manager
- Mr. Rick Jorgensen, Project Engineer
- Mr. Tony Cinquini, Field Review, Modeling and Report Figures

## CHAPTER 3 – STUDY AREA CHARACTERISTICS

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### I. INTRODUCTION

This chapter provides background data on the Study Area for this Stormwater Master Plan. The chapter defines the Study Area boundaries and watershed boundaries that form the basis for the hydrologic analysis; develops the land use and soils information used to calculate run-off coefficients; and outlines the hydrologic patterns that form the basis for the selection of rainfall intensity curves.

### II. STUDY AREA BOUNDARIES

The Study Area is part of the Putah Creek Basin. This large watershed drains from southern Lake County, southeast to Lake Berryessa in Solano County, and ultimately into the Sacramento River. Lake Berryessa is the primary water supply for Solano County. The Putah Creek watershed is included in the ongoing studies conducted under the Cal-Fed Bay-Delta program.

The Subdivision is located in Coyote Valley on the northerly side of Putah Creek and extends from the flat alluvial plain of Coyote Valley into the hillsides. Two main tributaries, Coyote Creek and Gallagher Creek, pass through the Subdivision and eventually combine and discharge into Putah Creek. In order to evaluate the amount of runoff generated or passing through the Subdivision, the Study Area *includes* upstream drainage basin reaches that extend beyond the Subdivision boundaries. The total drainage basin tributary to the Subdivision's stormwater management system is 6,750 acres (10.55 square miles).

The drainage basin can be subdivided into 6 tributary watersheds, 3 of which are located outside of the Subdivision Boundaries. Watersheds 2, 4, 5 and 6 are tributary to Coyote Creek. Coyote Creek is dammed within the Subdivision boundaries to form Hidden Valley Lake. Watersheds 4, 5 and 6 contribute flow to Coyote Creek above the dam. Watershed 2 is located below the dam. Watershed 3 is tributary to Gallagher Creek. Watershed 1 is tributary directly to Putah Creek. Figure 3-1 illustrates the drainage basin and tributary watersheds developed for this Master Plan.

While this Master Plan, identifies and models a drainage basin well outside of the Subdivision boundaries, its recommendations are generally focused on areas within the Subdivision boundaries. Identification of improvements in the upstream watersheds is beyond the scope of this Master Plan.

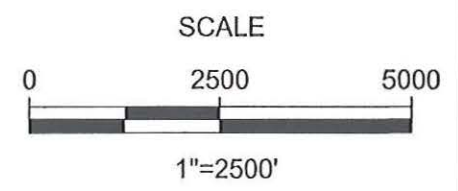
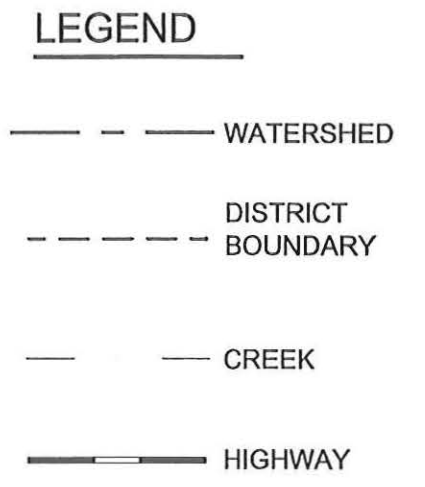
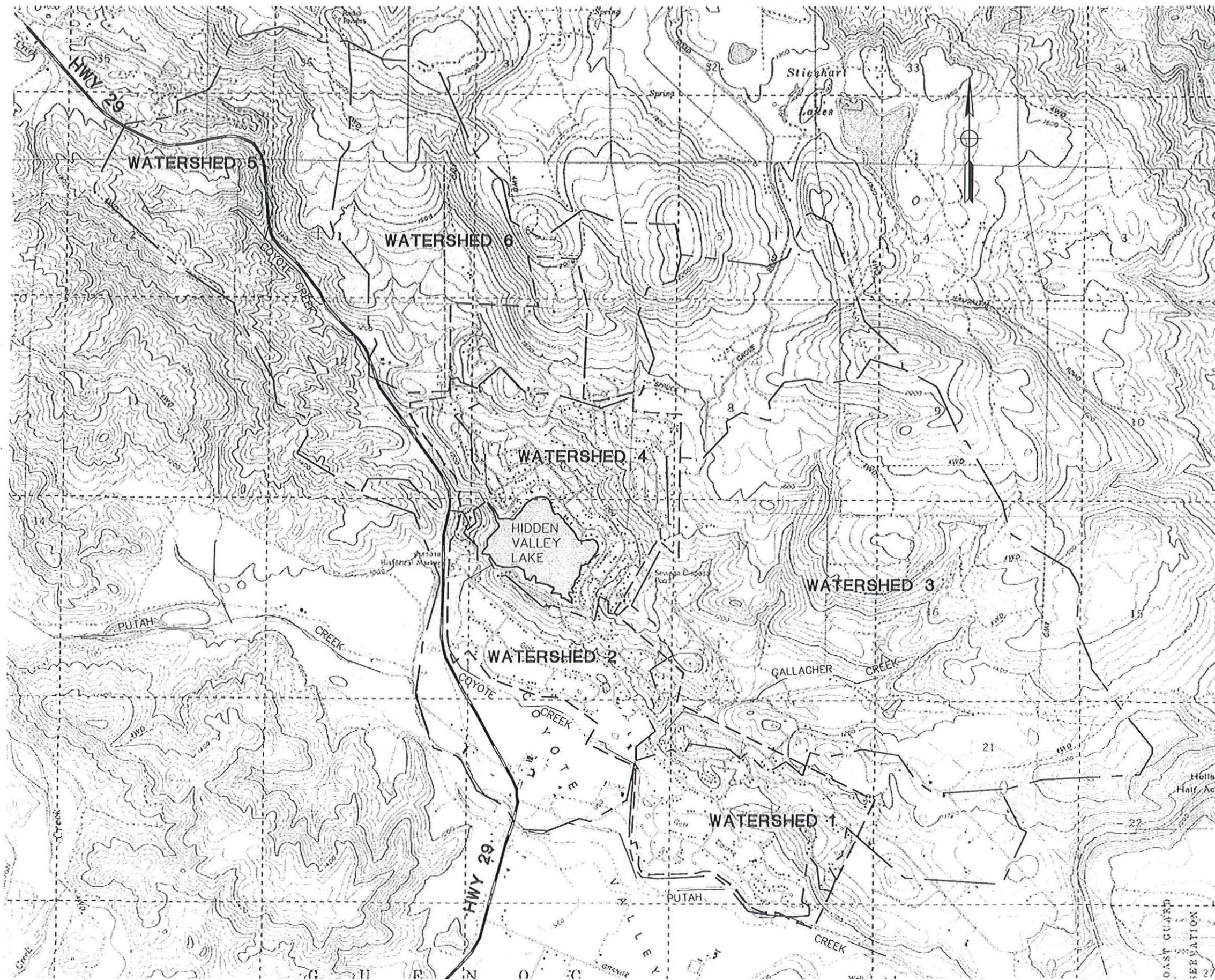


FIGURE 3-1  
WATERSHED BOUNDARY MAP

### **III. GEOGRAPHICAL SETTING**

#### **A. Topography**

The terrain within the drainage basin is quite diverse. Portions of the subdivision lie in the Coyote Valley, which consists of the alluvial plain formed by Putah Creek. However, large portions of the drainage basin are composed of steep hillsides.

Watersheds 1 and 2 are relatively flat; large portions of these watersheds are under 5-percent slopes. The surrounding hills vary from 10 to 30 percent slopes. Watersheds 3 and 4 consist of moderately sloping hillsides at approximately 15 percent slopes. Watersheds 5 and 6 are quite steep, with many slopes in excess of 30 percent.

#### **B. Soils**

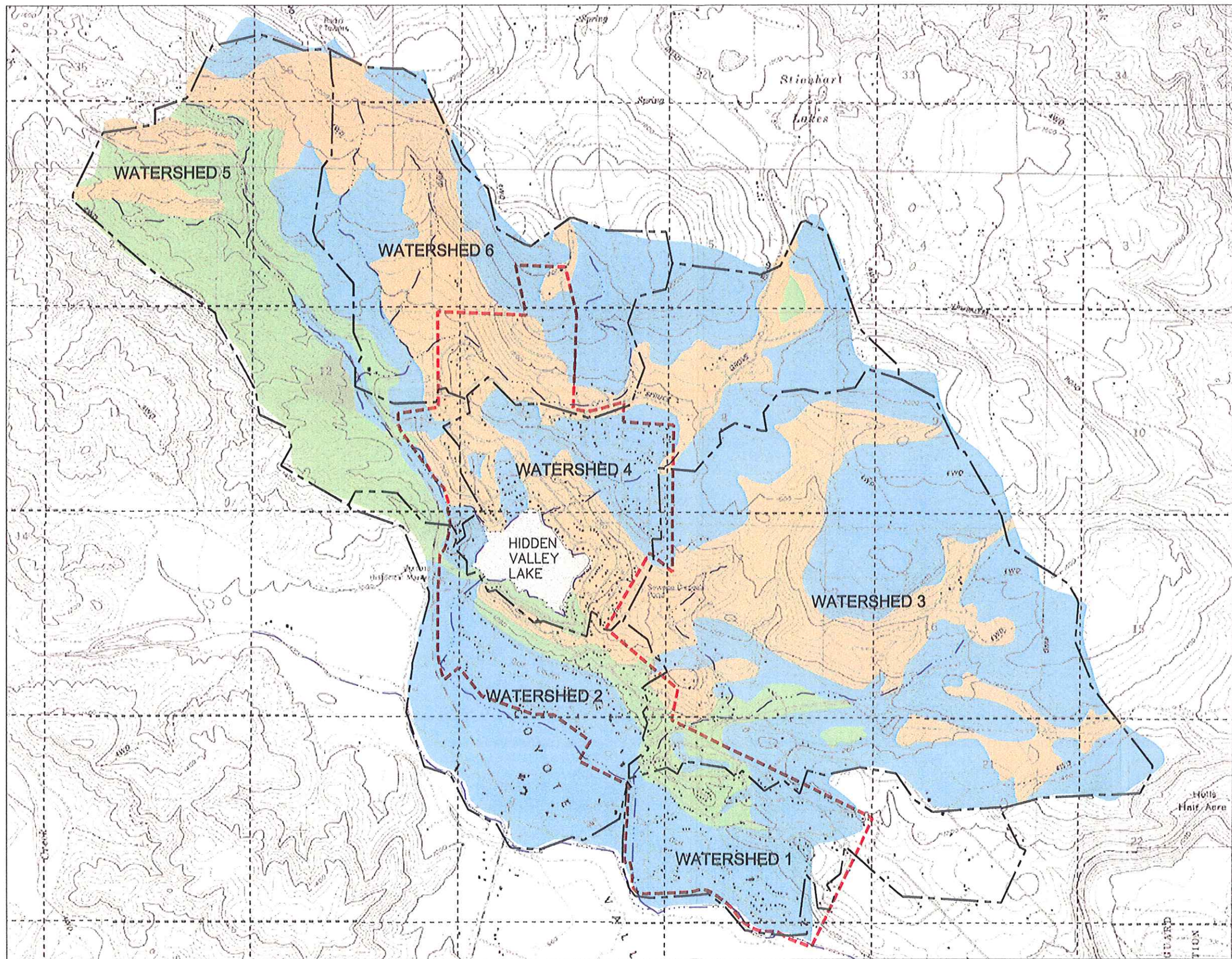
The underlying soil types in the Study Area are used to assist in the development of the runoff coefficient in the hydrologic model. For this project, the Soil Conservation Service (now the Natural Resources Conservation Service or NRCS), Soil Survey for Lake County was used to determine soil type. The Study Area includes three distinct types of hydrologic soils. Soil Type B includes sandy loams and shallow loess (wind-blown volcanic ashes). Soil Type C consists predominantly of soils with a high clay content, including clay loams and some shallow sandy loams. Soil Type D consists of heavy, plastic clays with significant swell potential. The soil types are illustrated in Figure 3-2.

### **IV. CLIMATE**

The climate in Lake County is typically dry in the summers, with mostly seasonal rainfall in the period from October through April. Countywide, rainfall averages from 22 to 80 inches per year. Average seasonal rainfall in Middletown, just south of the Study Area, is 45 inches per year.

### **V. HYDROLOGY**

Stormwater master planning and the design of drainage facilities are highly dependent on the selection of the "design storm." This storm, typically expressed in terms of its expected recurrence interval (e.g., 10 years), is used to determine rainfall intensity. The length of the design storm also affects storm flows and runoffs. This study is based on a 24-hour storm, which simulates the volume of rainfall anticipated to occur in 24 hours.



**LEGEND**

- HYDROLOGIC SOIL GROUP B
- HYDROLOGIC SOIL GROUP C
- HYDROLOGIC SOIL GROUP D
- WATERSHED BOUNDARY
- DISTRICT BOUNDARY

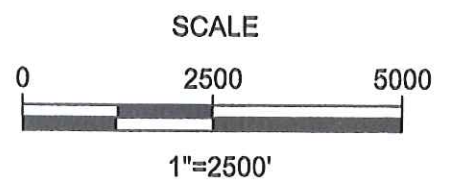


FIGURE 3-2  
SOIL TYPES



The *NOAA Atlas 2 Precipitation-Frequency Atlas of the Western United States, Volume XI – California* was used to determine the 24-hour design rainfall for the project site. The Atlas gives 6- and 24-hour rainfall for 2-, 5-, 10-, 25-, 50- and 100-year events throughout California. Figures 3-3, 3-4 and 3-5 indicate the 10-year, 24-hour; 25-year, 24-hour; and 100-year, 24-hour rainfall events taken from the NOAA Atlas are used in this study.

## **VI. LAND USE**

Land use patterns also affect stormwater master planning efforts because the rate at which stormwater runs off, as opposed to the amount that percolates into the soil, is proportional to the amount of impervious area in a watershed. For long-term planning efforts, it is important to look not only at current development, but also at planned development patterns. Storm drain infrastructure is intended to provide service for 50 to 100 years, and facilities must be designed to accommodate future development in a watershed.

The Lake County zoning map was used to identify land use projections within the study area. By far the most intensive projected development within the Study Area is the Hidden Valley Lake Subdivision. The Subdivision contains approximately 3,300 one-quarter acre residential lots. Approximately one-half of the residential lots are developed at this time. The Subdivision does include areas of open space consisting of an 18-hole Golf Course and Hidden Valley Lake. The “Ranchos,” east of the subdivision includes approximately 200, 5-acre residential parcels. The remainder of the drainage basin is zoned for relatively low levels of development, with an emphasis on agricultural zoning. Figure 3-6 illustrates the land use patterns in the Study Area.

## **VII. EXISTING FACILITIES**

The majority of the Study Area drains through natural channels and roadside ditches. The exception is within the boundaries of the Subdivision, where a storm drainage network has been developed.

The Subdivision is centered around Hidden Valley Lake, a man-made impoundment on Coyote Creek. Drainage is carried through the Subdivision in a network of corrugated metal (CMP) culverts and roadside ditches. Individual driveway crossings of the roadside ditch typically include a CMP or reinforced concrete (RCP) culvert.

At the southeastern edge of the Subdivision, east of Hartman Road, there is a levee along Putah Creek and a portion of Coyote Creek. Drainage from this area (Watershed 1) is piped through the



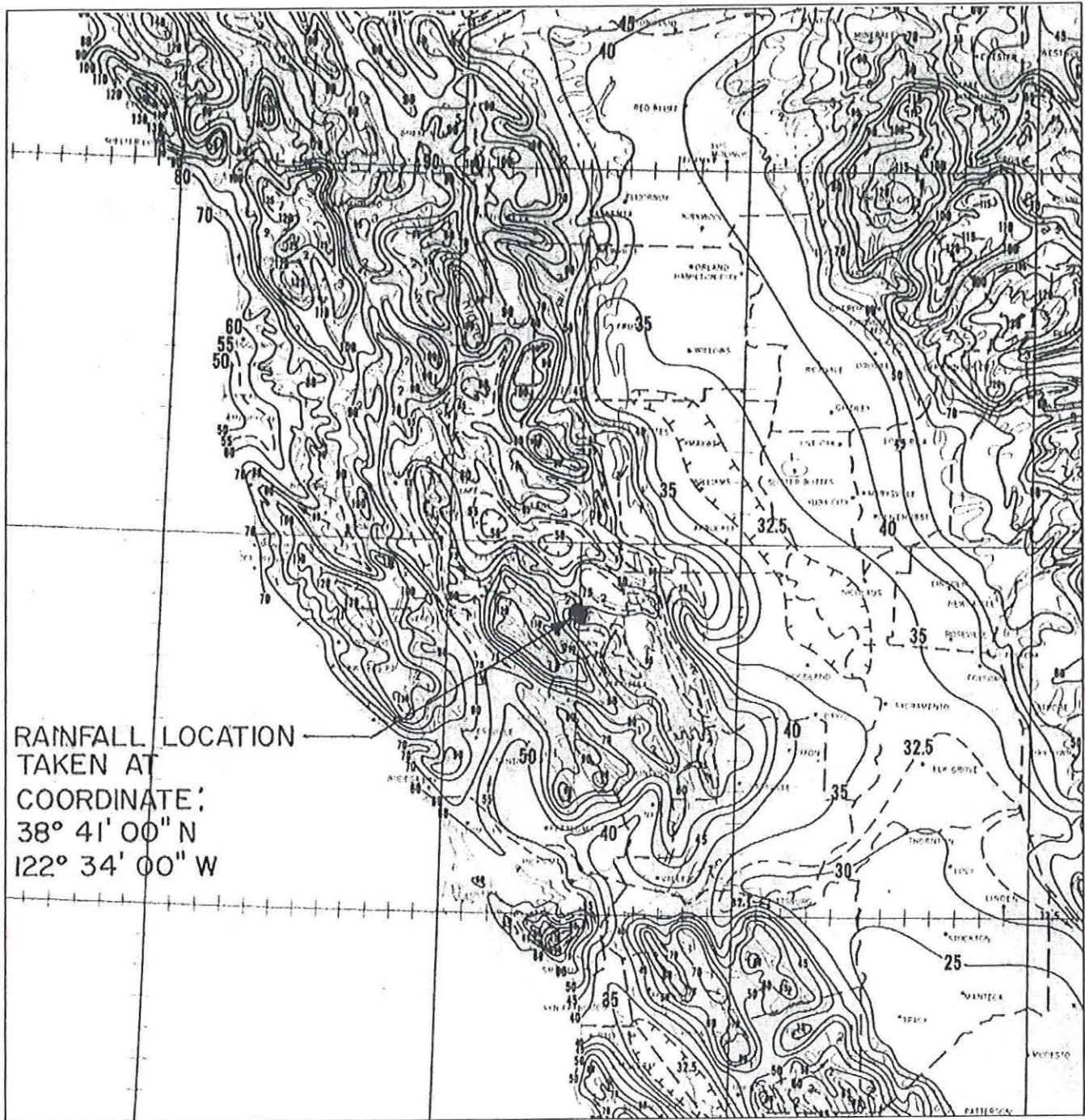


FIGURE 3-4  
25-YEAR, 24 HOUR  
RAINFALL-NOAA ATLAS

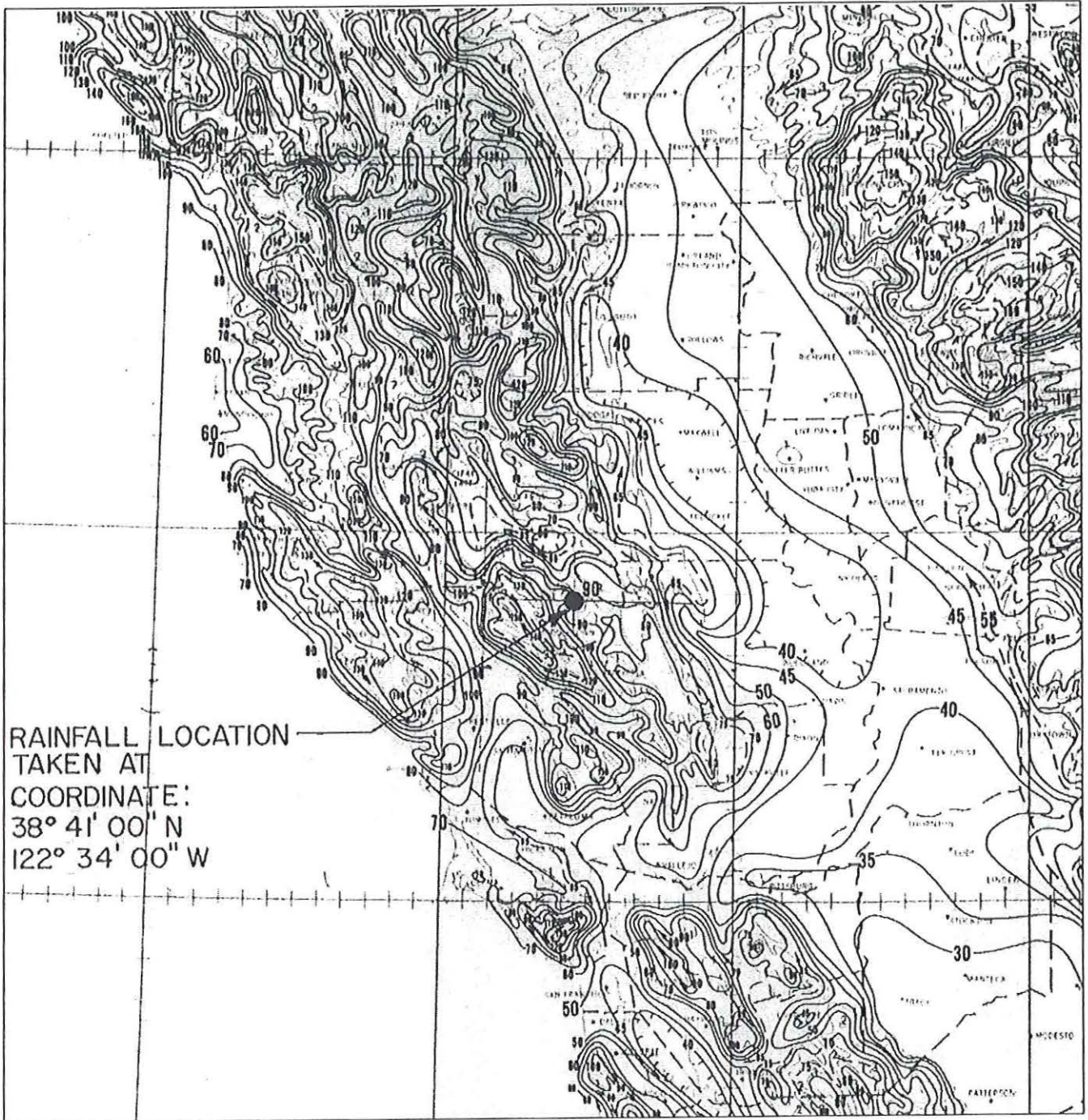
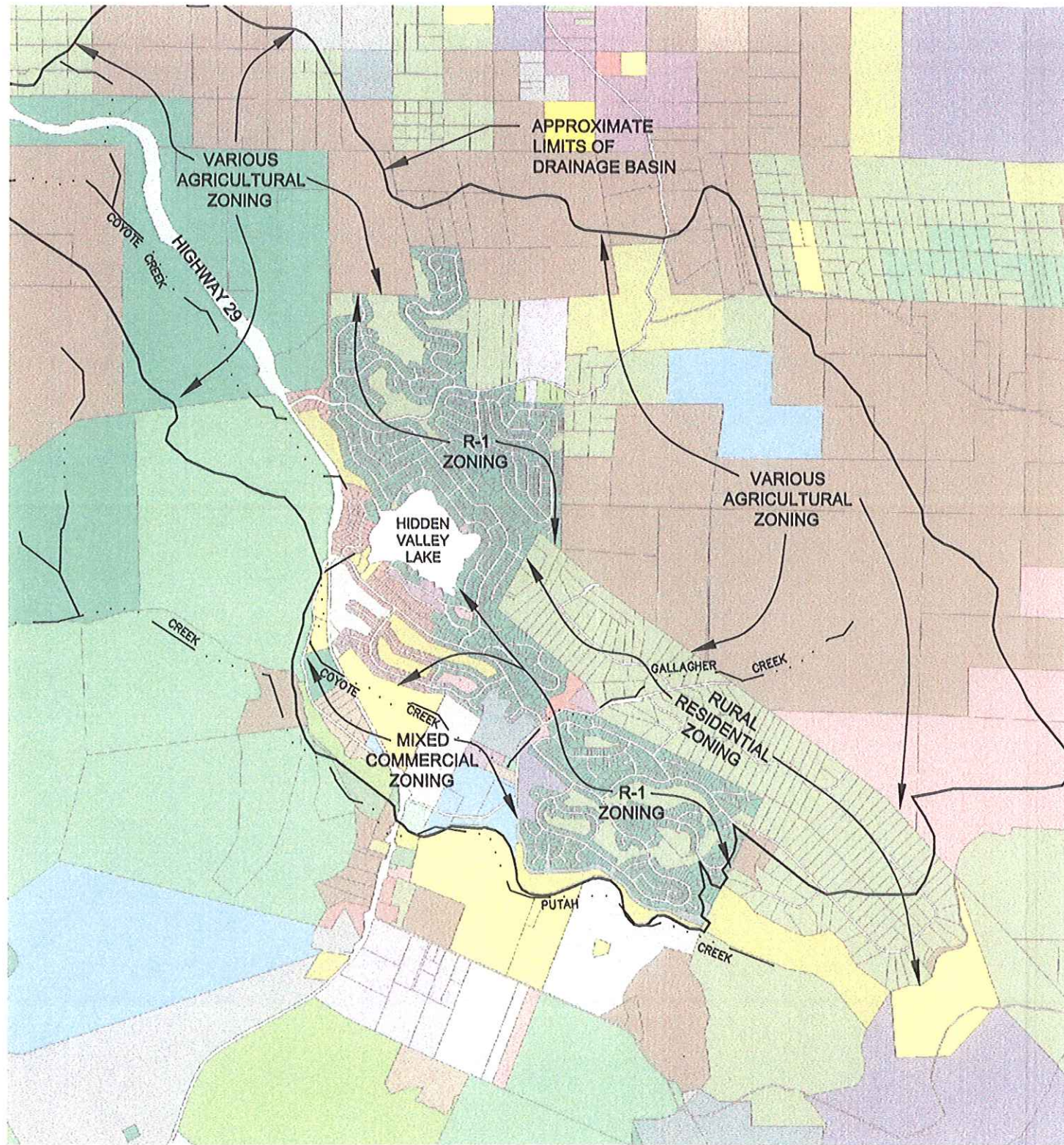


FIGURE 3-5  
100-YEAR, 24 HOUR  
RAINFALL-NOAA ATLAS



**LEGEND:**

- |                             |                                |                              |
|-----------------------------|--------------------------------|------------------------------|
| A                           | C1-DR-FF-WW;C2-DR-FF-P;CH-DR-F | R2-RD                        |
| A: RL                       | C1-DR-WW-FF : CH-DR-WW-FF      | R3                           |
| A: RL: RR                   | C2-DR                          | R3-FF                        |
| A: RL-SC                    | C2-DR-FF                       | RL                           |
| A: RL-WW-FF                 | C2-DR-FF-P                     | RL: RR                       |
| A: RR                       | C2-DR-P                        | RL: RR: RR-BF: RR-B5 (2.5ac) |
| A: RR-W                     | C3-DR                          | RL: RR: SR-B3 (3ac)          |
| A-FF: RL-FF                 | C3-DR: CR-DR-FF: O-FF          | RL: RR-FF                    |
| A-FF: RR-FF                 | C3-DR-FF                       | RL-FF                        |
| A-FF-SC                     | C3-DR-FF: CH-DR-FF             | RL-FF-SC                     |
| A-FF-SC: R1-FF-SC: SR-FF-SC | CH-DR                          | RL-FF-SC: C3-DR-FF           |
| A-FF-SC: RR-FF-SC           | CR-DR                          | RL-SC                        |
| A-SC                        | CR-DR-FF                       | RL-SC: M2                    |
| A-SC: RL                    | CR-DR-FF: O-FF                 | RL-SC: RR-FF-SC              |
| A-SC: RL-SC-FF: RR-SC       | O                              | RL-SC: RR-SC-FF              |
| A-SC: RL-WW-FF              | O-FF                           | RL-SC-FF                     |
| A-SC: RL-WW-FF: M1          | O-SC                           | RL-SC-FF: PDC-DR-FF: M2-FF   |
| A-SC-FF                     | O-SC-FF                        | RL-W                         |
| A-SC-FF: RL-SC              | PDC-DR-FF                      | RL-WW                        |
| A-SC-FF: RL-SC: RR-SC       | PDC-DR-FF: CH-DR-FF            | RL-WW: RR                    |
| A-SC-FF: RL-SC-FF           | PDR                            | RR                           |
| A-SC-FF: RL-SC-FF: RR-SC    | R1                             | RR: C2-DR                    |
| A-SC-FF: RR-FF              | R1: C2-DR-P                    | RR-FF                        |
| A-SC-FF: RR-SC              | R1: O                          | RR-FF: R1-FF                 |
| A-SC-FF-WW                  | R1-FF                          | RR-FF-SC                     |
| A-SC-WW-FF: RL              | R1-FF-SC: SR-FF-SC             | RR-FF-SC: CR-DR-FF           |
| A-SC-WW-FF: RL-WW-FF        | R1-RD                          | RR-FF-SC: R1-RD-FF-SC        |
| A-SC-WW-FF: RL              | R1-RD: O                       | RR-SC                        |
| A-W                         | R1-RD-FF                       | RR-SC-FF                     |
| A-W: RR                     | R1-RD-FF: C2-DR-FF             | RR-W                         |
| APZ                         | R1-RD-FF: O-FF                 | RR-WW                        |
| APZ-FF                      | R1-RD-SC                       | SR-B3 (3ac)                  |
| APZ-FF-SC                   | R1-RD-SC-FF                    | SR-B5-FF-SC                  |
| APZ-SC                      | R1-WW-FF                       | SR-FF                        |
| APZ-WW                      | R2                             | SR-FF: PDR                   |
| C1-DR-FF                    | R2-FF                          | SR-FF-SC                     |
|                             |                                | SR-SC-FF                     |

FIGURE 3-6  
LANDUSE MAP

levee in a 72-inch diameter culvert. A flap gate closes during high flows in Putah Creek. When the flap gate is closed, water held behind the levee is pumped into Putah Creek via a stormwater pump station.

### VIII. SUMMARY

The following Table 3-1 summarizes the primary characteristics of each of the tributary watersheds considered in this Master Plan.

<b>Watershed</b>	<b>Area (sq. mi.)</b>	<b>Slope</b>	<b>Soil Types</b>	<b>Land Use</b>	<b>Tributary</b>
Watershed 1	0.895	5% to 30%	B and D	Residential	Putah Creek
Watershed 2	1.297	5% to 30%	B and D	Residential	Coyote Creek
Watershed 3	3.675	<u>15%</u>	B and C	Rural Residential/Agricultural	Gallagher Creek
Watershed 4	1.117	<u>15%</u>	B and C	Residential/Agricultural	Coyote Creek
Watershed 5	1.940	>30%	B, C – D along Hwy 29	Agricultural	Coyote Creek
Watershed 6	1.624	>30%	Predominantly D	Agricultural Preserve - Scenic Resource	Coyote Creek

## CHAPTER 4 - STUDY METHODOLOGY

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### I. DESIGN CRITERIA

The Lake County Flood Control and Water Conservation District has developed a set of design standards incorporated in a document entitled: *Hydrology Design Standards, Lake County (The Lake County Standards)*. The *Lake County Standards* prescribe design storms for various types of waterways. The *Lake County Standards* defines a minor waterway as one with a watershed area of one square mile or less. Major waterways drain watersheds in excess of one square mile. Prescribed design storms are:

- The 10-year, 24-hour event for minor waterways
- The 25-year, 24-hour event for major waterways

This Master Plan calculates the two design flow events specified in the *Lake County Standards* and also develops the 100-year, 24-hour event. The 100-year, 24-hour event is used by FEMA in preparing Flood Insurance Rate Maps and provides an important point of comparison between this work and the work previously developed by FEMA.

Table 3-1 presented previously, summarizes the watershed areas under consideration. Most drainage features will be required to meet the minor waterway standard. Only drainage structures in the lower reaches of the watersheds will need to be designed for 25 or 100-year events.

*The Lake County Standards* allow the use of the Rational Method for minor waterways. This rather simple equation ( $Q=CIA$ ) presents the relationship between rainfall runoff ( $Q$ ), rainfall intensity ( $I$ ) watershed area ( $A$ ) and development intensity ( $C$ ). The relationship is reasonably accurate when the watershed area is less than one square mile, but can produce unreliable results for larger watersheds.

In this Master Plan, as the drainage flows are routed downstream, the overall watershed size exceeds one square mile. This Master Plan will use the Soil Conservation Service (SCS) Unit Hydrograph available in HEC-1 for all run-off analysis. This use of a single, consistent modeling device will result in coordinated improvements throughout the Subdivision.

## **II. MAPPING**

Watershed areas provide the basis for all hydrologic calculations. In order to arrive at appropriate watershed areas for this Master Plan, topographic mapping of the Subdivision developed in 1982 was digitized using AutoCAD. This mapping is at a scale of 1 inch equals 200 feet with 5-foot contours. For areas outside of the Subdivision, watershed areas were calculated using the U.S.G.S 15-Minute Quadrangle for Middletown, California. This mapping is at a scale of 1 inch equals 2000 feet with 20-foot contour intervals.

## **III. DATA REVIEW AND FIELD INVESTIGATIONS**

### **A. DATA REVIEW**

The Lake County Flood Control and Water Conservation District, the Homeowners Association and the District all keep files on drainage issues in the Subdivision. These files were reviewed to gather relevant data for this Master Plan. Existing drainage facilities and their contributory watersheds were identified from the available topographic mapping.

### **B. FIELD REVIEW**

Once the file and map review was complete, the identified drainage facilities and their contributory watersheds were field verified. The mapping presented in Chapter 5 of this Master Plan reflects the results of the field review effort.

Each drainage facility located in the field was photographed. The size and material of each drainage facility was recorded on a field investigation form. The detailed information was compiled to be used in developing Mannings "n" values for subsequent modeling effort.

## **IV. HYDROLOGY MODEL**

Each of the six individual watersheds was modeled using the Soil Conservation Service (SCS) Unit Hydrograph, available in HEC- 1. In addition to watershed area (A) and rainfall intensity (I), this model uses a Run-off Curve Number (CN) and Run-off Lag (L) to define the runoff hydrograph.

### **A. RUNOFF CURVE NUMBER**

The Runoff Curve Number (CN) is a relationship between runoff and soil type and land use. The higher the CN-value, the greater the runoff. CN-value increases with density of development and



with the relative impermeability of the underlying soils. The relatively dense residential development found in the Subdivision increases the CN value in Watershed 1, 2 and 4. Watersheds with a higher percentage of Type C and D soils will have a higher CN-value than those with predominantly Type B Soils.

#### **B. RUNOFF LAG**

The Runoff Lag (L) is defined as the time in hours from the center of mass of rainfall excess to the peak discharge. It has a relationship to the time of concentration of:

$$t_c = 1.67L.$$

The lag for the various watersheds was determined by estimating the time of concentration or travel time for runoff, and then using the above relationship to calculate the lag. A minimum lag of 6 minutes ( $t_c$  of 10 minutes) was assumed if the calculations for  $t_c$  for the various sub-watersheds indicated a shorter time of concentration.

#### **C. RAINFALL EVENT**

In addition, to Runoff Curve Number and Runoff Lag, the design rainfall and a rainfall distribution must be defined. *The Lake County Design Criteria* prescribes 24-hour design events (rainfall intensity and volume is predicted over a 24-hour period), with the design frequency which varies by size of watershed. For this Master Plan, 10-year, 25-year and 100-year frequencies are modeled.

Rainfall events can be developed by statistical review of rainfall records in the area under study or "synthetic" storms may be used. This Master Plan utilizes a synthetic storm developed by the Soil Conservation Service (SCS). The SCS synthetic storms were developed using the United States Weather Bureau's Rainfall Frequency Atlases. The SCS defined four different rainfall distributions, depending on the region of the country. These rainfall distributions are included in the HEC-1 modeling package. A Type IA distribution is assumed for the project site.

## V. HYDRAULIC MODELS

The Hydrology Model predicts the volume of flow generated at any point in a watershed from the defined rainfall event. This volume of flow can then be used to size the hydraulic structures (open channels or closed conduits) that carry the flow through a given area. Hydraulic sizing is based on several parameters including flow (Q), cross sectional area of the drainage structure (A), slope of the ground through the structure (S), and roughness of the ground (in this case, modeled by the roughness coefficient Manning's "n").

When designing single isolated drainage structures, hand calculations of the hydraulic capacity are often performed. However, when networks of interconnected structures are developed, as is the case with certain watersheds identified in this Master Plan, computer models are utilized to simulate hydraulic performance throughout the system.

The Lake County Flood Control and Water Conservation District provided a HEC-2 model for portions of the watershed that had been developed by FEMA. The cross sectional areas, ground slopes and roughness' developed by FEMA, were used as the basis of this Master Plan.

The design flows used in this Master Plan were developed using the Hydrologic Modeling Tool, HEC-1 (described above). Cross sectional areas and roughness coefficients were modified based on field review data, where it was available.

Open channels were modeled using HEC-2<sup>1</sup>, FLOWMASTER I<sup>2</sup> or FLOWMASTER<sup>3</sup> and closed conduits, such as storm drains and culverts were modeled using StormCAD and Inlet Control Nomographs.

All drainage nodes were numbered based on the watershed tributary to them. For example; Drainage Node 1.0-1 is in Watershed 1 and Drainage Node 4.0-2 is in Watershed 4.

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<sup>1</sup> HEC-2, Version 4.6.2.

<sup>2</sup> FLOWMASTER I, Version 3.21, Haested's.

<sup>3</sup> StormCAD, Version 1.0, Haested's.

## CHAPTER 5 - HYDRAULIC CAPACITY ANALYSIS

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### I. INTRODUCTION

As described earlier, the drainage area through the Subdivision includes the Coyote Creek watershed, the Gallagher Creek watershed and that portion of the Subdivision that drains directly to Putah Creek by way of a stormwater pump station. The hydraulic capacity analysis has been divided to review the drainage facilities within the Subdivision proper, which are typically closed conduits, and the larger open channels carrying Coyote Creek. Gallagher Creek has been modeled to provide information on the hydraulic capacity at its confluence with Coyote Creek.

### II. HIDDEN VALLEY LAKE SUBDIVISION

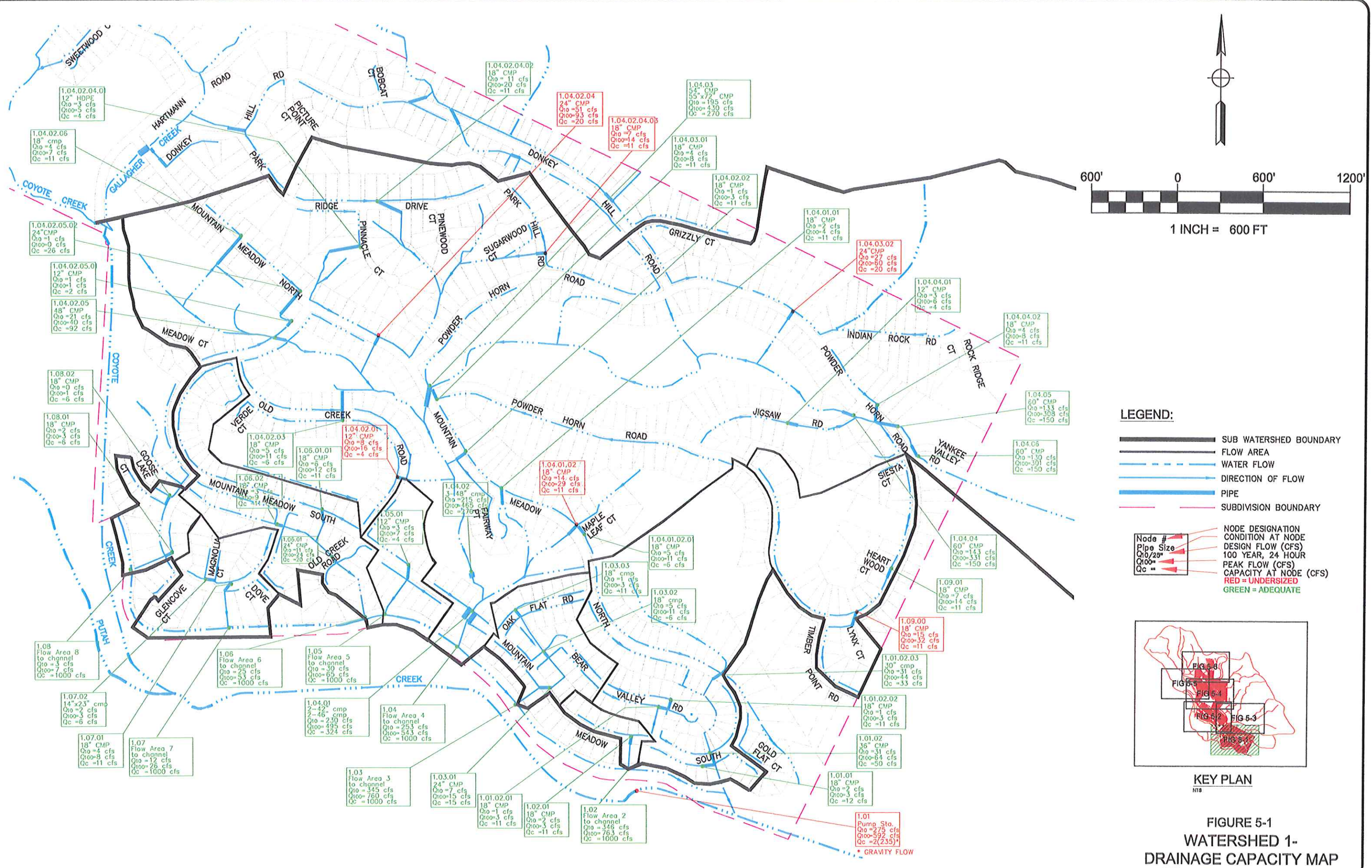
#### A. DESCRIPTION

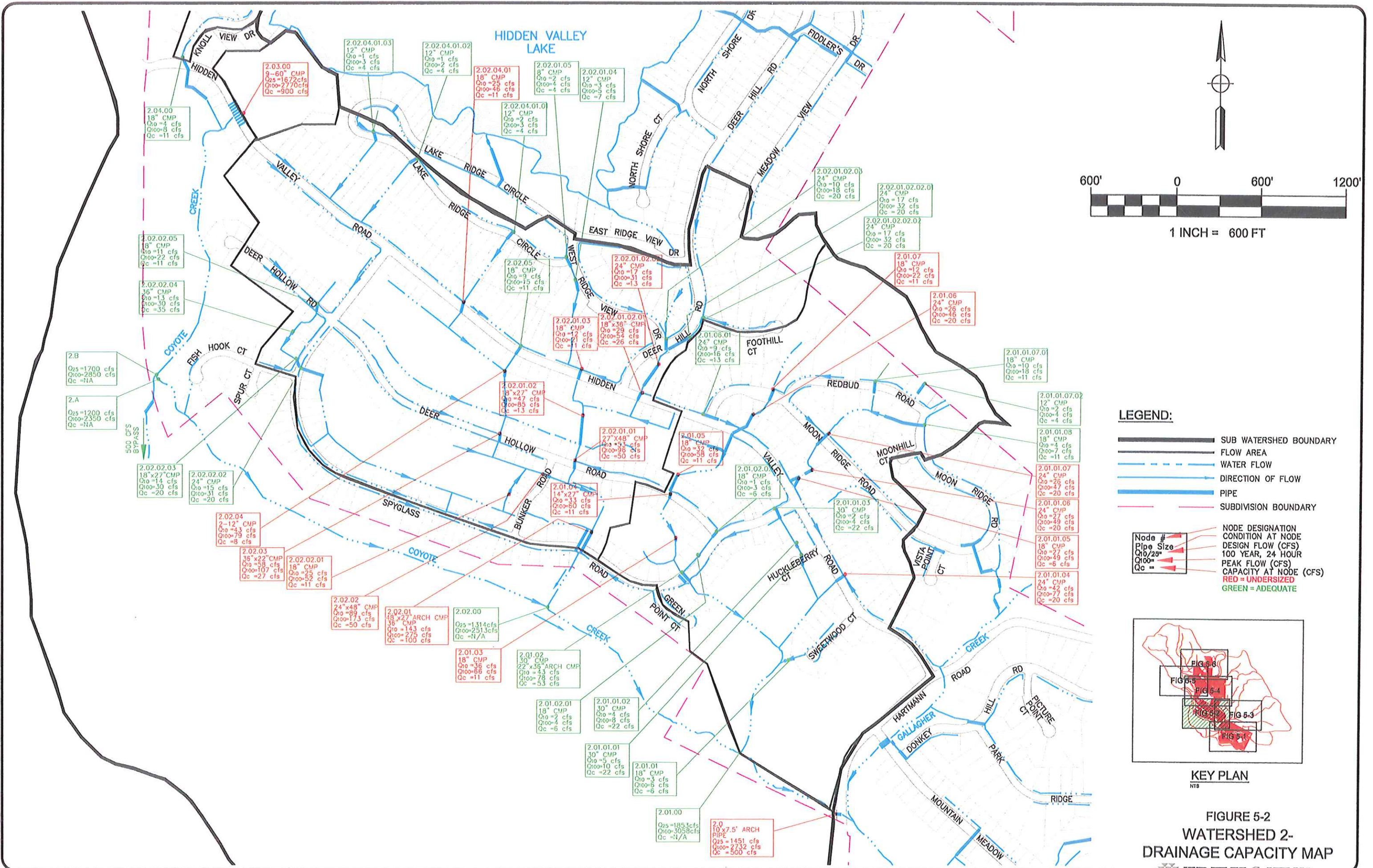
In order to analyze the capacity of drainage facilities within the Subdivision, the larger watersheds were divided into sub-watersheds at key nodes that corresponded to identify drainage structures. The design storm flow ( $Q$ ), at each node, was estimated using HEC-1. The capacity of the existing feature was then compared to the design storm flow.

For the most part, the sub-watersheds are less than one square mile in area (a "Minor Watershed") and the design flow was estimated using a 24-hour, 10-year event ( $Q_{10}$ ). Where the sub-watersheds exceeded one square mile, the design storm was increased to a 24-hour, 25-year event ( $Q_{25}$ ). The 100-year flow ( $Q_{100}$ ) was also estimated throughout the sub-watersheds. The  $Q_{100}$  provides an important capacity check at key nodes, most particularly where drainage structures cross major roadways.

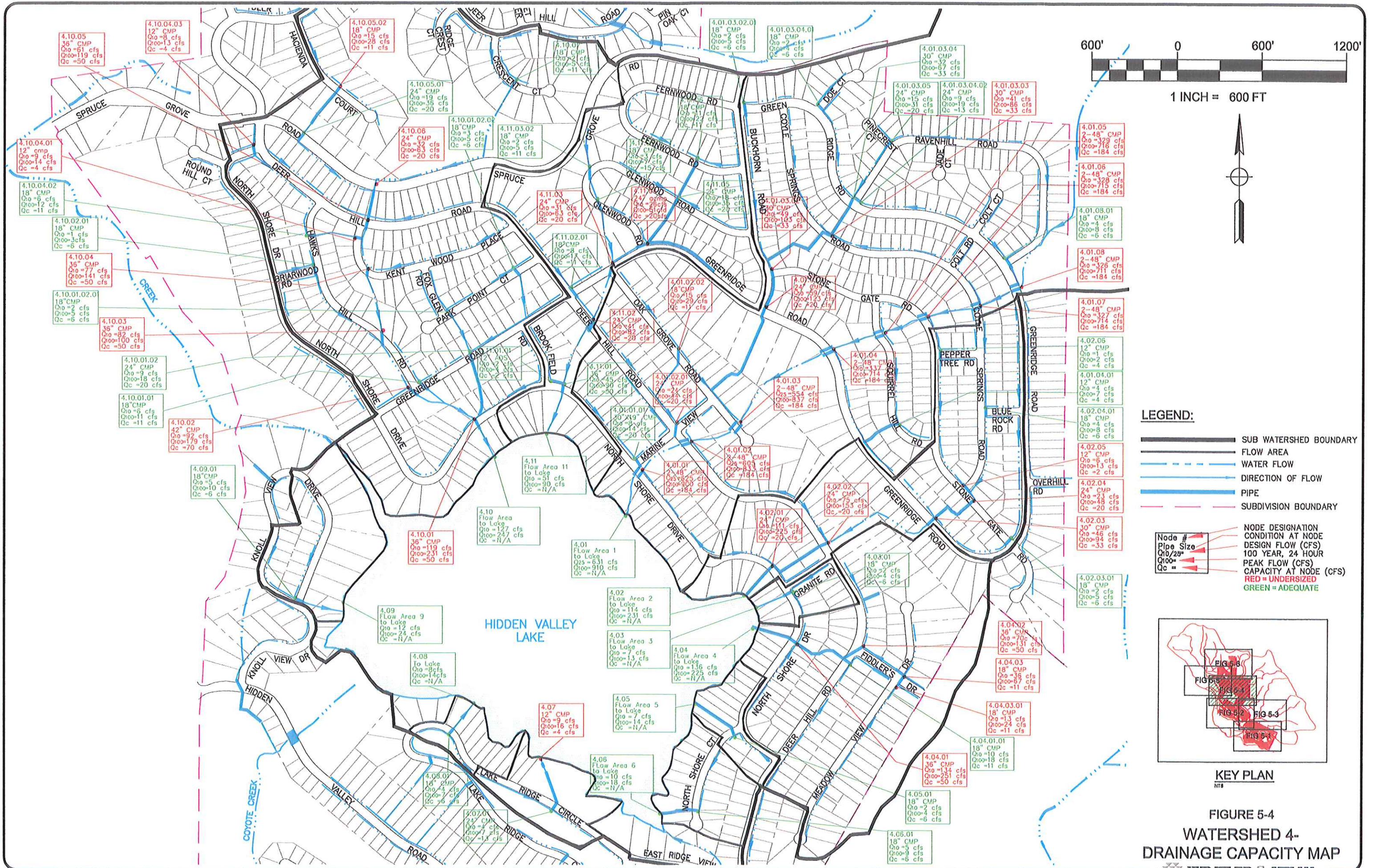
#### B. CAPACITY OF EXISTING DRAINAGE FACILITIES

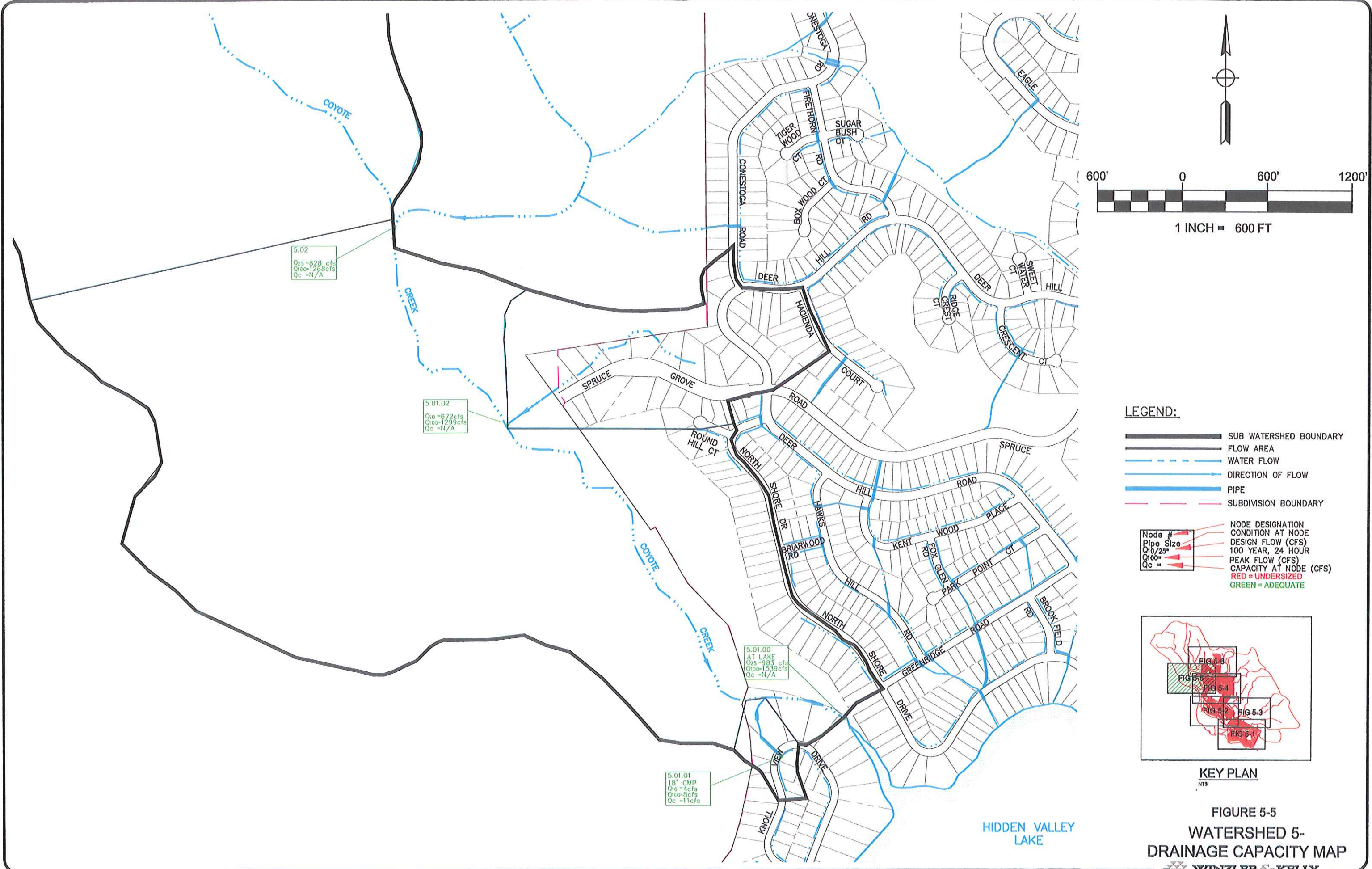
In addition to modeling runoff flow, the capacities of the drainage facilities at the key nodes were estimated. This allows for each drainage facility to be checked for adequate sizing. The capacities along with the design flows are presented in Table 5-1, following. Figures 5-1, 5-2, 5-3, 5-4, 5-5 and 5-6 graphically illustrate the results of modeling.









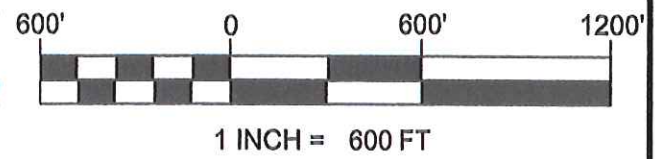


5.02  
 Q25 = 828 cfs  
 Q100 = 1268 cfs  
 Qc = N/A

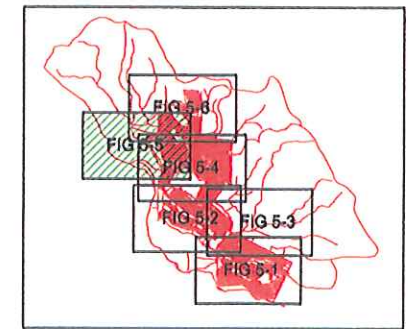
5.01.02  
 Q10 = 672 cfs  
 Q100 = 1299 cfs  
 Qc = N/A

5.01.00  
 AT LAKE  
 Q25 = 983 cfs  
 Q100 = 1539 cfs  
 Qc = N/A

5.01.01  
 18" CMP  
 Q10 = 4 cfs  
 Q100 = 8 cfs  
 Qc = 11 cfs



- LEGEND:**
- SUB WATERSHED BOUNDARY
  - FLOW AREA
  - WATER FLOW
  - DIRECTION OF FLOW
  - PIPE
  - SUBDIVISION BOUNDARY
- |  |   |
|--|---|
| <p>Node #</p> <p>Pipe Size</p> <p>Q10/25'</p> <p>Q100'</p> <p>Qc =</p> | <p>→ NODE DESIGNATION</p> <p>→ CONDITION AT NODE</p> <p>→ DESIGN FLOW (CFS)</p> <p>→ 100 YEAR, 24 HOUR</p> <p>→ PEAK FLOW (CFS)</p> <p>→ CAPACITY AT NODE (CFS)</p> <p>→ RED = UNDERSIZED</p> <p>→ GREEN = ADEQUATE</p> |
|--|---|



**KEY PLAN**  
 HTS

**FIGURE 5-5**  
**WATERSHED 5-**  
**DRAINAGE CAPACITY MAP**



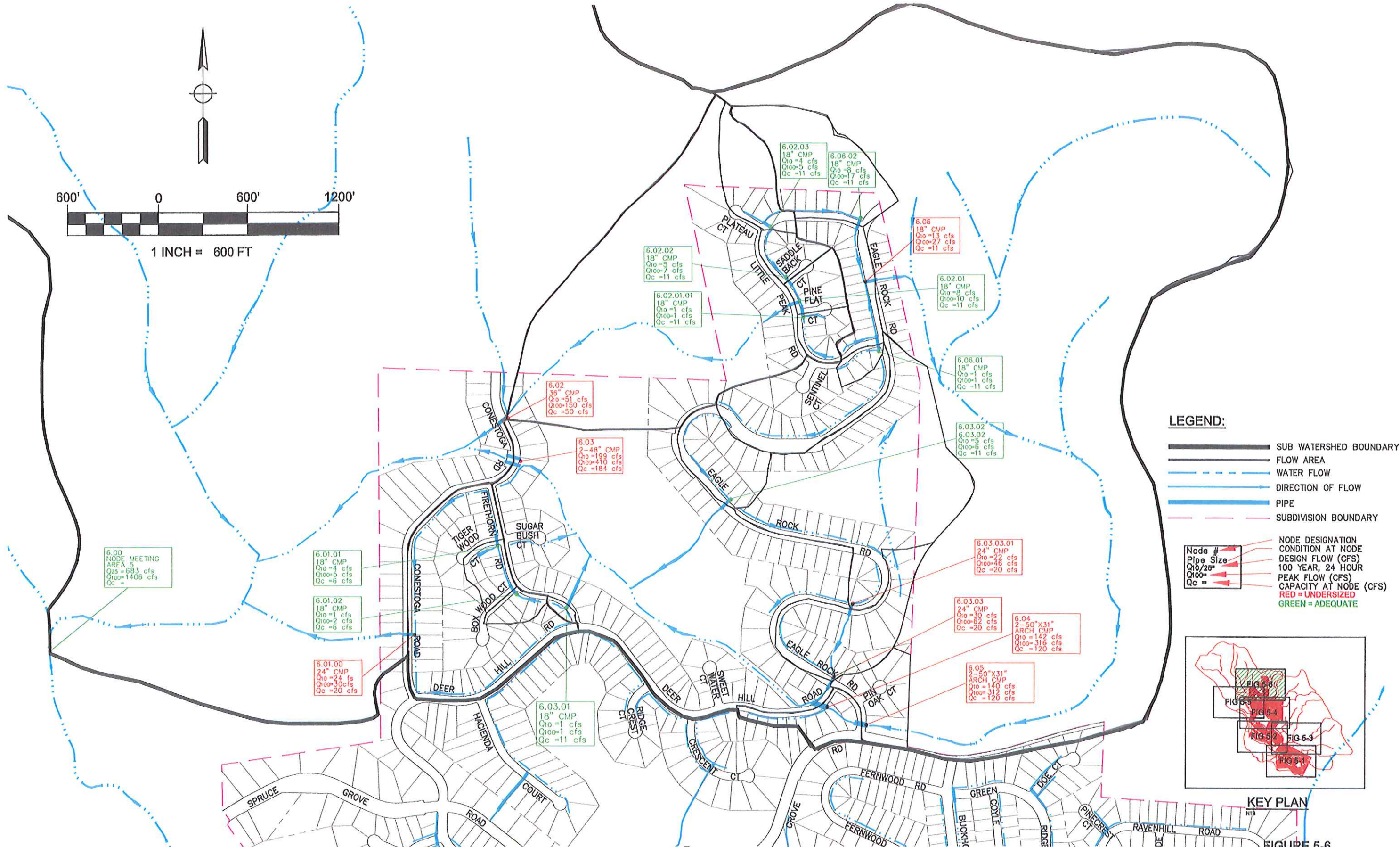


FIGURE 5-6  
WATERSHED 6-  
DRAINAGE CAPACITY MAP

Note:  
***Bold Italicized*** = Undersized

TABLE 5-1  
 CAPACITY ANALYSIS EXISTING DRAINAGE FACILITIES

Pipe Number	Existing Storm Drainage System	Existing Capacity (cfs)	Estimated Flows (cfs)		
			10-Year	25-Year	100-Year
<b>1.01.00</b>	<b><i>Pump Station</i></b>	<b><i>13 to 18</i></b>	<b><i>275</i></b>		<b><i>592</i></b>
1.01.01	18" CMP	12	2		3
1.01.02	36" CMP	50	31		64
1.01.02.01	18" CMP	11	1		3
1.01.02.02	18" CMP	11	1		3
1.01.02.03	30" CMP	33	31		44
1.02.00	Channel	1000	346		763
1.02.01	18" CMP	11	2		3
1.03.00	Channel	1000	345		760
1.03.01	24" CMP	15	7		15
1.03.02	18" CMP	6	5		11
1.03.03	18" CMP	11	1		3
1.04.00	CHANNEL	1000	253		543
1.04.01	2-48" CMP, 2-42" CMP	324	230		495
1.04.01.01	18" CMP	11	2		4
<b>1.04.01.02</b>	<b><i>18" CMP</i></b>	<b><i>11</i></b>	<b><i>14</i></b>		<b><i>29</i></b>
1.04.01.02.01	18" CMP	6	5		11
<b>1.04.02</b>	<b><i>3-48" CMP</i></b>	<b><i>276</i></b>	<b><i>215</i></b>		<b><i>465</i></b>
<b>1.04.02.01</b>	<b><i>12" CMP</i></b>	<b><i>4</i></b>	<b><i>8</i></b>		<b><i>16</i></b>
1.04.02.02	18" CMP	11	1		3
1.04.02.03	18" CMP	6	5		11
<b>1.04.02.04</b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>51</i></b>		<b><i>93</i></b>
1.04.02.04.01	12" HDPE	4	3		5
1.04.02.04.02	18" CMP	11	11		20
1.04.02.04.03	18" CMP	11	7		14
1.04.02.05	48" CMP	92	21		40
1.04.02.05.01	12" CMP	2	1		1
1.04.02.05.02	24" CMP	20	1		0
1.04.02.06	18" CMP	11	4		7
1.04.03	54" CMP, 72"x55"	270	195		430
1.04.03.01	18" CMP	11	4		8
<b>1.04.03.02</b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>27</i></b>		<b><i>60</i></b>
1.04.04	60" CMP	150	143		331
1.04.04.01	12" CMP	4	3		6
1.04.04.02	18" CMP	11	4		8
1.04.05	60" CMP	150	133		308
1.04.06	60" CMP	150	130		301
1.05.00	Channel	1000	30		65
1.05.01	12" CMP	4	3		7
1.06.00	Channel	1000	25		53
1.06.01	24" CMP	20	11		24
1.06.01.01	18" CMP	11	6		12

Note:  
***Bold Italicized*** = Undersized

TABLE 5-1  
 CAPACITY ANALYSIS EXISTING DRAINAGE FACILITIES

Pipe Number	Existing Storm Drainage System	Existing Capacity (cfs)	Estimated Flows (cfs)		
			10-Year	25-Year	100-Year
1.06.02	18" CMP	11	3		9
1.07.00	Channel	1000	12		26
1.07.01	18" CMP	11	4		8
1.07.02	23"x14" CMP	6	2		3
1.08.00	Channel	1000	3		7
1.08.01	18" CMP	6	2		3
1.08.02	18" CMP	6	0		1
<b>1.09.00</b>	<b>18" CMP</b>	<b>11</b>	<b>15</b>		<b>32</b>
1.09.01	18" CMP	11	7		14
2.00.00	10'x7.5' ARCH CMP	500		1451	2732
2.01.00	Channel			1853	3058
2.01.01	18" CMP	6	3		6
2.01.01.01	30" CMP	22	5		10
2.01.01.02	30" CMP	22	4		8
2.01.01.03	30" CMP	22	2		4
<b>2.01.01.04</b>	<b>24" CMP</b>	<b>20</b>	<b>42</b>		<b>77</b>
<b>2.01.01.05</b>	<b>18" CMP</b>	<b>6</b>	<b>27</b>		<b>49</b>
<b>2.01.01.06</b>	<b>24" CMP</b>	<b>20</b>	<b>27</b>		<b>49</b>
<b>2.01.01.07</b>	<b>24" CMP</b>	<b>20</b>	<b>26</b>		<b>47</b>
2.01.01.07.01	18" CMP	11	10		18
2.01.01.07.02	12" CMP	4	2		4
2.01.01.08	18" CMP	11	4		7
2.01.02	30" CMP, 36"x22" CMP	53	43		78
2.01.02.01	18" CMP	6	2		4
2.01.02.02	18" CMP	6	1		3
<b>2.01.03</b>	<b>18" CMP</b>	<b>11</b>	<b>36</b>		<b>66</b>
<b>2.01.04</b>	<b>18" CMP</b>	<b>11</b>	<b>33</b>		<b>60</b>
<b>2.01.05</b>	<b>18" CMP</b>	<b>11</b>	<b>32</b>		<b>58</b>
<b>2.01.06</b>	<b>24" CMP</b>	<b>20</b>	<b>26</b>		<b>46</b>
2.01.06.01	24" CMP	13	9		16
<b>2.01.07</b>	<b>18" CMP</b>	<b>11</b>	<b>12</b>		<b>22</b>
2.02.00	Channel		150	1314	2513
<b>2.02.01</b>	<b>48"x27" CMP, 36" CMP</b>	<b>100</b>	<b>143</b>		<b>275</b>
<b>2.02.01.01</b>	<b>48"x27" CMP</b>	<b>50</b>	<b>53</b>		<b>96</b>
<b>2.02.01.02</b>	<b>27"x18" CMP</b>	<b>13</b>	<b>47</b>		<b>85</b>
<b>2.02.01.02.01</b>	<b>27"x18" CMP</b>	<b>26</b>	<b>29</b>		<b>54</b>
<b>2.02.01.02.02</b>	<b>24" CMP</b>	<b>13</b>	<b>17</b>		<b>31</b>
2.02.01.02.02.01	24" CMP	20	17		32
2.02.01.02.02.02	24" CMP	20	17		31
2.02.01.02.03	24" CMP	20	10		18
<b>2.02.01.03</b>	<b>18" CMP</b>	<b>11</b>	<b>12</b>		<b>21</b>
2.02.01.04	12" CMP	7	3		5
2.02.01.05	8" CMP	4	2		4
<b>2.02.02</b>	<b>48"x27" CMP</b>	<b>50</b>	<b>89</b>		<b>173</b>

Note:  
***Bold Italicized*** = Undersized

TABLE 5-1 CAPACITY ANALYSIS EXISTING DRAINAGE FACILITIES					
Pipe Number	Existing Storm Drainage System	Existing Capacity (cfs)	Estimated Flows (cfs)		
			10-Year	25-Year	100-Year
<b>2.02.02.01</b>	<b>18" CMP</b>	<b>11</b>	<b>25</b>		<b>52</b>
2.02.02.02	24" CMP	20	15		31
2.02.02.03	27"x18" CMP	20	14		30
2.02.02.04	36" CMP	35	13		28
2.02.02.05	18" CMP	11	11		22
<b>2.02.03</b>	<b>36"x22" CMP</b>	<b>27</b>	<b>58</b>		<b>107</b>
<b>2.02.04</b>	<b>2-12" CMP</b>	<b>8</b>	<b>43</b>		<b>79</b>
<b>2.02.04.01</b>	<b>18" CMP</b>	<b>11</b>	<b>25</b>		<b>46</b>
2.02.04.01.01	12" CMP	4	2		3
2.02.04.01.02	12" CMP	4	1		2
2.02.04.01.03	12" CMP	4	1		3
2.02.05	18" CMP	11	9		15
<b>2.03.00</b>	<b>9-60" CMP</b>	<b>900</b>		<b>1672</b>	<b>2770</b>
2.04.00	18" CMP	11	4		8
3.00.00	Channel to Putah Creek			2524	4484
<b>3.01.00</b>	<b>3- 7'x5'1" CMP</b>	<b>720</b>		<b>1518</b>	<b>2484</b>
<b>3.01.01</b>	<b>12" CMP</b>	<b>4</b>	<b>7</b>		<b>12</b>
3.01.01.01	24" CMP	20	6		11
3.01.02	18" CMP	11	5		10
<b>3.02.00</b>	<b>Box Culvert</b>	<b>400</b>		<b>1482</b>	<b>2470</b>
3.02.01	48" CMP	50	24		43
<b>3.02.01.01</b>	<b>30" CMP</b>	<b>22</b>	<b>23</b>		<b>42</b>
3.02.01.01.01	18" CMP	6	2		3
3.02.01.02	18" CMP	11	7		13
<b>3.02.02</b>	<b>24" CMP</b>	<b>20</b>	<b>23</b>		<b>49</b>
3.02.03	24" CMP	20	25		32
3.02.03.01	18" CMP	11	4		8
3.02.04	24" CMP	20	9		19
4.01.00	Lake	-		631	910
<b>4.01.01</b>	<b>2-48" CMP</b>	<b>184</b>		<b>625</b>	<b>900</b>
4.01.01.01	18" CMP	20	8		14
<b>4.01.02</b>	<b>2-48" CMP</b>	<b>184</b>		<b>605</b>	<b>883</b>
4.01.02.01	24" CMP	20	24		44
<b>4.01.02.02</b>	<b>18" CMP</b>	<b>11</b>	<b>15</b>		<b>29</b>
<b>4.01.03</b>	<b>2-48" CMP</b>	<b>184</b>		<b>544</b>	<b>837</b>
<b>4.01.03.01</b>	<b>24" CMP</b>	<b>20</b>	<b>59</b>		<b>123</b>
<b>4.01.03.02</b>	<b>30" CMP</b>	<b>33</b>	<b>49</b>		<b>103</b>
4.01.03.02.01	18" CMP	6	2		5
<b>4.01.03.03</b>	<b>30" CMP</b>	<b>22</b>	<b>41</b>		<b>86</b>
4.01.03.04	30" CMP	33	32		67
4.01.03.04.01	18" CMP	6	2		4
4.01.03.04.02	24" CMP	13	9		19
4.01.03.05	24" CMP	20	15		31
<b>4.01.04</b>	<b>2-48" CMP</b>	<b>184</b>	<b>337</b>		<b>714</b>

Note:  
***Bold Italicized*** = Undersized

TABLE 5-1  
 CAPACITY ANALYSIS EXISTING DRAINAGE FACILITIES

Pipe Number	Existing Storm Drainage System	Existing Capacity (cfs)	Estimated Flows (cfs)		
			10-Year	25-Year	100-Year
4.01.04.01	12" CMP	4	4		7
<b><i>4.01.05</i></b>	<b><i>2-48" CMP</i></b>	<b><i>184</i></b>	<b><i>329</i></b>		<b><i>716</i></b>
<b><i>4.01.06</i></b>	<b><i>2-48" CMP</i></b>	<b><i>184</i></b>	<b><i>328</i></b>		<b><i>715</i></b>
<b><i>4.01.07</i></b>	<b><i>2-48" CMP</i></b>	<b><i>184</i></b>	<b><i>327</i></b>		<b><i>714</i></b>
<b><i>4.01.08</i></b>	<b><i>2-48" CMP</i></b>	<b><i>184</i></b>	<b><i>326</i></b>		<b><i>711</i></b>
4.01.08.01	18" CMP	6	4		8
4.02.00	Lake	-	114		231
<b><i>4.02.01</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>111</i></b>		<b><i>225</i></b>
<b><i>4.02.02</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>75</i></b>		<b><i>153</i></b>
<b><i>4.02.03</i></b>	<b><i>30" CMP</i></b>	<b><i>33</i></b>	<b><i>46</i></b>		<b><i>94</i></b>
4.02.03.01	18" CMP	6	2		5
4.02.04	24" CMP	20	23		48
4.02.04.01	18" CMP	6	4		8
4.02.05	12" CMP	2	6		13
4.02.06	12" CMP	4	1		2
4.03.00	Lake	-	7		13
4.03.01	18" CMP	6	2		4
4.04.00	Lake	-	136		255
<b><i>4.04.01</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>134</i></b>		<b><i>251</i></b>
4.04.01.01	18" CMP	11	10		18
<b><i>4.04.02</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>70</i></b>		<b><i>131</i></b>
<b><i>4.04.03</i></b>	<b><i>18" CMP</i></b>	<b><i>11</i></b>	<b><i>36</i></b>		<b><i>67</i></b>
<b><i>4.04.03.01</i></b>	<b><i>18" CMP</i></b>	<b><i>11</i></b>	<b><i>13</i></b>		<b><i>24</i></b>
4.05.00	Lake	-	7		14
4.05.01	18" CMP	6	2		4
4.06.00	Lake	-	10		18
4.06.01	18" CMP	6	5		9
<b><i>4.07.00</i></b>	<b><i>12" CMP</i></b>	<b><i>4</i></b>	<b><i>9</i></b>		<b><i>16</i></b>
4.07.01	24" CMP	13	4		7
4.08.00	Lake	-	8		14
4.08.01	18" CMP	6	4		7
4.09.00	Lake	-	12		24
4.09.01	18" CMP	6	5		10
4.10.00	Lake	-	127		247
<b><i>4.10.01</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>119</i></b>		<b><i>231</i></b>
4.10.01.01	18" CMP	11	6		11
4.10.01.02	18" CMP	11	9		18
4.10.01.02.01	18" CMP	6	2		5
4.10.01.02.02	18" CMP	6	3		5
<b><i>4.10.02</i></b>	<b><i>42" CMP</i></b>	<b><i>70</i></b>	<b><i>92</i></b>		<b><i>179</i></b>
4.10.02.01	18" CMP	6	1		3
<b><i>4.10.03</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>82</i></b>		<b><i>100</i></b>
<b><i>4.10.04</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>77</i></b>		<b><i>141</i></b>
<b><i>4.10.04.01</i></b>	<b><i>12" CMP</i></b>	<b><i>4</i></b>	<b><i>9</i></b>		<b><i>14</i></b>

Note:  
***Bold Italicized*** = Undersized

TABLE 5-1  
 CAPACITY ANALYSIS EXISTING DRAINAGE FACILITIES

Pipe Number	Existing Storm Drainage System	Existing Capacity (cfs)	Estimated Flows (cfs)		
			10-Year	25-Year	100-Year
4.10.04.02	18" CMP	11	6		12
4.10.04.03	12" CMP	4	8		13
<b><i>4.10.05</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>61</i></b>		<b><i>119</i></b>
4.10.05.01	24" CMP	20	19		36
<b><i>4.10.05.02</i></b>	<b><i>18" CMP</i></b>	<b><i>11</i></b>	<b><i>15</i></b>		<b><i>28</i></b>
<b><i>4.10.06</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>32</i></b>		<b><i>63</i></b>
4.10.07	18" CMP	11	2		5
4.11.00	Lake	-	51		90
4.11.01	36" CMP	50	45		90
4.11.01.01	12" CMP	2	2		4
<b><i>4.11.02</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>41</i></b>		<b><i>82</i></b>
4.11.02.01	18" CMP	11	8		17
<b><i>4.11.03</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>31</i></b>		<b><i>63</i></b>
4.11.03.01	18" CMP	11	3		7
4.11.03.02	18" CMP	11	2		5
<b><i>4.11.04</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>26</i></b>		<b><i>51</i></b>
4.11.05	24" CMP	15	18		35
4.11.06	18" CMP	11	11		22
5.01.00	Lake	-		983	1539
5.01.01	18" CMP	11	4		8
5.01.02	Node	-	672		1299
5.02.00	Node	-	656		1268
6.00.00	Node Meeting SW 5	-		683	1406
<b><i>6.01.00</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>24</i></b>		<b><i>30</i></b>
6.01.01	18" CMP	6	4		5
6.01.02	18" CMP	6	1		2
<b><i>6.02.00</i></b>	<b><i>36" CMP</i></b>	<b><i>50</i></b>	<b><i>51</i></b>		<b><i>150</i></b>
6.02.01	18" CMP	11	8		10
6.02.01.01	18" CMP	11	1		1
6.02.02	18" CMP	11	5		7
6.02.03	18" CMP	11	4		5
<b><i>6.03.00</i></b>	<b><i>2-48" CMP</i></b>	<b><i>104</i></b>	<b><i>199</i></b>		<b><i>410</i></b>
6.03.01	18" CMP	11	1		1
6.03.02	18" CMP	11	5		6
<b><i>6.03.03</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>30</i></b>		<b><i>62</i></b>
<b><i>6.03.03.01</i></b>	<b><i>24" CMP</i></b>	<b><i>20</i></b>	<b><i>22</i></b>		<b><i>46</i></b>
<b><i>6.04.00</i></b>	<b><i>2-50"x31" CMP</i></b>	<b><i>120</i></b>	<b><i>142</i></b>		<b><i>316</i></b>
<b><i>6.05.00</i></b>	<b><i>2-50"x31" CMP</i></b>	<b><i>120</i></b>	<b><i>140</i></b>		<b><i>312</i></b>
<b><i>6.06.00</i></b>	<b><i>18" CMP</i></b>	<b><i>11</i></b>	<b><i>13</i></b>		<b><i>27</i></b>
6.06.01	18" CMP	11	1		1
6.06.02	18" CMP	11	8		17

If the drainage facility capacity is less than the design flow, the structure is assumed to be inadequate and recommendations for correction or replacement are provided. Table 5-2 provides a listing of the locations where the existing facilities are undersize. Replacement costs are presented in Chapter 6.

**TABLE 5-2  
IDENTIFIED DEFICIENT FACILITIES**

Pipe Number	Existing Storm Drainage System	Node Location	Proposed Improvements
1.01.00	Pump Station	Mt. Meadow South	Increase Pump Capacity
1.04.01.02	18" CMP	Maple Leaf Ct.	Replace with 24" RCP
1.04.02	3-48" CMP	Golf Course Near Mt. Meadow South	Add 21" RCP
1.04.02.01	12" CMP	Old Creek Road	Replace with 18" RCP
1.04.02.04	24" CMP	Mt. Meadow North	Add 30" RCP
1.04.03.02	24" CMP	Powder Horn	Add 18" RCP
1.09.00	18" CMP	Powder Horn	Replace with 21" RCP
2.01.01.04	24" CMP	Hidden Valley Road	Add 27" RCP
2.01.01.05	18" CMP	Hidden Valley Road	Replace with 30" RCP
2.01.01.06	24" CMP	Hidden Valley Road	Replace with 30" RCP
2.01.01.07	24" CMP	Moon Ridge Road	Replace with 30" RCP
2.01.03	18" CMP	Golf Course near Spyglass Road	Add 30" RCP
2.01.04	18" CMP	Deer Hollow Road	Replace with 30" RCP
2.01.05	18" CMP	Deer Hollow Road	Replace with 30" RCP
2.01.06	24" CMP	Hidden Valley Road	Add 18" RCP
2.01.07	18" CMP	Moon Ridge Road	Replace with 21" RCP
2.02.01	48"x27" CMP, 36" CMP	Spyglass Road	Replace w/ 7½x3 Box Culvert
2.02.01.01	48"x27" CMP	Deer Hollow Road	Replace with 50"x31" RCP
2.02.01.02	27"x18" CMP	Golf Course near Deer Hollow Road	Replace with 45"x29" RCP
2.02.01.02.01	27"x18" CMP	Hidden Valley Road	Replace with 30" RCP
2.02.01.02.02	24" CMP	Hidden Valley Road	Add 21" RCP
2.02.01.03	18" CMP	Hidden Valley Road	Replace with 21" RCP
2.02.02	48"x24" CMP	Bunker Road	Add 36" RCP
2.02.02.01	18" CMP	Golf Course Near Bunker Road	Add 21" RCP
2.02.03	36"x22" CMP	Deer Hollow Road	Replace with 30" RCP
2.02.04	2-12" CMP	Golf Course near Deer Hollow Road	Replace with 50"x31" RCP
2.02.04.01	18" CMP	Hidden Valley Road	Add 21" RCP
2.03.00	9-60" CMP	Hidden Valley Road	Replace 4 Pipes w/ 4-54" RCP
3.01.00	3-7'-5'1" CMP	Mt. Meadow North	Replace w/ 8-5x5 Box Culverts
3.01.01	12" CMP	Donkey Hill Road	Replace with 18" RCP

**TABLE 5-2  
IDENTIFIED DEFICIENT FACILITIES**

Pipe Number	Existing Storm Drainage System	Node Location	Proposed Improvements
3.02.00	Box Culvert	Hartman Road	Replace with Box Culvert
3.02.01.01	30" CMP	Camp Ground	Replace with 33" RCP
3.02.02	24" CMP	Donkey Hill Road	Replace with 30" RCP
3.02.03	24" CMP	Donkey Hill Road	Replace with 30" RCP
4.01.01	2-48" CMP	North Shore Drive	Replace w/ 20'x4' Box Culvert
4.01.02	2-48" CMP	Deer Hill Road	Replace w/ 20'x4' Box Culvert
4.01.02.02	18" CMP	Deer Hill & Marine View Roads	Replace with 21" RCP
4.01.03	2-48" CMP	Oak Grove Road	Replace w/ 20'x4' Box Culvert
4.01.03.01	24" CMP	Greenridge Road	Add 24" RCP
4.01.03.02	30" CMP	Buckhorn Road	Add 24" RCP
4.01.03.03	30" CMP	Coyle Springs Road	Add 24" RCP
4.01.04	2-48" CMP	Greenridge Road	Replace w/ 12'x4' Box Culvert
4.01.05	2-48" CMP	Squirrel Hill Road	Replace w/ 12'x4' Box Culvert
4.01.06	2-48" CMP	Stonegate Road	Replace w/ 12'x4' Box Culvert
4.01.07	2-48" CMP	Coyle Springs Road	Replace w/ 12'x4' Box Culvert
4.02.01	24" CMP	North Shore Drive	Replace with 2-42" RCP
4.02.02	24" CMP	Deer Hill Road	Replace with 2-33" RCP
4.02.03	30" CMP	Greenridge Road	Add 21" RCP
4.02.05	12" CMP	Coyle Springs Road	Replace with 15" RCP
4.04.01	36" CMP	North Shore Drive	Replace with 2-42" RCP
4.04.02	36" CMP	Deer Hill Road	Replace with 42" RCP
4.04.03	18" CMP	Meadow View Drive	Replace with 33" RCP
4.04.03.01	18" CMP	Fiddlers Drive	Replace with 21" RCP
4.07.00	12" CMP	Lake Ridge Circle	Replace with 18" RCP
4.10.01	36" CMP	North Shore Drive	Add 42" RCP
4.10.02	42" CMP	Greenridge Road	Add 27" RCP
4.10.03	36" CMP	Hawk's Hill Road	Add 30" RCP
4.10.04	36" CMP	Kentwood Place	Add 27" RCP
4.10.04.01	12" CMP	Kentwood Place	Add 15" RCP
4.10.04.03	12" CMP	Spruce Grove Road	Replace with 18" RCP
4.10.05	36" CMP	Deer Hill Road	Add 18" RCP
4.10.05.02	18" CMP	Hacienda Court	Add 15" RCP
4.10.06	24" CMP	Spruce Grove Road	Add 21" RCP
4.11.02	24" CMP	Deer Hill Road	Add 27" RCP
4.11.03	24" CMP	Greenridge & Oak Grove Roads	Add 18" RCP
4.11.04	24" CMP	Greenridge Road	Add 15" RCP
6.01.00	24" CMP	Conestoga Road	Add 15" RCP



**TABLE 5-2  
IDENTIFIED DEFICIENT FACILITIES**

<b>Pipe Number</b>	<b>Existing Storm Drainage System</b>	<b>Node Location</b>	<b>Proposed Improvements</b>
6.02.00	36" CMP	Conestoga Road	Replace with 42" RCP
6.03.00	2-48" CMP	Conestoga Road	Replace with 2-54" RCP
6.03.03	24" CMP	Eagle Rock Road	Add 18" RCP
6.03.03.01	24" CMP	Eagle Rock Road	Replace with 27" RCP
6.04.00	2-50"x31" CMP	Deer Hill Road	Replace with 2-58"x36" RCP
6.05.00	2-50"x31" CMP	Eagle Rock Road	Replace with 2-58"x36" RCP
6.06.00	18" CMP	Eagle Rock Road	Replace with 24" RCP

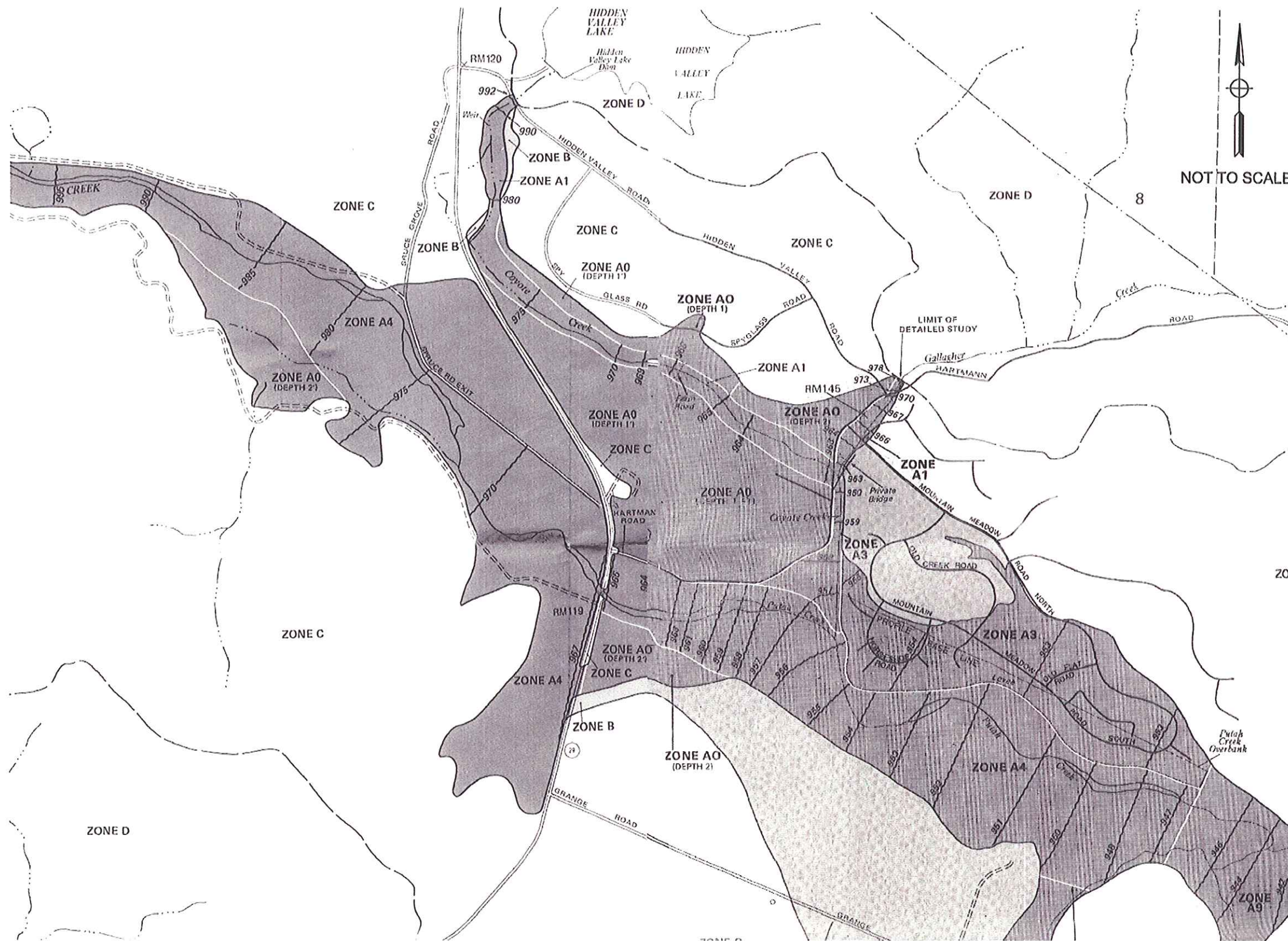
In addition to drainage ditches and culverts, the existing stormwater pump station has been analyzed. The station accepts flow from a tributary drainage area that is less than one square mile: By the *Lake County Standards* the design flow could be as low as the 10-year flow. The station has an approximate capacity of 6,000 to 8,000 gpm (13.4 to 17.8 cfs). The 10-year flow is 368 cfs.

### **III. COYOTE CREEK AND GALLAGHER CREEK ANALYSIS**

#### **A. DESCRIPTION**

In March 1998, FEMA published an analysis of Coyote and Gallagher Creeks, which indicated potential for flooding along the Coyote Creek corridor. The flooding pattern is published in the March 2, 1998 Flood Insurance Rate Maps (FIRM) and illustrated in Figure 5-7. In order to develop the FIRM Maps, FEMA developed a series of creek cross-sections and an HEC-2 model. The FEMA cross-sections for Coyote Creek and Gallagher Creek were used as the basis for this Storm Water Mater Plan.

This Storm Water Mater Plan developed independent 100-year design flows for both the Coyote Creek and Gallagher Creek Watershed, using HEC-1 and the SCS Type 1A rainfall distribution. These flows are higher than the design flows used in the FEMA modeling effort. Information regarding how FEMA design flows were generated could not be determined. Department of Water Resources calculated 100-year design flows which were slightly higher than the design flows presented in the report. Discussions with Lake County regarding the design flows concluded that design flows presented in the report are reasonable and should be utilized for Master Plan design. When the current estimated flows are entered into the original HEC-2 model, flooding exceeds the flooding limits indicated on the FIRM mapping.



### LEGEND

- 500-Year Flood Boundary
- 100-Year Flood Boundary
- Zone Designations\*
- 100-Year Flood Boundary
- 500-Year Flood Boundary
- Base Flood Elevation Line With Elevation In Feet\*\* 513
- Base Flood Elevation in Feet Where Uniform Within Zone\*\* (EL 987)
- Elevation Reference Mark RM7X
- Zone D Boundary
- River Mile M1.5
- Approximate 100- Year Flood Boundary ZONE A

- \*\*Reference to the National Geodetic Vertical Datum of 1929
- UNDEVELOPED COASTAL BARRIERS†
- Identified 1983
  - Identified 1990
  - Otherwise Protected Areas

† Coastal barrier areas are normally located within or adjacent to special flood hazard areas.

### \*EXPLANATION OF ZONE DESIGNATIONS

ZONE	EXPLANATION
A	Areas of 100-year flood; base flood elevations and flood hazard factors not determined.
AO	Areas of 100-year shallow flooding where depths are between one (1) and three (3) feet; average depths of inundation are shown, but no flood hazard factors are determined.
AH	Areas of 100-year shallow flooding where depths are between one (1) and three (3) feet; base flood elevations are shown, but no flood hazard factors are determined.
A1-A30	Areas of 100-year flood; base flood elevations and flood hazard factors determined.
A99	Areas of 100-year flood to be protected by flood protection system under construction; base flood elevations and flood hazard factors not determined.
B	Areas between limits of the 100-year flood and 500-year flood; or certain areas subject to 100-year flooding with average depths less than one (1) foot or where the contributing drainage area is less than one square mile; or areas protected by levees from the base flood. (Medium shading)
C	Areas of minimal flooding. (No shading)
D	Areas of undetermined, but possible, flood hazards.
V	Areas of 100-year coastal flood with velocity (wave action); base flood elevations and flood hazard factors not determined.
V1-V30	Areas of 100-year coastal flood with velocity (wave action); base flood elevations and flood hazard factors determined.

FIGURE 5-7  
FLOOD ZONE MAP



**B. CAPACITY OF EXISTING FACILITIES**

Coyote Creek currently is a relatively natural channel that averages 15 to 25 feet wide and 3 to 8 feet deep. The hydraulic capacity of this channel is estimated to be 600- to 1000-cfs.

The existing Gallagher Creek channel from its confluence with Coyote Creek upstream to the crossing of Hartman is incapable of handling the 10-year storm event without over topping its banks.

Recommendations for the improvement work along Coyote and Gallagher Creek are presented in Chapter 6.

## CHAPTER 6 - RECOMMENDATIONS AND COST ESTIMATES

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### I. COST ESTIMATE AND PRIORITIES

#### A. COST ESTIMATE DEVELOPMENT

Cost estimates for the drainage improvements are developed using Means Construction Cost Data. The following items are added to this subtotal amount:

- General Conditions (30%)
- Sales Tax (4%)
- General Contractors Overhead and Profit (8%)
- Legal, Administration & Engineering (25%)
- Bond (0.15%)
- Contingency (10%)

#### B. PROJECT PRIORITY ANALYSIS

The costs for all drainage improvements are substantial, ranging in cost from \$3,689,770 to \$8,707,110, and will require a number of years to complete. This Master Plan prioritizes the various improvements by watershed. Several factors were used in prioritizing the projects. Generally entire sub-watersheds were picked for improvement based on how undersized the drainage facilities are and the potential for flooding impacts if known: improvements were made from downstream to upstream within the individual sub-watersheds, although this factor was modified depending on the severity of the storm drain deficiency.

#### C. SUMMARY COSTS AND PRIORITIES

This chapter summarizes proposed drainage improvements, their costs and priority. All improvements are listed in Table 6-1. The projects are prioritized within each watershed.

**TABLE 6-1  
RECOMMENDED ORDER OF IMPROVEMENTS**

Priority	Pipe No.	Location	Improvement	Cost
1		Coyote Creek Alternative 3	Widen Channel & Install Weir	\$240,160*
1		Coyote Creek Alternative 2	Widen Channel & Install Weir	\$427,900
1		Coyote Creek Alternative 1	Excavate to Widen Channel	\$713,000
2		Gallagher Creek	Widen Channel	\$79,020
3	1.01.00	Pump Station Alternative 1	Construct new Pump Station	\$4,633,750
3	1.01.00	Pump Station Alternative 2A	10' x 5' Box Culvert	\$3,707,000
3	1.01.00	Pump Station Alternative 2B	Graded Channel	\$89,250*
1	1.04.02.04	Mt. Meadow North	Add 30" RCP	\$26,670
2	1.04.02.01	Old Creek Road	Replace with 18" RCP	\$19,630
3	1.04.01.02	Maple Leaf CT.	Replace with 24" RCP	\$20,960
4	1.04.03.02	Powder Horn	Add 18" RCP	\$19,260
5	1.09.00	Powder Horn	Replace with 21" RCP	\$20,220
6	1.04.02	Golf Course Near Mt. Meadow South	Add 21" RCP	\$17,440
1	2.03.00	Hidden Valley Road	Replace 4 Pipes w/ 4-54"RCP	\$60,570
2	2.0	Hartman Road	Replace w/ 3-10x6 Box Culvert	\$278,030
3	2.02.01	Spyglass Road	Replace w/ 7½x3 Box Culvert	\$126,540
4	2.02.04	Golf Course near Deer Hollow Road	Replace with 50"x31" RCP	\$28,750
5	2.02.03	Deer Hollow Road	Replace with 30" RCP	\$27,200
6	2.02.02	Bunker Road	Add 36" RCP	\$28,380
7	2.02.04.01	Hidden Valley Road	Add 21" RCP	\$19,850
8	2.01.01.04	Hidden Valley Road	Add 27" RCP	\$26,000
9	2.01.01.05	Hidden Valley Road	Replace with 30" RCP	\$27,040
10	2.01.03	Golf Course near Spyglass Road	Add 30" RCP	\$26,670
11	2.01.04	Deer Hollow Road	Replace with 30" RCP	\$26,250
12	2.01.05	Deer Hollow Road	Replace with 30" RCP	\$27,040
13	2.02.02.01	Golf Course Near Bunker Road	Add 21" RCP	\$19,850
14	2.01.01.06	Hidden Valley Road	Replace with 30" RCP	\$27,040
15	2.01.01.07	Moon Ridge Road	Replace with 30" RCP	\$27,040
16	2.02.01.01	Deer Hollow Road	Replace with 50"x31" RCP	\$44,530
17	2.02.01.02	Golf Course near Deer Hollow Road	Replace with 45"x29" RCP	\$28,900
18	2.02.01.02.01	Hidden Valley Road	Replace with 30" RCP	\$26,250
19	2.02.01.02.02	Hidden Valley Road	Add 21" RCP	\$19,850
20	2.02.01.03	Hidden Valley Road	Replace with 21" RCP	\$19,750
21	2.01.06	Hidden Valley Road	Add 18" RCP	\$18,890
22	2.01.07	Moon Ridge Road	Replace with 21" RCP	\$32,620
1	3.01.00	Mt. Meadow North	Replace w/ 8-5x5 Box Culverts	\$159,860
2	3.02.00	Hartman Road	Replace with Box Culvert	25,950
3	3.02.03	Donkey Hill Road	Replace with 30" RCP	\$27,200

**TABLE 6-1  
RECOMMENDED ORDER OF IMPROVEMENTS**

Priority	Pipe No.	Location	Improvement	Cost
4	3.02.02	Donkey Hill Road	Replace with 30" RCP	\$27,200
5	3.01.01	Donkey Hill Road	Replace with 18" RCP	\$19,200
6	3.02.01.01	Camp Ground	Replace with 33" RCP	\$28,280
1	4.01.01	North Shore Drive	Replace w/ 20'x4' Box Culvert	\$85,630
2	4.01.02	Deer Hill Road	Replace w/ 20'x4' Box Culvert	\$85,630
3	4.01.03	Oak Grove Road	Replace w/ 20'x4' Box Culvert	\$85,630
4	4.01.04	Greenridge Road	Replace w/ 12'x4' Box Culvert	\$62,650
5	4.01.05	Squirrel Hill Road	Replace w/ 12'x4' Box Culvert	\$62,650
6	4.01.06	Stonegate Road	Replace w/ 12'x4' Box Culvert	\$62,650
7	4.01.07	Coyle Springs Road	Replace w/ 12'x4' Box Culvert	\$62,650
8	4.01.08	Greenridge Road	Replace w/ 12'x4' Box Culvert	\$62,650
9	4.01.03.01	Greenridge Road	Add 24" RCP	\$20,590
10	4.01.03.04 to 4.01.03.02	Coyle Springs Road	Replace w/ 36" RCP	\$202,320
11	4.01.02.01	Green Ridge	Add 21" RCP	\$19,850
12	4.01.02.02	Deer Hill & Marine View Roads	Replace with 21" RCP	\$20,220
13	4.10.01	North Shore Drive	Add 42" RCP	\$29,750
14	4.10.02	Greenridge Road	Add 27" RCP	\$26,000
15	4.10.03	Hawk's Hill Road	Add 30" RCP	\$26,670
16	4.10.04	Kentwood Place	Add 27" RCP	\$26,000
17	4.10.05	Deer Hill Road	Add 18" RCP	\$19,260
18	4.10.06	Spruce Grove Road	Add 21" RCP	\$19,850
19	4.10.04.01	Kentwood Place	Add 15" RCP	\$18,630
20	4.02.01	North Shore Drive	Replace with 2-42" RCP	\$49,120
21	4.02.02	Deer Hill Road	Replace with 2-33" RCP	\$44,890
22	4.02.03	Greenridge Road	Add 21" RCP	\$23,560
23	4.04.01	North Shore Drive	Replace with 2-42" RCP	\$41,700
24	4.04.02	Deer Hill Road	Replace with 42" RCP	\$30,120
25	4.04.03	Meadow View Drive	Replace with 33" RCP	\$28,010
26	4.04.03.01	Fiddlers Drive	Replace with 21" RCP	\$20,220
27	4.02.04	Stonegate Road	Add 27" RCP	\$26,000
28	4.02.05	Coyle Springs Road	Add 15" RCP	\$19,000
29	4.10.04.03	North Shore Drive	Add 18" RCP	\$19,630
30	4.10.05.02	Hacienda Court	Add 15" RCP	\$18,630
31	4.11.02	Deer Hill Road	Add 27" RCP	\$26,000
32	4.11.03	Greenridge & Oak Grove Roads	Add 18" RCP	\$19,260
33	4.11.04	Greenridge Road	Add 15" RCP	\$18,630
34	4.07.00	Lake Ridge Circle	Replace with 18" RCP	\$19,630
35	4.11.03.02	Fernwood Road to Deer Hill Road	Replace with 30" RCP	\$225,000
1	6.04.00	Deer Hill Road	Replace with 2-58"x36" RCP	\$52,010
2	6.05.00	Eagle Rock Road	Replace with 2-58"x36" RCP	\$52,010
3	6.03.00	Conestoga Road	Replace with 2-54" RCP	\$54,380
4	6.03.03	Eagle Rock Road	Add 18" RCP	\$19,260

TABLE 6-1 RECOMMENDED ORDER OF IMPROVEMENTS				
Priority	Pipe No.	Location	Improvement	Cost
5	6.01.00	Conestoga Road	Add 15" RCP	\$18,630
6	6.03.03.01	Eagle Rock Road	Replace with 27" RCP	\$26,380
7	6.06.00	Eagle Rock Road	Replace with 24" RCP	\$20,960
8	6.02.00	Conestoga Road	Replace with 42" RCP	\$30,120
			<b>PROJECT TOTAL</b>	<b>\$3,689,770</b>

\*Alternative included in Project Total Cost

## II. HIDDEN VALLEY LAKE SUBDIVISION

### A. DRAINAGE STRUCTURES

Approximately 78 culverts within the Subdivision will need to be replaced to accommodate the design flows. The replacements are generally recommended in areas where the culverts cross roadways within the subdivision. Figures 6-1 through 6-5 illustrates the location of the proposed improvements. The total estimated cost of improvements is \$ 3,689,770.

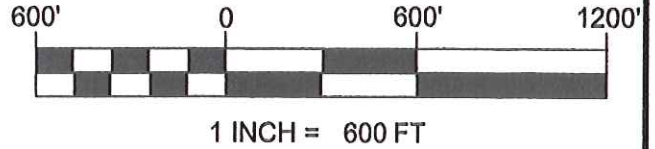
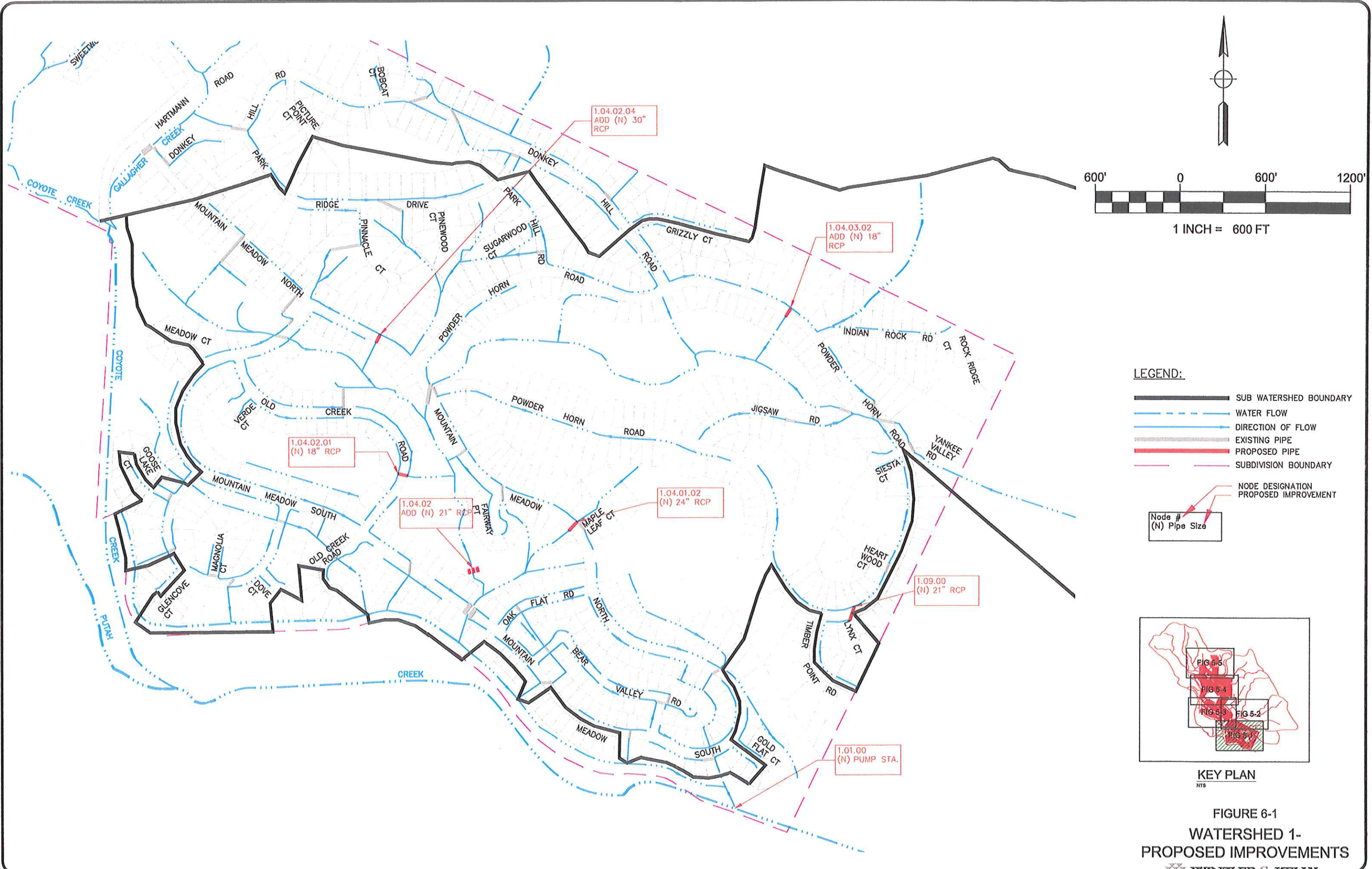
### B. PUMP STATION

The existing storm water pump station should be upgraded if 100-year flood protection is desired in Watershed 1. The Putah Creek Levee Evaluation will determine the storm recurrence interval for the interior and exterior of the levee. The District has developed some preliminary design work for the addition of two additional high capacity stormwater pumps.

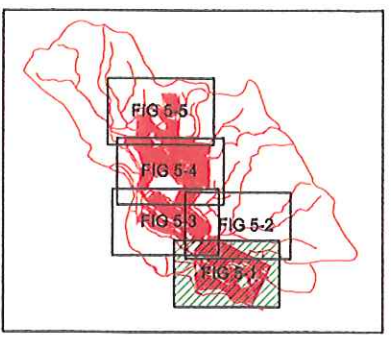
With the available detention storage under 10-year design conditions, the pump station and bypass system must provide a total capacity of 235 cfs. This is available through the bypass conduit; however, the existing pumping station and detention pond is undersized to provide adequate flood protection when high flows in Putah Creek eliminate the bypass conduit.

The existing pump station configuration provides for 235 cfs of bypass capacity through a 72-inch CMP. The 72-inch CMP is operational until the flood level in Putah Creek reaches elevation 935. The pump station itself has approximately 6,000 to 8,000 gpm (13.4 to 17.8 cfs) of pumping capacity and approximately 10-acre feet of storm water detention storage.

With the available detention storage under 100-year design conditions, the required capacity of the pump station is 555 cfs. This is well beyond the existing available capacity.

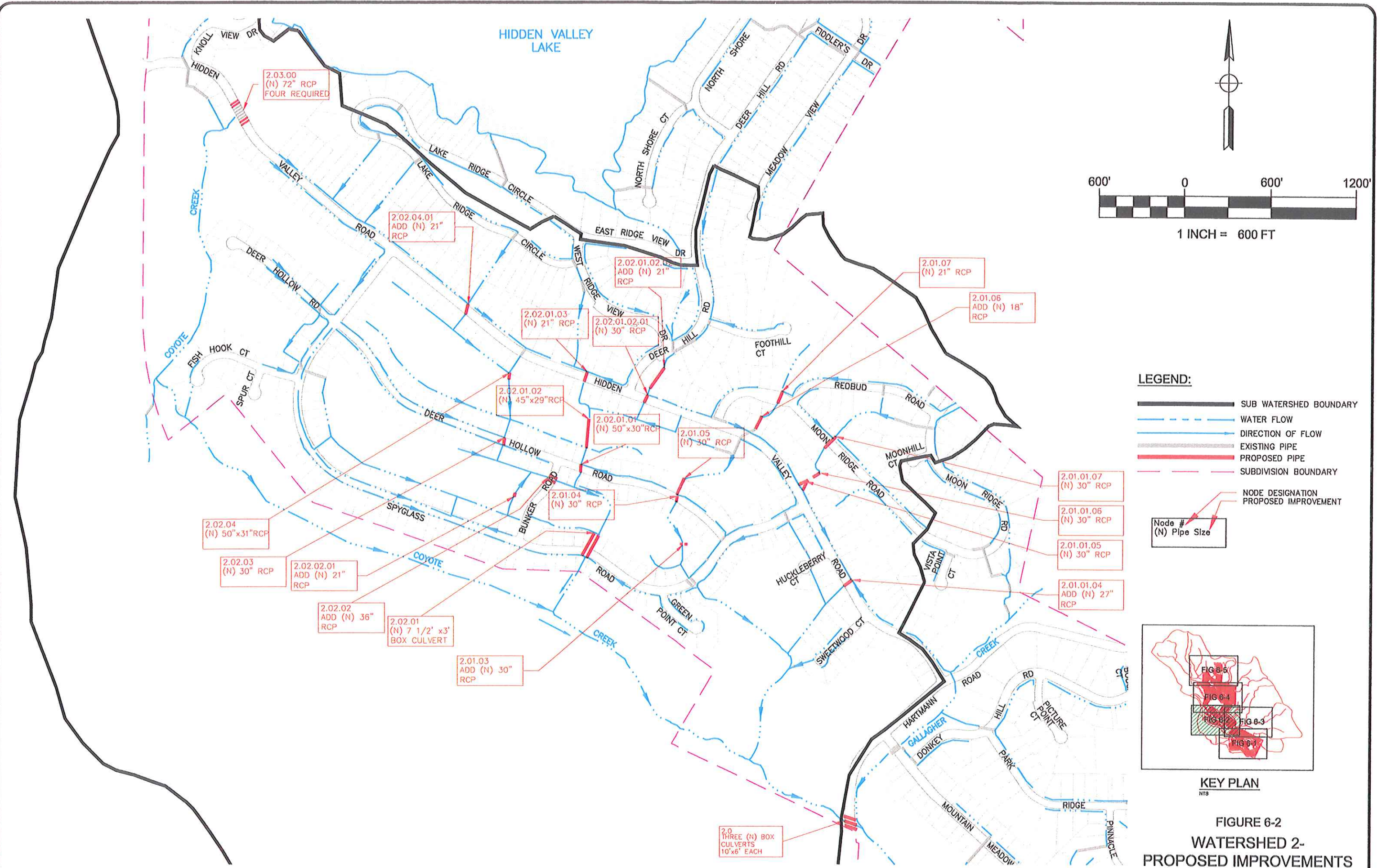


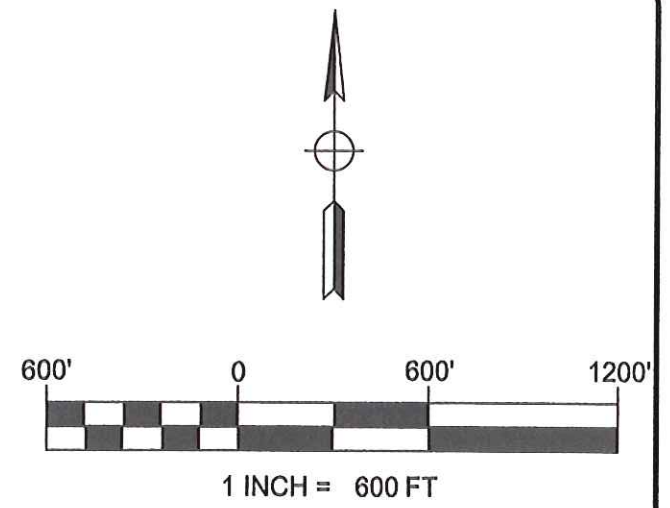
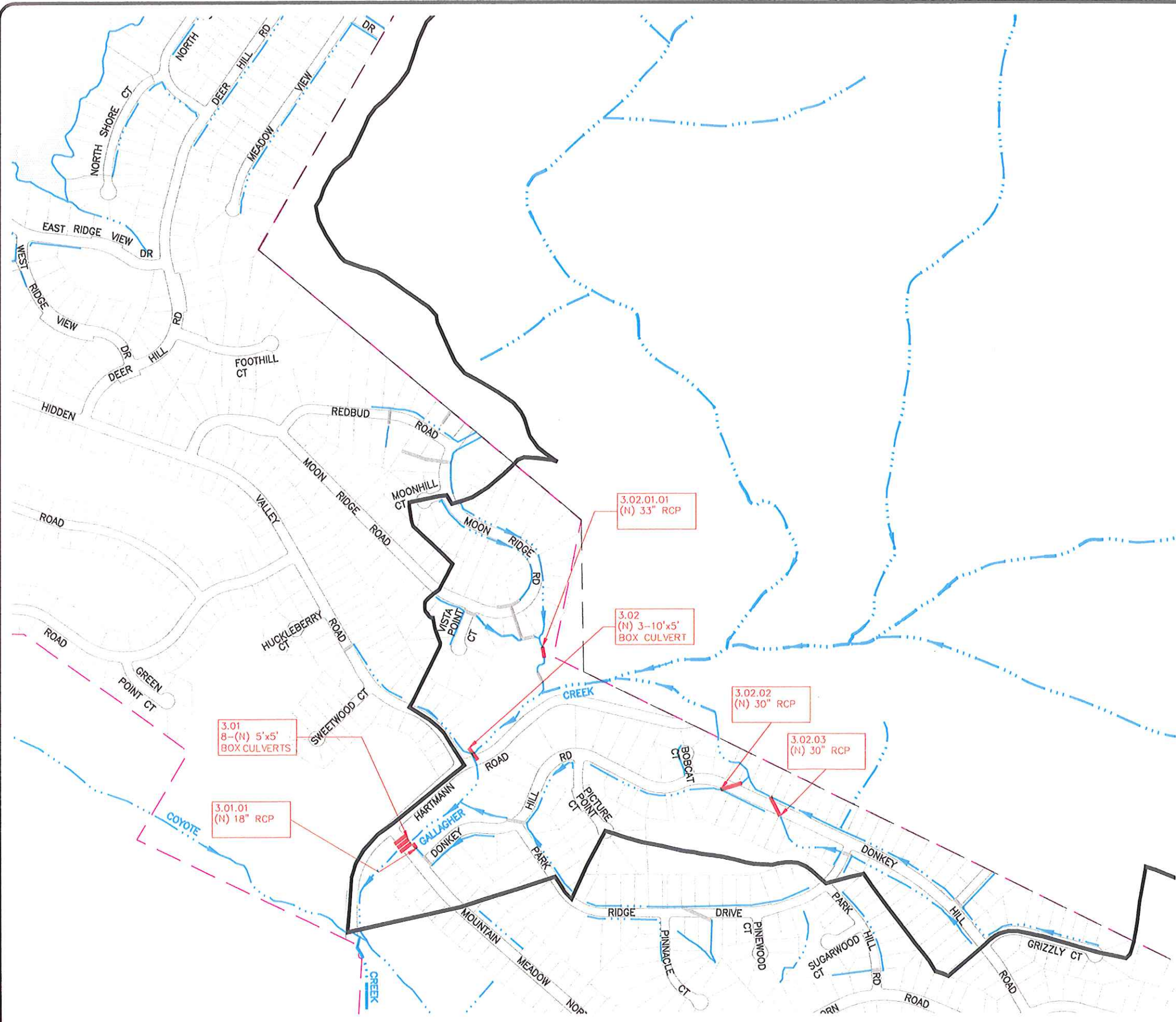
- LEGEND:**
- SUB WATERSHED BOUNDARY
  - WATER FLOW
  - DIRECTION OF FLOW
  - EXISTING PIPE
  - PROPOSED PIPE
  - SUBDIVISION BOUNDARY
- NODE DESIGNATION  
 PROPOSED IMPROVEMENT
- Node #  
 (N) Pipe Size



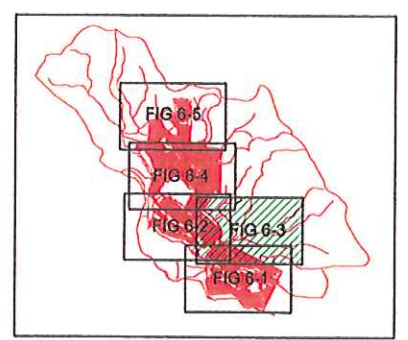
**KEY PLAN**  
 FIGURE 6-1  
 WATERSHED 1-  
 PROPOSED IMPROVEMENTS





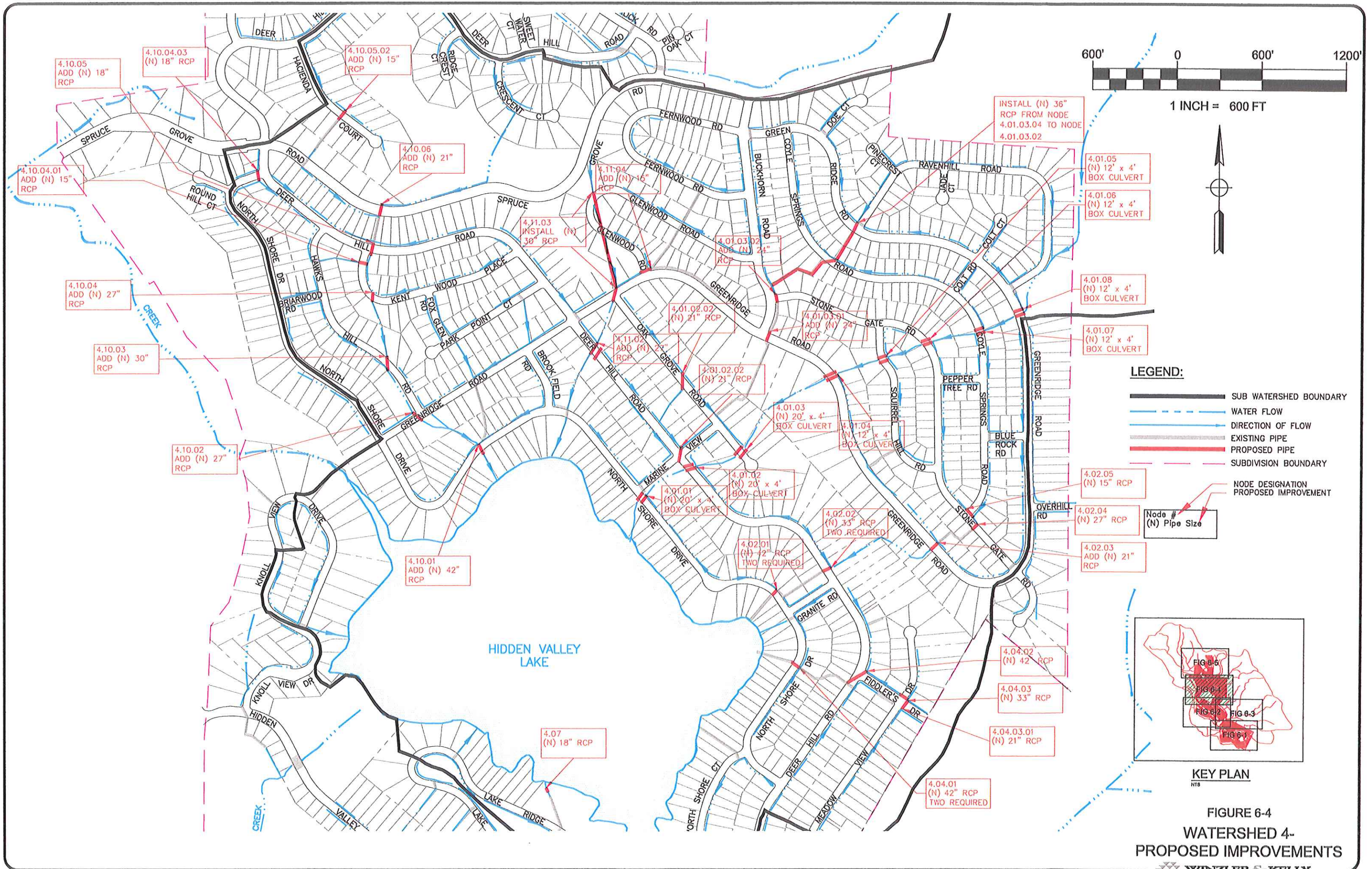


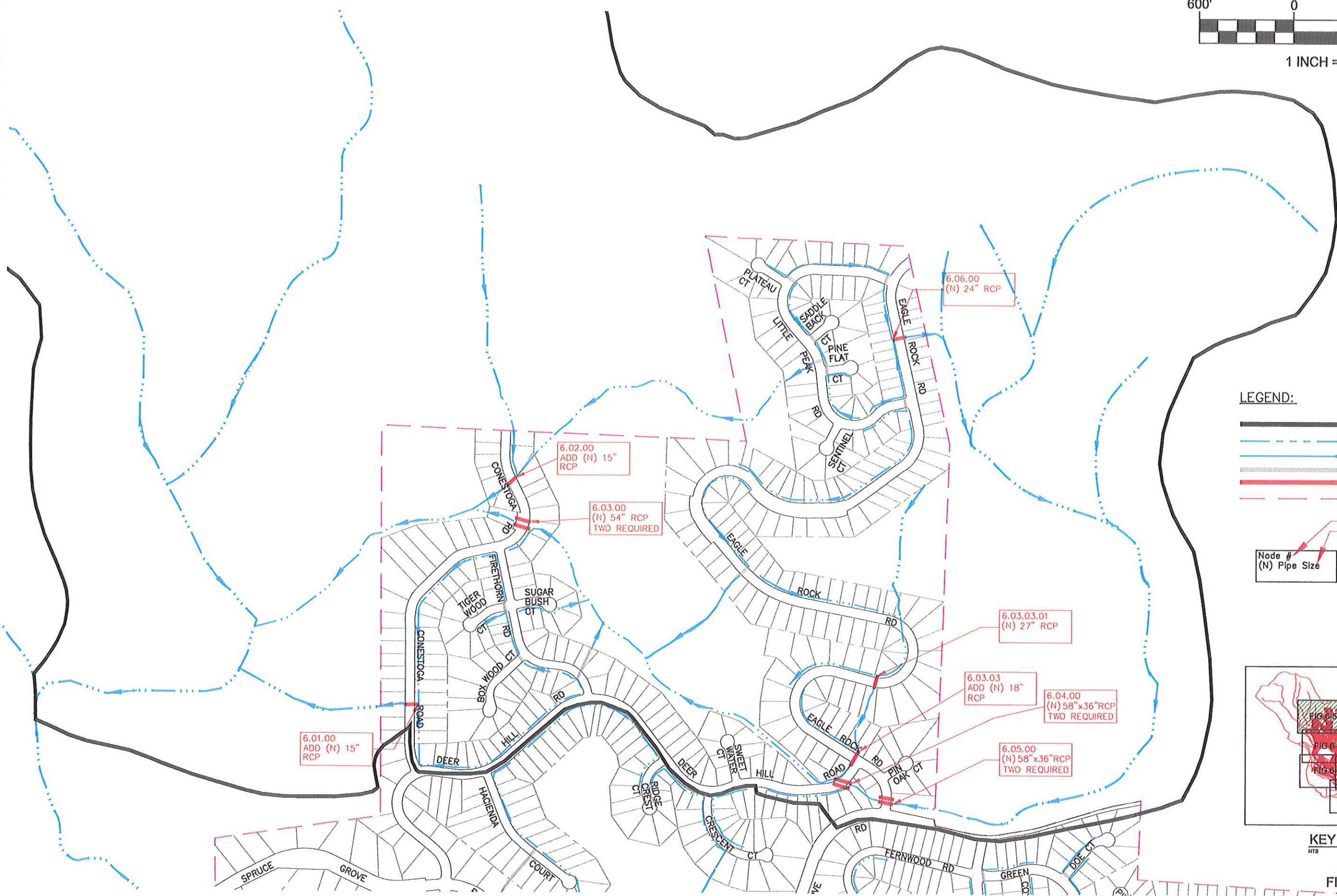
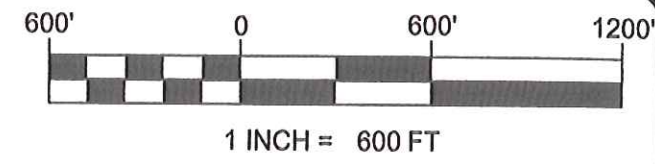
- LEGEND:**
- SUB WATERSHED BOUNDARY
  - WATER FLOW
  - DIRECTION OF FLOW
  - EXISTING PIPE
  - PROPOSED PIPE
  - SUBDIVISION BOUNDARY
  - NODE DESIGNATION
  - PROPOSED IMPROVEMENT
- Node #  
 (N) Pipe Size



**KEY PLAN**  
 NTS

**FIGURE 6-3**  
**WATERSHED 3-**  
**PROPOSED IMPROVEMENTS**

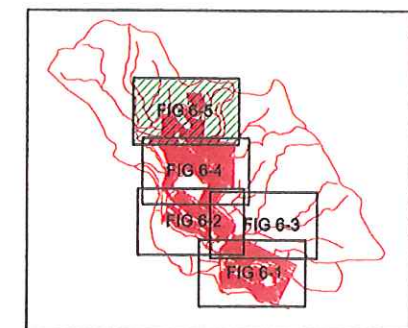




**LEGEND:**

- SUB WATERSHED BOUNDARY
- WATER FLOW
- DIRECTION OF FLOW
- EXISTING PIPE
- PROPOSED PIPE
- SUBDIVISION BOUNDARY
- NODE DESIGNATION PROPOSED IMPROVEMENT

Node #  
(N) Pipe Size



**KEY PLAN**  
NTS

**FIGURE 6-5  
WATERSHED 6-  
PROPOSED IMPROVEMENTS**

The district has purchased two 100 HP pumps, when installation will increase the capacity of the pump station adding approximately 44 cfs. As can be seen from the above analysis, these pumps will not be adequate to handle the 10-year or 100-year runoff during high water conditions on Putah Creek.

Several options have been explored. It may be possible to extend a gravity system downstream tying into Putah Creek at a water surface that would allow gravity flow even at 100-year flows in Putah Creek. Based on the existing FEMA mapping, a water surface of 944 on Putah Creek occurs approximately 2000 feet downstream of the pump station site. However, a large gravity pipe system would be required to handle the total flows, estimated as three 10'x 5' RCB's or, alternatively, it may be possible to construct an earthen channel to carry this flow. This channel is estimated to be 30 feet wide, 6 feet deep with 2:1 side slopes.

It may be possible to construct detention basin facilities upstream through the golf course. Rough estimates indicate that 18 to 27 acre-feet of storage could be developed by construction of earthen berms across the channel at key locations. This storage would potentially reduce runoff to the pump station to between 130 and 165 cfs during a 10-year event and between 395 and 470 cfs during a 100-year event. With the maximum sized detention capacity in place, the gravity system would still require dual 10'x 5' RCB's or an earthen channel with a bottom width of 15 feet.

The other option would be to upsize the pump station as required depending on what other improvements (such as detention basins) are constructed. The alternatives need to be further investigated during the evaluation of the Putah Creek levee. The actual design criteria approved by FEMA needs to be established. It is unclear at this time what the internal design (pump station) and external Putah Creek flooding levels are.

### **III. COYOTE CREEK CHANNEL**

#### **A. ALTERNATIVES REVIEWED**

The hydraulic capacity of the Coyote Creek channel within the subdivision was reviewed utilizing the FEMA cross sections as a basis for the hydraulic analysis. Coyote Creek, in its current configuration below the Hidden Valley Lake Dam (20 to 25 feet wide and 3 feet deep), has an approximate carrying capacity of 650 to 950 cubic feet per second (cfs). Currently, the creek splits below Hidden Valley Lake; a 500-cfs bypass system carries a portion of the Creek under Highway 29. The remaining flow is carried in the main creek channel along the southern boundary of the Subdivision. Coyote Creek meets Putah Creek near Hartman Road. An existing

flood control levee separates Putah Creek from the Subdivision below the confluence. Table 6-2 below outlines the anticipated flows and channel capacity in Coyote Creek downstream from Hidden Valley Lake Dam.

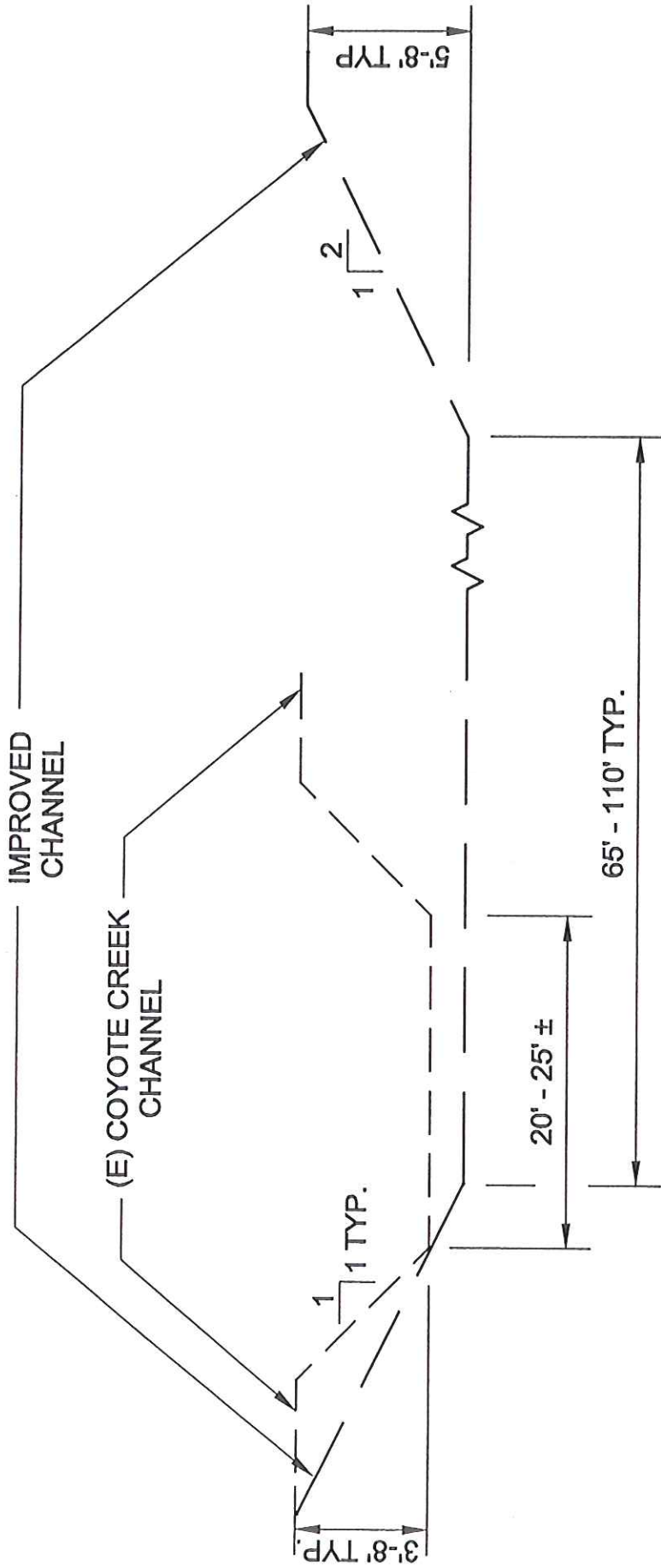
<b>Design Flow</b>	<b>Below Hidden Valley Lake</b>	<b>At Highway 29 Bypass</b>	<b>At Hartman Road</b>	<b>At Putah Creek Confluence</b>	<b>Estimated Channel Capacity</b>
25-Year	1672 cfs	1170 cfs	1451 cfs	2621 cfs	650-950 cfs
100-Year	2770 cfs	2270 cfs	2732 cfs	4643 cfs	650-950 cfs

In order to accommodate the 100-year design flows, the Coyote Creek section would need to be increased to 65- to 100-feet wide and 5-feet deep, with 2 to 1 side slopes to form a trapezoidal channel. Figure 6-6 illustrates the proposed Creek cross section (Alternate 1).

Because of the dramatic increase required in the creek's cross section, an alternative was developed that used Hidden Valley Lake to provide flood storage. Hidden Valley Lake has an approximate surface area of 99 acres. Both 3 feet (Alternate 2) and 6 feet (Alternate 3) of storage capacity were analyzed which equates to approximately 289 acre-feet and 594 acre-feet of flood storage. When a hydraulic routing analysis was performed using these flood storage volumes, the outlet flow from Hidden Valley Lake was reduced as indicated in Table 6-3.

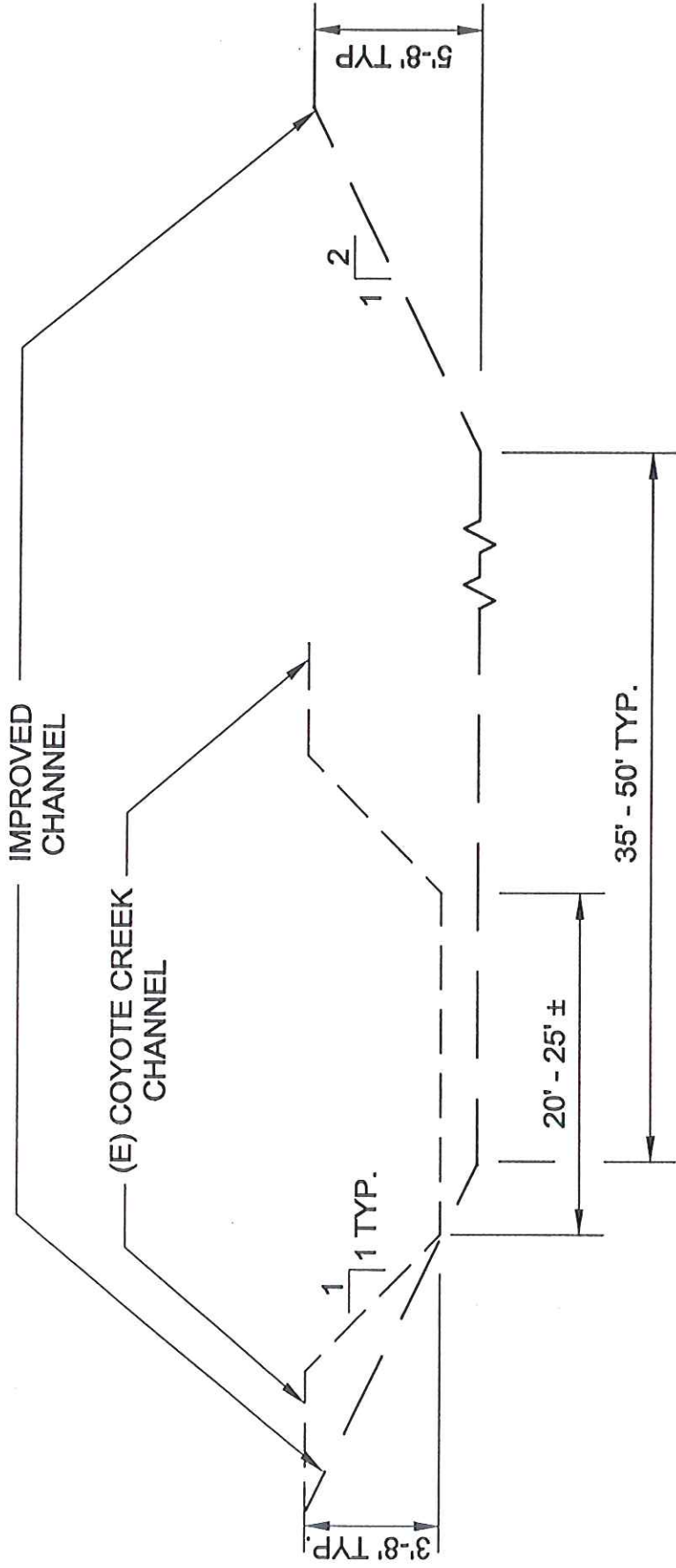
<b>LAKE STORAGE</b>	<b>25-Year Runoff</b>	<b>100-Year Runoff</b>
0' Lake Storage (Alternate 1)	1672 cfs	2770 cfs
3' Lake Storage (Alternate 2)	780 cfs	1200 cfs
6' Lake Storage (Alternate 3)	560 cfs	835 cfs

Alternate 2, assumes 3 feet of storage in Hidden Valley Lake. The downstream improved channel could be reduced to a range of 35 to 50 feet wide; 5 feet deep; with 2:1 side slopes. This cross section is illustrated in Figure 6-7. Alternate 3, assumes 6 feet of storage in Hidden Valley Lake. The existing channel section is generally adequate. It is recommended that the bottom of the channel be graded to get rid of irregularities and deepen the channel in sections where it is



SCALE: 1"=10'

FIGURE 6-6  
ALTERNATE 1  
COYOTE CREEK  
Q100 CHANNEL



SCALE: 1"=10'

FIGURE 6-7  
ALTERNATE 2  
COYOTE CREEK  
Q<sub>100</sub> CHANNEL WITH  
3' LAKE STORAGE



currently less than 4 feet deep. Figure 6-8 shows the general channel configuration utilizing 6 feet of lake storage.

Reconstruction of the channel between its confluence with Putah Creek, upstream to the crossing at Hartman Road where Gallagher Creek enters is necessary. This section requires deepening and widening to reduce the water surface at the Hartman Road crossing. The typical cross section is illustrated in Figure 6-9. This analysis needs to be further refined during the Putah Creek Levee evaluation as it is presently unclear if a less than 100-year Putah Creek water surface elevation can be assumed during the peak Coyote Creek runoff.

#### **B. RECOMMENDATIONS**

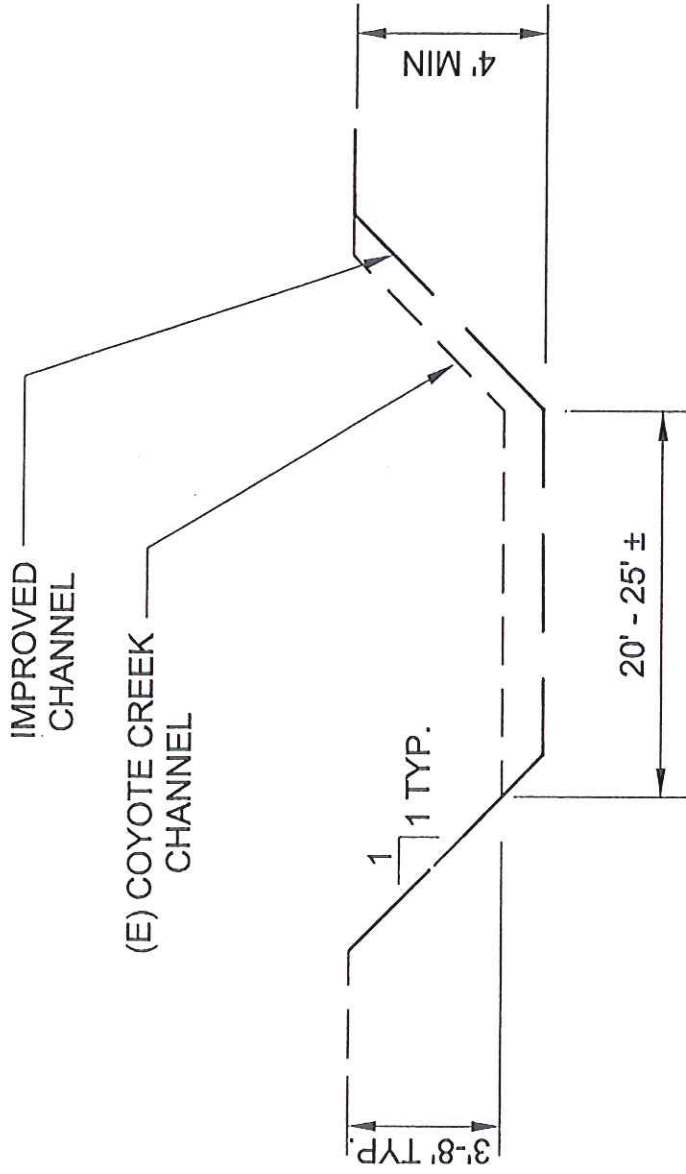
The initial hydraulic modeling for Coyote Creek, utilized creek cross sections prepared by FEMA. Review of these cross sections indicates a high probability that they do not accurately represent the field conditions encountered in the subdivision. Because FEMA's work is quite broad-based, it is likely that they did not have access to the quality of mapping the District has and the creek cross sections may not have been field verified. Prior to developing any detailed design recommendations, it will be important to perform field surveys of the reach of Coyote Creek that is in questions and re-run the HEC-2 models with more precise input data.

Use of the Hidden Valley Lake provides significant attenuation of peak design flows. In order to achieve flood control benefits, it may be necessary to modify the operations of the dam and reservoir. Reservoir levels would need to be drawn down in the fall to provide a "buffer" for flood storage. This type of operation could compromise recreational and aesthetic benefits associated with the Hidden Valley Lake. However, because if the potential cost savings involved, it is important to explore this option.

### **IV. GALLAGHER CREEK CHANNEL**

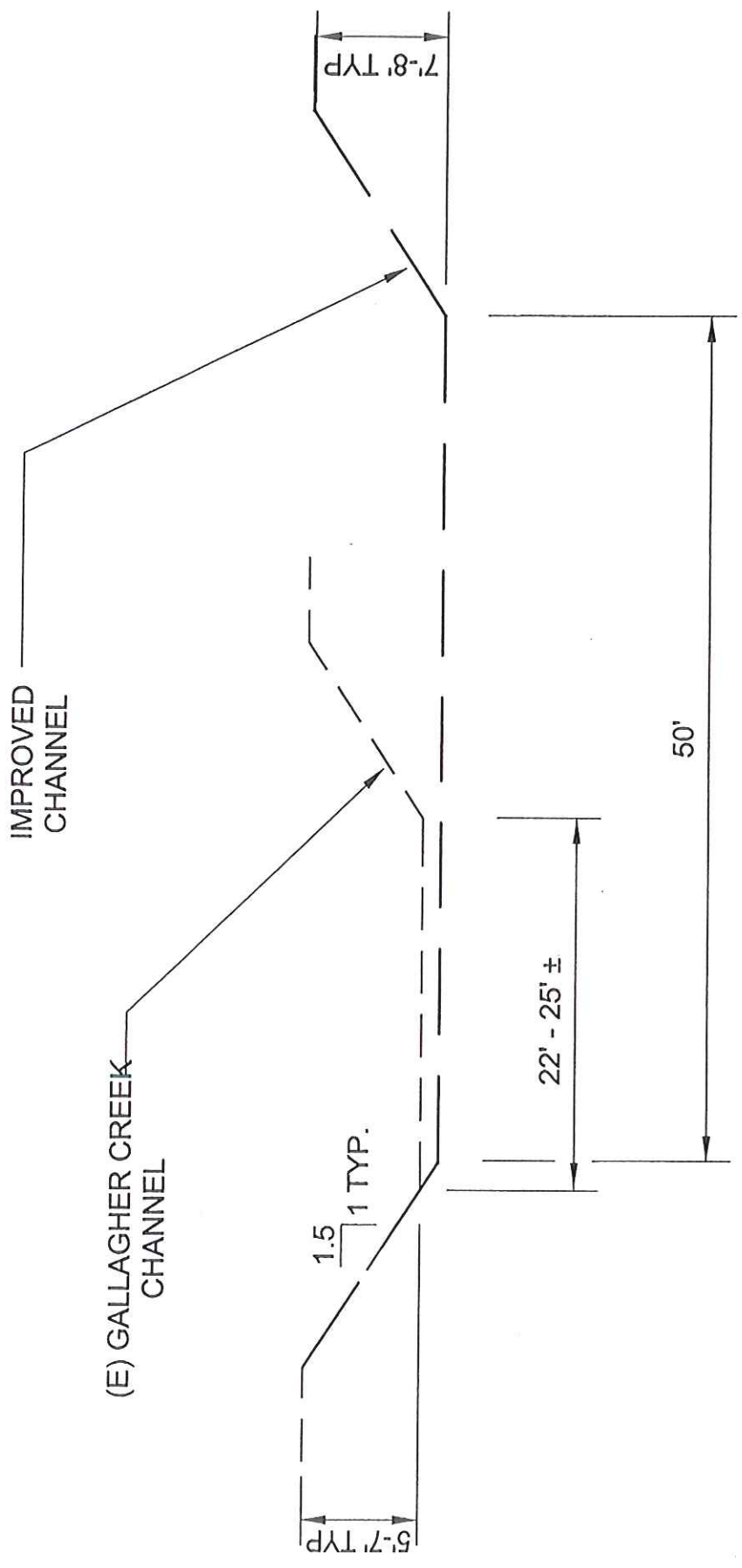
#### **C. ALTERNATIVES REVIEWED**

The hydraulic capacity of the Gallagher Creek channel from its confluence with Coyote Creek upstream approximately 0.5 miles where it diverges away from Hartman Road was reviewed. The FIRM Map indicates substantial flooding through this reach and our analysis confirms this flooding. Section II A of Chapter 6 indicates that the crossings of Mountain Meadow North and Hartman are both significantly undersized. However, upsizing of these drainage facilities will do little to alleviate the flooding of the area. The existing channel is undersized for the estimated 10-



SCALE: 1"=10'

FIGURE 6-8  
ALTERNATE 3  
COYOTE CREEK  
Q<sub>100</sub> CHANNEL WITH  
6' LAKE STORAGE



SCALE: 1"=10'

FIGURE 6-9  
COYOTE CREEK Q<sub>100</sub> CHANNEL  
IMPROVEMENTS DOWNSTREAM  
OF GALLAGHER CREEK  
WINZLER & KELLY  
CONSULTING ENGINEERS

year flows. This channel has relatively low banks on the southeast side of the channel and a relatively wide flood plain. The channel section would need to be substantially widened and deepened in order to contain the 10-year flows and reduce the FEMA flood plain. A typical channel section is indicated on Figure 6-10.

## **V. YEARLY COSTS**

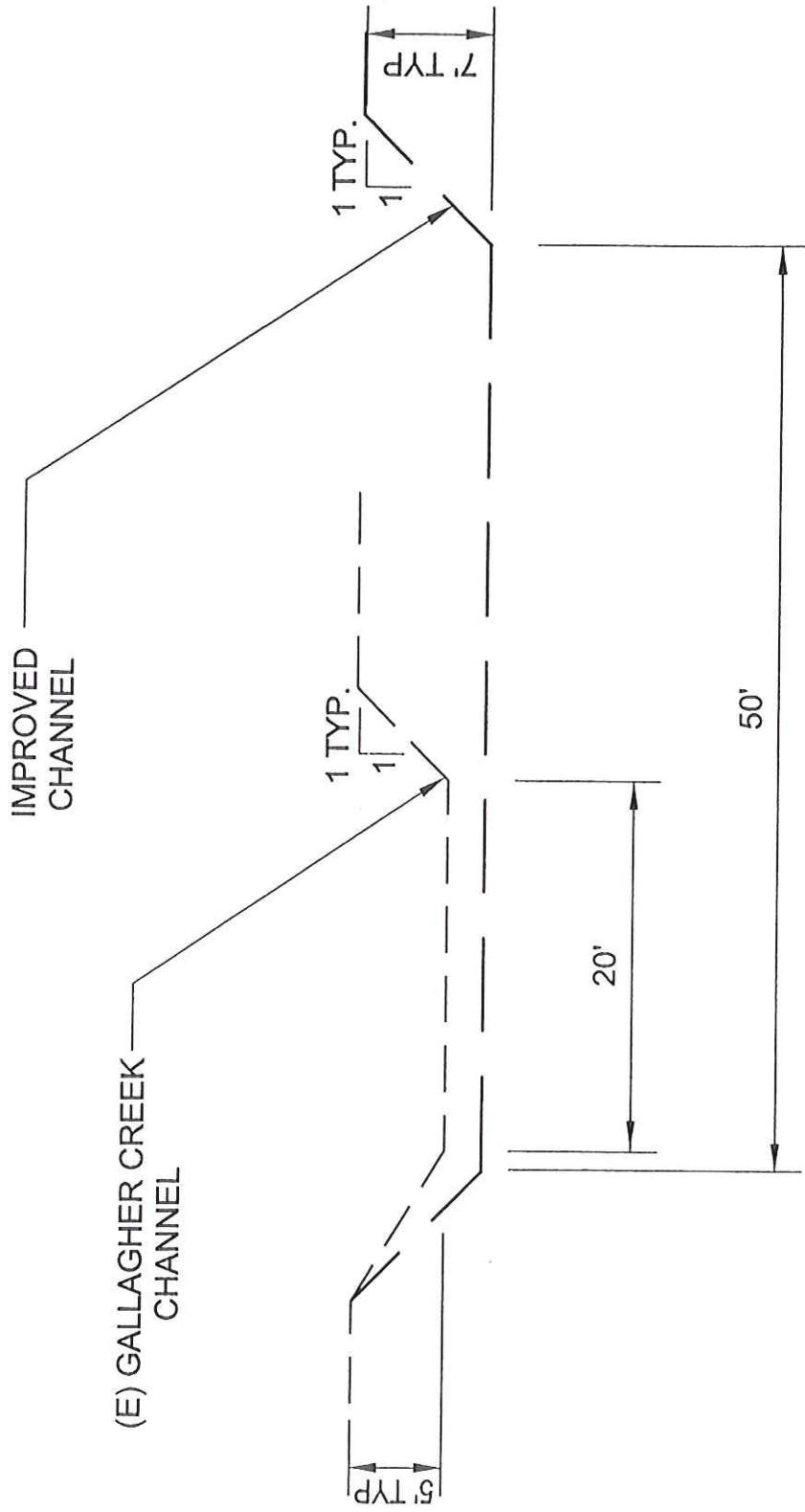
### **A. MAINTENANCE COSTS**

Since the establishment of the subdivision, there has not been a basic yearly maintenance operation established. The typical yearly maintenance operation would consist of cleaning of the ditches, channels, and culverts from debris, vegetation, and silt. Over time, without the yearly maintenance, the long-term effects of sediment buildup and vegetation growth will develop into changes in the flow path of the storm water. The lack of yearly maintenance is primarily due to the ownership of the storm drain system which is divided between three individual agencies: County of Lake, Hidden Valley Lake Homeowners Association, and Hidden Valley Lake Community Services District. As stated earlier in the report, the County of Lake has limited resources, and the entire County is vying for the available dollars. Hidden Valley Lake Homeowners Association has limited resource capacities and these have not been focused on storm drain management. Hidden Valley Lake Community Services District is not authorized to handle storm water management and does not have a current source of funding.

The yearly maintenance cost would generally comprise of workmen, equipment, materials, and administration for implementation.

### **B. IMPROVEMENT COSTS**

The estimated cost for all drainage improvements ranges from \$3,689,770 to \$8,707,110. These drainage improvements would require a number of years to complete. As an example, if these improvements were completed by borrowing money and repaid through a 20-year loan of \$3,689,770 at 5 percent interest, the amortized repayment is \$292,210 per year. The cost of the loan would require additional administration for the loan maintenance.



SCALE: 1"=10'

FIGURE 6-10  
GALLAGHER CREEK Q<sub>100</sub> CHANNEL  
IMPROVEMENTS UPSTREAM  
OF COYOTE CREEK

**C. COST SUMMARY**

The following is a summary of the yearly anticipated costs for Hidden Valley Lake as an example:

Foreman, 2 Operators, 2 Laborers, a Backhoe and Dump Truck for 2 months	\$75,612
Materials	25,000
Administration	35,000
Billing	33,000
Loan Repayment	292,210
<b>Total Estimate Yearly Cost</b>	<b>\$460,822</b>
Estimated Yearly Cost per Lot (3,300 lots)	\$139.64
Monthly Cost per Lot	\$11.64

## CHAPTER 7 - PROJECT FINANCING

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### I. BACKGROUND

Lake County Flood Control and Water Conservation District, is generally financed by a portion of the county property tax. The Lake County Flood Control District encompasses the entire Lake County. The 1999-2000 property tax revenue is estimated to be approximately \$278,300. Since these funds are used throughout the county, all projects within the County vie for a portion of the available funds. The cost of development and implementation of the stormwater and flood control solutions will place an increased and significant financial burden on the County. Therefore, it is difficult to obtain any funds without other influences to have Hidden Valley Lake placed higher priority on the funding.

Financing the storm drainage improvements and maintenance operations will require a well-planned, long-range effort by an agency that has jurisdiction over the drainage conveyance facilities. Multiple ownership of the storm drain conveyance facilities results in difficult funding and project solutions:

- Hidden Valley Lake Association has ownership of the property for the levee on Putah Creek and a portion of the subdivision drainage;
- Lake County, has been dedicated the roads and some subdivision drainage;
- Hidden Valley Lake Community Services District (through merger with Stonehouse Mutual Water District) owns the storm water pump station.

This multiple ownership of these conveyance facilities precludes typical stormwater agency functions necessary to develop and carry out a well-planned, long-range effort to control or eliminate negative stormwater impacts. Single ownership/responsibility will be capable of correcting long-standing flooding and erosion problems.

Over the last few years emergency storm water grants from FEMA, administered by Hidden Valley Lake Community Services District, has repaired and maintained a portion of the drainage conveyance facilities within the subdivision.

A stormwater management program cannot be successful without a consistent, dedicated source of revenue on which it can rely. Hidden Valley area is not much different from many

communities that are grappling with how to fund and administer a new service while trying to upgrade and maintain their already inadequate drainage infrastructure.

In recognition of the need to assess the financial impact of the proposed improvements, an appropriate revenue plan for both construction and operation/maintenance costs is warranted. This report is intended to serve, in part, as a basis for further evaluation and creation of a new stormwater and flood control revenue plan for Hidden Valley Lake.

## **II. ALTERNATIVE STORMWATER REVENUE**

Historically, stormwater management has been financed with general revenues from property taxes, but these taxes have proven to be undependable and inadequate. The best alternative to property-tax-supported general fund stormwater management appears to be a stormwater utility through which service or user charges and related funding mechanisms distribute the costs among owners of properties in proportion to some estimate of the amount of runoff from their properties. Faced with the reduction in tax-based revenue many agencies have identified the need to develop additional revenue sources to supplement general fund obligations, and develop a cost and revenue stream to recover the costs of stormwater management and compliance.

For most agencies, there are basic revenue alternatives available to avoid the continued use of general funds to support stormwater related activities. These alternatives are to establish a benefit assessment or special tax for all county property owners, or to create a new user charge or fee for allocation to the users/beneficiaries of the stormwater program. These mechanisms are discussed in the following sections. Stormwater services can secure increased recognition under both funding systems, rather than having to compete with the more politically powerful police, fire, and other municipal departments for general funds.

### **A. BENEFIT ASSESSMENTS**

Benefit assessments are a common way of funding capital improvements and maintenance activities. In establishing a benefit assessment program, an agency is charged with determining who benefits from the proposed improvements. Assessment proceedings can only be used when properties receive special benefits. Protection from flooding, either as a result of new construction or regular maintenance, is the common benefit for assessments funding flood control and drainage activities.



The State codes provide various Acts by which public agencies may establish and levy assessments, and these designate specifically what types of improvements are allowed to be funded. Flood control facilities can be funded under the Improvement Act of 1911 (the 1911 Act), the Municipal Improvement Act of 1913 (the 1913 Act), and the Benefit Assessment Act of 1982 (the 1982 Act). In addition, many District Acts also provide agencies with the authority to levee assessments.

Assessments formed under the authority of the 1913 Act, the 1982 Act or an agency's own District Act is the most commonly used. The 1913 Act can fund flood control capital improvements, and can fund maintenance only when the 1913 Act is used to construct the improvements. The 1913 Act also allows the use of land-secured bonds to fund the capital improvements. The 1982 Act may fund both capital improvements and maintenance. The 1911 Act can fund both capital improvements and maintenance of flood control facilities, but is seldom used and only on small projects due to its requirement that bonds be sold after the improvements have been constructed.

The assessment process is usually seen as the most attainable funding mechanism available to public agencies because it relies on majority approval (50% or more). For flood control projects, however, the assessment process may not be the most appropriate tool because it concentrates the costs on only the benefiting properties (primarily those being removed from a flood plain). This can result in large costs spread on only a small number of properties.

Some municipal entities, nationally and throughout the State, have used benefit assessments for stormwater management. This method appears to be used throughout California primarily by Special Flood Control Districts where legislation empowered the Districts to levy assessments or taxes upon property to pay specific costs and expenses. For most counties, the use of benefit assessments is dependent upon the legislative enabling acts to authorize the funding of stormwater operational costs and capital expenditures.

#### **B. USER-FEE-FUNDED STORMWATER UTILITIES**

User fees are also a common way of funding capital improvements and maintenance activities. In establishing a user fee program, an agency is required to determine who uses the proposed improvements. In the case of drainage facilities, a user fee allows an agency to collect revenue from properties that contribute runoff into the system but may not flood because of their location.

A user fee can be structured proportionally to the amount each parcel uses the flood control facilities rather than how much each property benefits from the services or improvements provided. This allows program costs to be spread over a larger customer base. For flood control work, user fees are typically related to impervious area on the property, which can be equated to runoff. Like the benefit assessment, a user fee may also be implemented by a 50% vote; however, before the vote may be initiated, a noticed protest hearing must take place and less than 50% written protest must be received. The Proposition 218 voting requirements are new and relatively untested for storm water utilities. Some agency counsel has interpreted the voter pool to be property owners (the user fee is a property-based fee); others are inclined to view the storm drain utility ratepayers as the voter pool. In areas where the storm drain fee is collected with the water and sewer bill and paid by the property resident, this may result in a situation where tenants, rather than the owners, vote.

Funded primarily through service charges user-fee-funded programs provide stable and adequate revenue and equitably distribute the cost of stormwater services and facilities. The concept of a user-fee-funded program or stormwater is not new. The financing is from dedicated user charges, not property taxes. Dedicated user charges means that the charges can only be for stormwater management. Generally these charges are based on the total amount or percentage of run-off (or impervious area) for each parcel of land. This method of calculation of charges requires a change in the thinking of the users: Users are properties that add runoff to a stormwater system; and beneficiaries are properties that gain from the stormwater management.

Stormwater user fees are currently used in many counties throughout the country to fund storm drainage related activities. Although less prevalent in California, State law provides the legal authority to establish a fee for storm drainage services in direct proportion to the beneficiaries of those costs. It is through this general authority that some California counties have established user fees to fund stormwater activity.

Hidden Valley Lake Community Services District currently has water and sewer powers but is not responsible for storm drainage facilities. If the district passed a storm drainage user-fee: based on an estimated 3,300 single-family units within the district, a monthly fee of between \$5 and \$10 per lot would generate \$200,000 to \$400,000 annually assuming that all property owners, both on developed and undeveloped lots paid the fee.

### C. SPECIAL TAXES

As a funding tool, special taxes provide an agency with the most flexibility. There is no benefit or use requirement to satisfy, and the special tax may fund any public improvement or activity the agency undertakes. However, when contemplating a special tax, an agency must obtain a 2/3-voter approval. This is clearly the challenge of a special tax proposal, as a 2/3 approval is very difficult to obtain on even very popular measures.

Another type of special tax is a Mello-Roos Community Facilities District. Although this is sometimes thought of as an assessment district, it is actually a special tax district that allows land-secured bonds. Its establishment procedures can be cumbersome, requiring both a public hearing process and an election process. The Mello-Roos CFD can be a very useful tool for funding development-related capital projects: it provides for a property owner election (rather than a registered voter election) if there are less than 12 registered voters within the district.

Table 7-1 provides a summary of relevant issues for the benefit assessment, user fee and special tax.

Table 7-1 Funding Mechanism Summary					
Funding Mechanism	Hearing Required	Vote Required	Voter Pool	Weighted Votes	Rate Structure
Benefit Assessment	Yes	50%	Property Owners	Yes	Benefit
User Fee	Yes	50%	Property Owners	Yes	Use
Special Tax	No	2/3	Registered Voters	No	Any

### III. BILLING METHODOLOGY

There are three primary methods that could be utilized to accommodate the billing of stormwater fees: utilization of the County Auditor/Controller's Office; utilization of an existing utility billing system or creating a new utility billing system. Each option requires the assessment of County tax roll data for the size and type of land use of each applicable parcel. However, creating a new billing system requires additional data correlation based on parcel address/APN number, as well as additional billing administration and mailing costs.

**A. COUNTY TAX ROLLS**

The County Auditor/Controller's Office provides for the billing of property taxes to all property owners in the County. This system is used as a billing mechanism for taxes and user charges by other municipalities, particularly when the municipality does not have a mechanism to bill charges to the appropriate beneficiaries. The County tax rolls can be used to bill new/special taxes and non-tax (user charges) items.

The advantages of recovering costs through the tax billings are: the percentage of collection is usually very high; as a semi-annual bill, the County should receive minimal customer service calls; the data files are in place; it readily provides for the billing of all property including undeveloped land; and, bills will be sent to property owners without special handling. The disadvantages of this mechanism are: billing costs are relatively high; initial billing errors (estimated at approximately 1% to 2%) may be time consuming and expensive to reconcile; and the County requires a setup fee and annual property tax administrative fee that must be negotiated. To pursue this methodology, the County must adopt the appropriate legal authority and submit the charge per parcel to the County Auditor's Office by the first of August of each year.

**B. UTILIZE AN EXISTING UTILITY BILLING SYSTEM:**

The advantages of using an existing billing system mechanism are: database and billing corrections are all completed by one agency; and cash flow from revenue receipts is continuous. The disadvantages of this methodology are: existing billing schedule would have to be utilized; costs may be incurred for utilizing another agencies billing system; initial number of customers calls/complaints is expected to exceed the calls from the tax mechanism; a special utility bill would be required to bill owners of undeveloped land.

**C. CREATE A NEW BILLING SYSTEM**

The advantages of using a new billing system mechanism are: it provides a flexible implementation schedule; data base adjustments and billing corrections are all completed by one agency; and, cash flow from revenue receipts is continuous. The disadvantages of this methodology are: the billing system must be created; utility accounts billed directly to rental property tenants may require reconciliation to accommodate a special bill to property owners; initial number of customers calls/complaints is expected to exceed the calls from the tax mechanism; and, a special utility bill is required to bill owners of undeveloped land.

#### **IV. RECOMMENDATIONS**

Without clear ownership/responsibilities of the stormwater conveyance facilities within Hidden Valley Lake, a stormwater management program cannot be successfully implemented. A number of factors emerge from the review of the material:

- Determine the authority to implement and manage the storm water facilities for Hidden Valley Lake.
- Grants and funding from FEMA and other government agencies generally require a government entity for administering the funds.
- A defined tax base must be established to dedicate funds for operation/maintenance and implementation of the recommendations.
- A user-fee approach appears to be best suited for Hidden Valley Lake.

## APPENDIX A - HEC OUTPUT FILES

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   MAY 1991 *
*   VERSION 4.0.1E *
* RUN DATE 07/21/1999 TIME 10:19:47 *
*****
```

```
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
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X X XXXXXXX XXXX X
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XXXXXXX XXXX X XXXXX X
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```
*****
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
::: :::
*****
```

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subasin 1 - 10 Year Storm									
2	IT	1	1440								
3	IO	5	0								
4	KK	0406									
5	KM	SCS 24 Hour Type IA Rainfall HVLSWMP Node 1.04.06									
6	KO	22									
7	BA	.3602									
8	PB	6									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184

K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT

ISAV2           1440   LAST ORDINATE PUNCHED OR SAVED  
TIMINT         0.017   TIME INTERVAL IN HOURS

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\*           \*  
1668 KK     \*     0101   \*  
\*           \*  
\*\*\*\*\*

1670 KO       OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1440	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.017	TIME INTERVAL IN HOURS

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\*           \*  
1701 KK     \*     1.01   \*  
\*           \*  
\*\*\*\*\*

1703 KO       OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1440	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.017	TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD		BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
24-HOUR	72-HOUR		6-HOUR					
HYDROGRAPH AT								
0406	130.	8.10	51.	26.	26.	0.36		
ROUTED TO								
R406	130.	8.12	51.	26.	26.	0.36		
HYDROGRAPH AT								
0405	3.	8.02	1.	1.	1.	0.01		
2 COMBINED AT								
P405	133.	8.10	52.	27.	27.	0.37		
ROUTED TO								
R405	132.	8.12	52.	27.	27.	0.37		
HYDROGRAPH AT								
040401	3.	8.00	1.	1.	1.	0.01		
ROUTED TO								
R40401	3.	8.02	1.	1.	1.	0.01		
HYDROGRAPH AT								
040402	4.	8.00	1.	1.	1.	0.01		
ROUTED TO								
R40402	4.	8.02	1.	1.	1.	0.01		
HYDROGRAPH AT								
0404	5.	8.02	2.	1.	1.	0.01		
4 COMBINED AT								
P404	143.	8.10	56.	29.	29.	0.39		



K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT

ROUTED TO R404	143.	8.18	56.	29.	29.	0.39
HYDROGRAPH AT 040302	27.	8.02	10.	5.	5.	0.06
ROUTED TO 40302	27.	8.13	10.	5.	5.	0.06
HYDROGRAPH AT 0403	33.	8.10	13.	7.	7.	0.08
HYDROGRAPH AT 040301	4.	8.07	1.	1.	1.	0.01
4 COMBINED AT P403	205.	8.17	80.	41.	41.	0.55
ROUTED TO R403	204.	8.23	80.	41.	41.	0.55
HYDROGRAPH AT 040206	4.	7.95	1.	1.	1.	0.01
ROUTED TO R40206	4.	8.20	1.	1.	1.	0.01
HYDROGRAPH AT 040205	16.	8.17	6.	3.	3.	0.03
HYDROGRAPH AT 420502	0.	0.02	0.	0.	0.	0.01
HYDROGRAPH AT 420501	1.	8.00	0.	0.	0.	0.00
4 COMBINED AT P40205	21.	8.17	8.	4.	4.	0.04
ROUTED TO R40205	14.	8.68	8.	4.	4.	0.04
HYDROGRAPH AT 420401	3.	7.95	1.	0.	0.	0.00
ROUTED TO R42401	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 420402	11.	7.97	3.	2.	2.	0.02
ROUTED TO R42402	11.	8.02	3.	2.	2.	0.02
HYDROGRAPH AT 420403	7.	7.98	2.	1.	1.	0.01
ROUTED TO R42402	7.	8.05	2.	1.	1.	0.01
HYDROGRAPH AT 040204	30.	7.95	10.	5.	5.	0.04
4 COMBINED AT P40204	51.	7.98	17.	8.	8.	0.08
ROUTED TO R40204	50.	8.10	17.	8.	8.	0.08
HYDROGRAPH AT 040202	1.	8.00	1.	0.	0.	0.00
ROUTED TO R40202	1.	8.12	1.	0.	0.	0.00
HYDROGRAPH AT 040201	8.	8.12	3.	1.	1.	0.02
ROUTED TO R40201	8.	8.25	3.	1.	1.	0.02
HYDROGRAPH AT 040203	5.	8.07	2.	1.	1.	0.01
ROUTED TO R40203	5.	8.20	2.	1.	1.	0.01
HYDROGRAPH AT 0402	16.	8.42	7.	4.	4.	0.04
7 COMBINED AT P402	289.	8.22	117.	59.	59.	0.74
ROUTED TO						

R402	288.	8.23	116.	59.	59.	0.74
HYDROGRAPH AT 410201	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 040102	9.	8.00	3.	2.	2.	0.02
2 COMBINED AT P40102	14.	8.00	5.	2.	2.	0.03
ROUTED TO R40102	14.	8.07	5.	2.	2.	0.03
HYDROGRAPH AT 040101	2.	8.00	1.	0.	0.	0.00
ROUTED TO R40101	2.	8.03	1.	0.	0.	0.00

K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT

HYDROGRAPH AT 0401	8.	8.07	3.	1.	1.	0.02
4 COMBINED AT P0401	308.	8.22	125.	63.	63.	0.78
ROUTED TO R0401	308.	8.22	125.	63.	63.	0.78
HYDROGRAPH AT 0802	0.	7.97	0.	0.	0.	0.00
ROUTED TO R0802	0.	8.10	0.	0.	0.	0.00
HYDROGRAPH AT 0801	1.	7.98	0.	0.	0.	0.00
2 COMBINED AT P0801	2.	8.02	1.	0.	0.	0.00
ROUTED TO R0801	2.	8.23	1.	0.	0.	0.00
HYDROGRAPH AT 0800	2.	8.07	1.	0.	0.	0.00
2 COMBINED AT 1.08	3.	8.12	1.	1.	1.	0.01
ROUTED TO R08	3.	8.32	1.	1.	1.	0.01
HYDROGRAPH AT 0702	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0702	2.	8.08	1.	0.	0.	0.00
HYDROGRAPH AT 0701	2.	8.02	1.	0.	0.	0.00
2 COMBINED AT P0701	4.	8.05	1.	1.	1.	0.01
ROUTED TO R0701	4.	8.08	1.	1.	1.	0.01
HYDROGRAPH AT 0700	6.	8.02	2.	1.	1.	0.01
3 COMBINED AT 1.07	12.	8.08	5.	2.	2.	0.03
ROUTED TO R07	12.	8.18	5.	2.	2.	0.03
HYDROGRAPH AT 0602	3.	8.03	1.	1.	1.	0.01
ROUTED TO R0602	3.	8.13	1.	1.	1.	0.01
HYDROGRAPH AT 060101	6.	8.37	3.	1.	1.	0.01
ROUTED TO R60101	6.	8.42	3.	1.	1.	0.01
HYDROGRAPH AT 0601	4.	8.05	1.	1.	1.	0.01
3 COMBINED AT P0601	11.	8.17	5.	3.	3.	0.03
ROUTED TO R0604	11.	8.23	5.	3.	3.	0.03
HYDROGRAPH AT 0600	3.	8.00	1.	0.	0.	0.01
3 COMBINED AT 1.06	25.	8.18	11.	5.	5.	0.06
ROUTED TO R06	25.	8.20	11.	5.	5.	0.06
HYDROGRAPH AT 0501	3.	8.00	1.	1.	1.	0.01
ROUTED TO R0501	3.	8.05	1.	1.	1.	0.01
HYDROGRAPH AT						

0500	3.	8.00	1.	1.	1.	0.01
3 COMBINED AT 1.05	30.	8.13	13.	7.	7.	0.07
ROUTED TO R05	30.	8.18	13.	6.	6.	0.07
HYDROGRAPH AT 0400	2.	7.97	1.	0.	0.	0.00
3 COMBINED AT 1.04	339.	8.22	138.	70.	70.	0.86
ROUTED TO R04	339.	8.23	138.	70.	70.	0.86
HYDROGRAPH AT 0303	1.	8.02	0.	0.	0.	0.00

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ROUTED TO R0303	1.	8.07	0.	0.	0.	0.00
HYDROGRAPH AT 0302	4.	8.00	1.	1.	1.	0.01
2 COMBINED AT P0302	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0302	5.	8.05	2.	1.	1.	0.01
HYDROGRAPH AT 0301	2.	8.05	1.	0.	0.	0.00
2 COMBINED AT P0301	7.	8.05	3.	1.	1.	0.01
ROUTED TO R0301	7.	8.07	3.	1.	1.	0.01
HYDROGRAPH AT 0300	1.	8.00	0.	0.	0.	0.00
3 COMBINED AT 1.03	345.	8.23	141.	71.	71.	0.88
ROUTED TO R03	344.	8.27	141.	71.	71.	0.88
HYDROGRAPH AT 0201	2.	8.02	1.	0.	0.	0.00
ROUTED TO R0201	2.	8.05	1.	0.	0.	0.00
HYDROGRAPH AT 010201	1.	8.02	0.	0.	0.	0.00
3 COMBINED AT 1.02	346.	8.27	142.	72.	72.	0.89
ROUTED TO R02	346.	8.30	142.	71.	71.	0.89
HYDROGRAPH AT 010203	21.	8.00	7.	4.	4.	0.04
ROUTED TO R10203	21.	8.03	7.	4.	4.	0.04
HYDROGRAPH AT 010202	1.	8.00	0.	0.	0.	0.00
ROUTED TO R10202	1.	8.03	0.	0.	0.	0.00
HYDROGRAPH AT 010201	1.	8.02	0.	0.	0.	0.00
ROUTED TO R10201	1.	8.03	0.	0.	0.	0.00
HYDROGRAPH AT 0102	7.	8.07	3.	1.	1.	0.02
4 COMBINED AT P0102	31.	8.05	11.	5.	5.	0.06
ROUTED TO R0102	31.	8.05	11.	5.	5.	0.06
HYDROGRAPH AT 0101	2.	8.00	1.	0.	0.	0.00
3 COMBINED AT 1.01	368.	8.28	154.	77.	77.	

0.95

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R406	MANE	0.50	129.84	486.87	2.69	1.00	129.82	487.00	2.69

R405 MANE 0.35 132.51 486.65 2.69 1.00 132.48 487.00 2.69

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5293E+02 EXCESS=0.0000E+00 OUTFLOW=0.5291E+02 BASIN STORAGE=0.2129E-01 PERCENT ERROR= 0.0

R40401 MANE 1.00 2.99 481.00 3.27 1.00 2.99 481.00 3.27

HEC1 S/N: 1343001909

HMVersion: 6.33 K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT  
Data File: C:\WINDOWS\TEMP\vbh203A.TMP

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\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* MAY 1991 \*  
\* VERSION 4.0.1E \*  
\* RUN DATE 07/21/1999 TIME 10:28:28 \*  
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\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
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::::::::::::::::::::::::::::::::::::
:: Full Microcomputer Implementation ::
:: by ::
:: Haestad Methods, Inc. ::
:: ::
::::::::::::::::::::::::::::::::::::
```

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

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THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID HVL SWMP - Subasin 1 - 100 Year Storm
2	IT 1 1440
3	IO 5 0
4	KK 0406
5	KM SCS 24 Hour Type IA Rainfall HVLSWMP Node 1.04.06
6	KO 22
7	BA .3602
8	PB 9.5
9	IN 6
10	PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776
11	PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695
12	PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880
13	PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229
14	PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159
15	PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049
16	PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127
17	PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.33142 0.35469 0.37876 0.40255
18	PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296
19	PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184

ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

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 \* \*  
 1668 KK \* 0101 \*  
 \* \*  
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1670 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

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 \* \*  
 1701 KK \* 1.01 \*  
 \* \*  
 \*\*\*\*\*

1703 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
24-HOUR	72-HOUR								
HYDROGRAPH AT									
0406	301.	8.08	109.	54.	54.	0.36			
ROUTED TO									
R406	301.	8.08	109.	54.	54.	0.36			
HYDROGRAPH AT									
0405	7.	7.98	2.	1.	1.	0.01			
2 COMBINED AT									
P405	308.	8.08	111.	56.	56.	0.37			
ROUTED TO									
R405	308.	8.08	111.	56.	56.	0.37			
HYDROGRAPH AT									
040401	6.	7.97	2.	1.	1.	0.01			
ROUTED TO									
R40401	6.	7.98	2.	1.	1.	0.01			
HYDROGRAPH AT									
040402	8.	7.97	3.	1.	1.	0.01			
ROUTED TO									
R40402	8.	7.98	3.	1.	1.	0.01			
HYDROGRAPH AT									
0404	11.	7.98	4.	2.	2.	0.01			
4 COMBINED AT									
P404	331.	8.08	119.	60.	60.	0.39			



K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT

ROUTED TO R404	331.	8.15	119.	59.	59.	0.39
HYDROGRAPH AT 040302	60.	8.00	20.	10.	10.	0.06
ROUTED TO 40302	60.	8.08	20.	10.	10.	0.06
HYDROGRAPH AT 0403	75.	8.08	27.	13.	13.	0.08
HYDROGRAPH AT 040301	8.	8.05	3.	1.	1.	0.01
4 COMBINED AT P403	471.	8.13	169.	84.	84.	0.55
ROUTED TO R403	469.	8.18	169.	84.	84.	0.55
HYDROGRAPH AT 040206	7.	7.93	2.	1.	1.	0.01
ROUTED TO R40206	7.	8.15	2.	1.	1.	0.01
HYDROGRAPH AT 040205	32.	8.15	12.	6.	6.	0.03
HYDROGRAPH AT 420502	0.	0.02	0.	0.	0.	0.01
HYDROGRAPH AT 420501	1.	7.95	0.	0.	0.	0.00
4 COMBINED AT P40205	40.	8.13	15.	7.	7.	0.04
ROUTED TO R40205	28.	8.43	14.	7.	7.	0.04
HYDROGRAPH AT 420401	5.	7.93	2.	1.	1.	0.00
ROUTED TO R42401	5.	7.98	2.	1.	1.	0.00
HYDROGRAPH AT 420402	20.	7.95	6.	3.	3.	0.02
ROUTED TO R42402	20.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 420403	14.	7.95	4.	2.	2.	0.01
ROUTED TO R42402	14.	8.02	4.	2.	2.	0.01
HYDROGRAPH AT 040204	55.	7.93	18.	9.	9.	0.04
4 COMBINED AT P40204	93.	7.97	30.	15.	15.	0.08
ROUTED TO R40204	93.	8.07	30.	15.	15.	0.08
HYDROGRAPH AT 040202	3.	7.95	1.	0.	0.	0.00
ROUTED TO R40202	3.	8.08	1.	0.	0.	0.00
HYDROGRAPH AT 040201	16.	8.10	6.	3.	3.	0.02
ROUTED TO R40201	16.	8.22	6.	3.	3.	0.02
HYDROGRAPH AT 040203	11.	8.05	4.	2.	2.	0.01
ROUTED TO R40203	11.	8.17	4.	2.	2.	0.01
HYDROGRAPH AT 0402	32.	8.40	14.	7.	7.	0.04
7 COMBINED AT P402	638.	8.17	237.	118.	118.	0.74
ROUTED TO						

R402	636.	8.18	237.	118.	118.	0.74
HYDROGRAPH AT 410201	11.	7.97	4.	2.	2.	0.01
HYDROGRAPH AT 040102	18.	7.97	6.	3.	3.	0.02
2 COMBINED AT P40102	29.	7.97	9.	5.	5.	0.03
ROUTED TO R40102	29.	8.03	9.	5.	5.	0.03
HYDROGRAPH AT 040101	4.	7.97	1.	1.	1.	0.00
ROUTED TO R40101	4.	8.00	1.	1.	1.	0.00

K:\RICKJ\HECPACK\GHEC1\99205301\AREAL\1-00.OUT

HYDROGRAPH AT 0401	16.	8.07	6.	3.	3.	0.02
4 COMBINED AT P0401	679.	8.17	253.	126.	126.	0.78
ROUTED TO R0401	678.	8.17	253.	126.	126.	0.78
HYDROGRAPH AT 0802	1.	7.95	0.	0.	0.	0.00
ROUTED TO R0802	1.	8.07	0.	0.	0.	0.00
HYDROGRAPH AT 0801	3.	7.95	1.	0.	0.	0.00
2 COMBINED AT P0801	3.	7.98	1.	1.	1.	0.00
ROUTED TO R0801	3.	8.17	1.	1.	1.	0.00
HYDROGRAPH AT 0800	4.	8.05	2.	1.	1.	0.00
2 COMBINED AT 1.08	7.	8.08	3.	1.	1.	0.01
ROUTED TO R08	7.	8.23	3.	1.	1.	0.01
HYDROGRAPH AT 0702	3.	7.95	1.	1.	1.	0.00
ROUTED TO R0702	3.	8.05	1.	1.	1.	0.00
HYDROGRAPH AT 0701	5.	8.02	2.	1.	1.	0.00
2 COMBINED AT P0701	8.	8.02	3.	1.	1.	0.01
ROUTED TO R0701	8.	8.05	3.	1.	1.	0.01
HYDROGRAPH AT 0700	12.	8.02	4.	2.	2.	0.01
3 COMBINED AT 1.07	26.	8.07	9.	5.	5.	0.03
ROUTED TO R07	26.	8.15	9.	5.	5.	0.03
HYDROGRAPH AT 0602	6.	8.02	2.	1.	1.	0.01
ROUTED TO R0602	6.	8.10	2.	1.	1.	0.01
HYDROGRAPH AT 060101	12.	8.35	5.	3.	3.	0.01
ROUTED TO R60101	12.	8.38	5.	3.	3.	0.01
HYDROGRAPH AT 0601	8.	8.03	3.	1.	1.	0.01
3 COMBINED AT P0601	24.	8.15	10.	5.	5.	0.03
ROUTED TO R0604	24.	8.20	10.	5.	5.	0.03
HYDROGRAPH AT 0600	5.	7.97	2.	1.	1.	0.01
3 COMBINED AT 1.06	53.	8.15	21.	10.	10.	0.06
ROUTED TO R06	53.	8.15	21.	10.	10.	0.06
HYDROGRAPH AT 0501	7.	7.98	2.	1.	1.	0.01
ROUTED TO R0501	7.	8.02	2.	1.	1.	0.01
HYDROGRAPH AT						

0500	7.	7.97	2.	1.	1.	0.01
3 COMBINED AT 1.05	65.	8.10	26.	13.	13.	0.07
ROUTED TO R05	65.	8.13	26.	13.	13.	0.07
HYDROGRAPH AT 0400	4.	7.95	1.	1.	1.	0.00
3 COMBINED AT 1.04	746.	8.17	280.	139.	139.	0.86
ROUTED TO R04	745.	8.18	280.	139.	139.	0.86
HYDROGRAPH AT 0303	3.	8.00	1.	0.	0.	0.00

K:\RICKJ\HECPACK\GHEC1\99205301\AREA1\1-00.OUT

ROUTED TO R0303	3.	8.03	1.	0.	0.	0.00
HYDROGRAPH AT 0302	8.	7.97	3.	1.	1.	0.01
2 COMBINED AT P0302	11.	7.98	4.	2.	2.	0.01
ROUTED TO R0302	11.	8.02	4.	2.	2.	0.01
HYDROGRAPH AT 0301	4.	8.03	1.	1.	1.	0.00
2 COMBINED AT P0301	15.	8.02	5.	3.	3.	0.01
ROUTED TO R0301	15.	8.05	5.	3.	3.	0.01
HYDROGRAPH AT 0300	3.	7.95	1.	0.	0.	0.00
3 COMBINED AT 1.03	760.	8.18	286.	142.	142.	0.88
ROUTED TO R03	758.	8.22	286.	142.	142.	0.88
HYDROGRAPH AT 0201	3.	8.00	1.	1.	1.	0.00
ROUTED TO R0201	3.	8.02	1.	1.	1.	0.00
HYDROGRAPH AT 010201	3.	8.00	1.	0.	0.	0.00
3 COMBINED AT 1.02	763.	8.22	288.	143.	143.	0.89
ROUTED TO R02	763.	8.22	288.	143.	143.	0.89
HYDROGRAPH AT 010203	44.	7.97	14.	7.	7.	0.04
ROUTED TO R10203	44.	8.00	14.	7.	7.	0.04
HYDROGRAPH AT 010202	3.	7.95	1.	0.	0.	0.00
ROUTED TO R10202	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 010201	3.	8.00	1.	0.	0.	0.00
ROUTED TO R10201	3.	8.02	1.	0.	0.	0.00
HYDROGRAPH AT 0102	15.	8.05	5.	3.	3.	0.02
4 COMBINED AT P0102	64.	8.02	21.	11.	11.	0.06
ROUTED TO R0102	64.	8.03	21.	11.	11.	0.06
HYDROGRAPH AT 0101	3.	7.95	1.	1.	1.	0.00
3 COMBINED AT 1.01	813.	8.20	311.	154.	154.	

0.95

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R406	MANE	0.38	301.37	485.47	5.61	1.00	301.24	485.00	5.62

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA1\1-09.OUT  
Data File: C:\WINDOWS\TEMP\vbh0E27.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   MAY 1991 *
*   VERSION 4.0.1E *
* RUN DATE 08/14/1999 TIME 07:13:22 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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:::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
1	ID	HVL SWMP Node 1.09 10 Year Storm									
2	IT	1	1440								
3	IO	5	0								
4	KK	0901									
5	KM	SCS 24 Hour Type IA Rainfall HVL SWMP Node 1.09.01 10 Year Storm									
6	KO	22									
7	BA	0.0131									
8	PB	6									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026

```
*****
*
* 41 KK      * 0900 *
*
* *****
```

```
43 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      0  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
            IPNCH      0  PUNCH COMPUTED HYDROGRAPH
            IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
            ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
            ISAV2     1440  LAST ORDINATE PUNCHED OR SAVED
            TIMINT     0.017  TIME INTERVAL IN HOURS
```

\*\*\*\*\*

```
*****
*
* 74 KK      * 1.09 *
*
* *****
```

```
76 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      0  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
            IPNCH      0  PUNCH COMPUTED HYDROGRAPH
            IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
            ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
            ISAV2     1440  LAST ORDINATE PUNCHED OR SAVED
            TIMINT     0.017  TIME INTERVAL IN HOURS
```

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT									
0901	7.	8.00	2.	1.	1.	0.01			
ROUTED TO									
R0901	7.	8.02	2.	1.	1.	0.01			
HYDROGRAPH AT									
0900	9.	8.00	3.	2.	2.	0.02			
2 COMBINED AT									
1.09	15.	8.02	5.	3.	3.	0.03			

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0901	MANE	1.00	6.62	482.00	3.26	1.00	6.62	482.00	3.26

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2285E+01 EXCESS=0.0000E+00 OUTFLOW=0.2280E+01 BASIN STORAGE=0.5249E-02 PERCENT ERROR= 0.0

\*\*\* NORMAL END OF HEC-1 \*\*\*

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA1\1-09.OUT  
Data File: C:\WINDOWS\TEMP\vbh2534.TMP

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 08/14/1999 TIME 07:15:39 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID HVL SWMP Node 1.09 100 Year Storm
2 IT 1 1440
3 IO 5 0
4 KK 0901
5 KM SCS 24 Hour Type IA Rainfall HVLSWMP Node 1.09.01 100 Year Storm
6 KO 22
7 BA 0.0131
8 PB 9.5
9 IN 6
10 PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776
11 PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695
12 PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880
13 PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229
14 PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159
15 PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049
16 PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127
17 PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.33142 0.35469 0.37876 0.40255
18 PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296
19 PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184
20 PC 0.5770 0.58198 0.58685 0.59163 0.59635 0.60100 0.60576 0.61044 0.61504 0.61956
21 PC 0.6240 0.62836 0.63264 0.63684 0.64096 0.64500 0.64889 0.65272 0.65651 0.66026

```



```
*****
*
* 41 KK      0900
*
*****
```

```
43 KO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL     0.  HYDROGRAPH PLOT SCALE
          IPNCH     0  PUNCH COMPUTED HYDROGRAPH
          IOUT      22  SAVE HYDROGRAPH ON THIS UNIT
          ISAV1     1  FIRST ORDINATE PUNCHED OR SAVED
          ISAV2    1440  LAST ORDINATE PUNCHED OR SAVED
          TIMINT    0.017  TIME INTERVAL IN HOURS
```

\*\*\*\*\*

```
*****
*
* 74 KK      1.09
*
*****
```

```
76 KO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL     0.  HYDROGRAPH PLOT SCALE
          IPNCH     0  PUNCH COMPUTED HYDROGRAPH
          IOUT      22  SAVE HYDROGRAPH ON THIS UNIT
          ISAV1     1  FIRST ORDINATE PUNCHED OR SAVED
          ISAV2    1440  LAST ORDINATE PUNCHED OR SAVED
          TIMINT    0.017  TIME INTERVAL IN HOURS
```

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT									
0901	14.	7.97	4.	2.	2.	0.01			
ROUTED TO									
R0901	14.	7.98	4.	2.	2.	0.01			
HYDROGRAPH AT									
0900	19.	7.97	6.	3.	3.	0.02			
2 COMBINED AT									
1.09	32.	7.98	11.	5.	5.	0.03			

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		
							PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0901	MANE	1.00	13.68	479.00	6.38	1.00	13.68	479.00	6.38

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4456E+01 EXCESS=0.0000E+00 OUTFLOW=0.4459E+01 BASIN STORAGE=0.7869E-02 PERCENT ERROR= 0.0

\*\*\* NORMAL END OF HEC-1 \*\*\*

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA2\2-00.OUT  
Data File: C:\WINDOWS\TEMP\vbh0D08.TMP

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 07/27/1999 TIME 12:09:05 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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::::::::::::::::::::::::::::::::::::
:: Full Microcomputer Implementation ::
:: by ::
:: Haestad Methods, Inc. ::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

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 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subbasin 2 - 10 Year Storm									
2	IT	1			1440						
3	IO	5	0								
4	KK	021222									
5	KM	SCS 24 Hour Type IA Rainfall Subbasin 2.02.01.02.02.02									
6	KO					22					
7	BA	.0255									
8	PB	6									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184

\*\*\* \*\*

```
*****
*
800 KK *   R01   *
*           *
*****
```

```
802 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      0  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
            IPNCH      0  PUNCH COMPUTED HYDROGRAPH
            IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
            ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
            ISAV2     1440  LAST ORDINATE PUNCHED OR SAVED
            TIMINT     0.017  TIME INTERVAL IN HOURS
```

\*\*\* \*\*

```
*****
*
804 KK *   2.0   *
*           *
*****
```

```
806 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      0  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
            IPNCH      0  PUNCH COMPUTED HYDROGRAPH
            IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
            ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
            ISAV2     1440  LAST ORDINATE PUNCHED OR SAVED
            TIMINT     0.017  TIME INTERVAL IN HOURS
```

\*\*\* WARNING \*\*\* UNIT HYDROGRAPH TRUNCATED FROM 369 TO 300 INTERVALS

\*\*\* \*\*

```
*****
*
837 KK *   2.0   *
*           *
*****
```

```
839 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      0  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
            IPNCH      0  PUNCH COMPUTED HYDROGRAPH
            IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
            ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
            ISAV2     1440  LAST ORDINATE PUNCHED OR SAVED
            TIMINT     0.017  TIME INTERVAL IN HOURS
```

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
24-HOUR	72-HOUR						
HYDROGRAPH AT							
021222	17.	7.97	6.	3.	3.	0.03	

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ROUTED TO R21222	17.	7.97	6.	3.	3.	0.03
HYDROGRAPH AT 021221	0.	7.92	0.	0.	0.	0.00
2 COMBINED AT 021221	17.	7.97	6.	3.	3.	0.03
ROUTED TO R21221	17.	7.97	6.	3.	3.	0.03
HYDROGRAPH AT 02123	10.	7.95	3.	2.	2.	0.01
ROUTED TO R02123	10.	7.95	3.	2.	2.	0.01
HYDROGRAPH AT 02122	1.	7.95	0.	0.	0.	0.00
3 COMBINED AT 02122p	28.	7.97	9.	5.	5.	0.04
ROUTED TO R02122	28.	7.97	9.	5.	5.	0.04
HYDROGRAPH AT 02121	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 02121p	29.	7.97	10.	5.	5.	0.04
ROUTED TO R02121	29.	7.98	10.	5.	5.	0.04
HYDROGRAPH AT 0215	2.	7.95	1.	0.	0.	0.00
ROUTED TO R0215	2.	7.95	1.	0.	0.	0.00
HYDROGRAPH AT 020104	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 0214p	3.	7.95	1.	0.	0.	0.00
ROUTED TO R0214	3.	7.98	1.	0.	0.	0.00
HYDROGRAPH AT 0213	9.	7.95	3.	1.	1.	0.01
2 COMBINED AT 0213p	12.	7.97	4.	2.	2.	0.02
ROUTED TO R0213	12.	7.98	4.	2.	2.	0.02
HYDROGRAPH AT 0212	5.	7.95	2.	1.	1.	0.01
3 COMBINED AT 0212p	47.	7.98	15.	8.	8.	0.07
ROUTED TO R0212	47.	7.98	15.	8.	8.	0.07
HYDROGRAPH AT 0211	6.	7.97	2.	1.	1.	0.01
2 COMBINED AT 0211p	53.	7.98	17.	9.	9.	0.08
ROUTED TO R0211	53.	8.02	17.	9.	9.	0.08
HYDROGRAPH AT 0225	11.	8.10	4.	2.	2.	0.02
ROUTED TO R0225	11.	8.12	4.	2.	2.	0.02
HYDROGRAPH AT 0224	3.	8.00	1.	0.	0.	0.01
2 COMBINED AT 0224p	13.	8.07	5.	2.	2.	0.03
ROUTED TO R0224	13.	8.10	5.	2.	2.	0.03
HYDROGRAPH AT						

0223	1.	8.00	0.	0.	0.	0.00
2 COMBINED AT 0223p	14.	8.08	5.	3.	3.	0.03
ROUTED TO R0223	14.	8.08	5.	3.	3.	0.03
HYDROGRAPH AT 0222	1.	7.98	0.	0.	0.	0.00
2 COMBINED AT 0222p	15.	8.08	6.	3.	3.	0.03
ROUTED TO R0222	15.	8.28	6.	3.	3.	0.03
HYDROGRAPH AT 0221	10.	8.22	4.	2.	2.	0.02

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2 COMBINED AT 0221p	25.	8.27	10.	5.	5.	0.06
ROUTED TO R0221	25.	8.28	10.	5.	5.	0.06
HYDROGRAPH AT 02413	1.	7.95	0.	0.	0.	0.00
ROUTED TO R02413	1.	7.95	0.	0.	0.	0.00
HYDROGRAPH AT 02412	1.	7.95	0.	0.	0.	0.00
ROUTED TO R02412	1.	8.03	0.	0.	0.	0.00
HYDROGRAPH AT 02411	2.	7.95	1.	0.	0.	0.00
ROUTED TO R02411	2.	7.98	1.	0.	0.	0.00
HYDROGRAPH AT 0241	21.	8.10	8.	4.	4.	0.03
4 COMBINED AT 0241p	25.	8.08	9.	4.	4.	0.04
ROUTED TO R241	25.	8.12	9.	4.	4.	0.04
HYDROGRAPH AT 025	9.	7.95	3.	1.	1.	0.01
ROUTED TO R025	9.	7.97	3.	1.	1.	0.01
HYDROGRAPH AT 024	11.	8.00	4.	2.	2.	0.02
3 COMBINED AT 024p	43.	8.05	15.	8.	8.	0.07
ROUTED TO R024	43.	8.07	15.	8.	8.	0.07
HYDROGRAPH AT 023	14.	8.05	5.	2.	2.	0.02
2 COMBINED AT 023p	58.	8.07	20.	10.	10.	0.09
ROUTED TO R023	57.	8.10	20.	10.	10.	0.09
HYDROGRAPH AT 022	10.	8.13	4.	2.	2.	0.02
3 COMBINED AT 022p	89.	8.13	34.	17.	17.	0.17
ROUTED TO R022	88.	8.18	34.	17.	17.	0.17
HYDROGRAPH AT 021	8.	8.00	3.	1.	1.	0.01
3 COMBINED AT 021p	143.	8.10	53.	27.	27.	0.26
ROUTED TO R021	143.	8.12	53.	27.	27.	0.26
HYDROGRAPH AT 2.04	4.	7.98	1.	1.	1.	0.01
ROUTED TO R04	4.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 2.03	9.	7.97	3.	2.	2.	0.02
2 COMBINED AT 2.03	13.	7.98	4.	2.	2.	0.02
ROUTED TO R03	13.	8.65	4.	2.	2.	0.02
HYDROGRAPH AT 2.02	4.	8.07	2.	1.	1.	0.01
3 COMBINED AT						

2.02	150.	8.12	59.	30.	30.	0.29
ROUTED TO R02	146.	8.27	59.	29.	29.	0.29
HYDROGRAPH AT 01172	2.	7.95	1.	0.	0.	0.00
ROUTED TO R01172	2.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 01171	8.	7.95	3.	1.	1.	0.01
2 COMBINED AT 01171p	10.	7.97	3.	2.	2.	0.01
ROUTED TO R01171	10.	7.98	3.	2.	2.	0.01

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HYDROGRAPH AT 0118	4.	7.97	1.	1.	1.	0.01
ROUTED TO R0118	4.	7.98	1.	1.	1.	0.01
HYDROGRAPH AT 0117	13.	7.95	4.	2.	2.	0.02
3 COMBINED AT 0117p	26.	7.97	8.	4.	4.	0.04
ROUTED TO R0117	26.	7.98	8.	4.	4.	0.04
HYDROGRAPH AT 0116	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 0116p	27.	7.98	9.	4.	4.	0.04
ROUTED TO R0116	27.	7.98	9.	4.	4.	0.04
HYDROGRAPH AT 0115	0.	7.92	0.	0.	0.	0.00
2 COMBINED AT 0115p	27.	7.98	9.	4.	4.	0.04
ROUTED TO R0115	27.	8.02	9.	4.	4.	0.04
HYDROGRAPH AT 0114	16.	7.95	5.	3.	3.	0.02
2 COMBINED AT 0114p	42.	8.00	14.	7.	7.	0.06
ROUTED TO R0114	42.	8.07	14.	7.	7.	0.06
HYDROGRAPH AT 0161	9.	7.95	3.	1.	1.	0.01
ROUTED TO R0161	9.	7.97	3.	1.	1.	0.01
HYDROGRAPH AT 017	12.	7.95	4.	2.	2.	0.02
ROUTED TO R017	12.	7.97	4.	2.	2.	0.02
HYDROGRAPH AT 016	4.	7.95	1.	1.	1.	0.01
3 COMBINED AT 016p	26.	7.97	8.	4.	4.	0.04
ROUTED TO R016	26.	7.97	8.	4.	4.	0.04
HYDROGRAPH AT 015	6.	7.97	2.	1.	1.	0.01
2 COMBINED AT 015p	32.	7.97	10.	5.	5.	0.05
ROUTED TO R015	32.	7.98	10.	5.	5.	0.05
HYDROGRAPH AT 014	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 014p	33.	7.98	11.	5.	5.	0.05
ROUTED TO R014	33.	7.98	11.	5.	5.	0.05
HYDROGRAPH AT 013	3.	7.97	1.	0.	0.	0.00
2 COMBINED AT 013p	36.	7.98	12.	6.	6.	0.05
ROUTED TO R013	36.	8.00	12.	6.	6.	0.05
HYDROGRAPH AT 0122	1.	8.00	0.	0.	0.	0.00



R0122	1.	8.00	0.	0.	0.	0.00
HYDROGRAPH AT 0121	1.	7.98	0.	0.	0.	0.00
2 COMBINED AT 0121p	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0121	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 012	5.	7.97	2.	1.	1.	0.01
3 COMBINED AT 012p	43.	8.00	14.	7.	7.	0.06
ROUTED TO R012	42.	8.13	14.	7.	7.	0.06

HYDROGRAPH AT 0113	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0113	2.	8.02	1.	0.	0.	0.00
HYDROGRAPH AT 0112	2.	8.00	1.	0.	0.	0.00
2 COMBINED AT 0112p	4.	8.00	1.	1.	1.	0.01
ROUTED TO R0112	4.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 0111	1.	7.98	0.	0.	0.	0.00
2 COMBINED AT 0111p	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0111	5.	8.07	2.	1.	1.	0.01
HYDROGRAPH AT 011	3.	7.97	1.	1.	1.	0.01
4 COMBINED AT 011p	91.	8.08	31.	15.	15.	0.14
ROUTED TO R11	91.	8.13	31.	15.	15.	0.14
HYDROGRAPH AT 2.01	23.	8.10	8.	4.	4.	0.04
3 COMBINED AT 2.01	254.	8.20	98.	48.	48.	0.47
ROUTED TO R01	253.	8.23	98.	48.	48.	0.47
HYDROGRAPH AT 2.0	201.	9.32	131.	65.	65.	0.83
2 COMBINED AT 2.0	351.	8.30	226.	114.	114.	

1.30

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R21222	MANE	0.20	17.04	477.78	4.08	1.00	17.04	478.00	4.08
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5545E+01 EXCESS=0.0000E+00 OUTFLOW=0.5544E+01 BASIN STORAGE=0.9749E-03 PERCENT ERROR= 0.0									
R21221	MANE	0.19	17.34	478.04	4.08	1.00	17.34	478.00	4.08
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5641E+01 EXCESS=0.0000E+00 OUTFLOW=0.5640E+01 BASIN STORAGE=0.9423E-03 PERCENT ERROR= 0.0									
R02123	MANE	0.22	9.98	477.39	4.26	1.00	9.98	477.00	4.26
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3224E+01 EXCESS=0.0000E+00 OUTFLOW=0.3223E+01 BASIN STORAGE=0.6157E-03 PERCENT ERROR= 0.0									
R02122	MANE	0.18	28.37	478.02	4.15	1.00	28.37	478.00	4.15
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9205E+01 EXCESS=0.0000E+00 OUTFLOW=0.9204E+01 BASIN STORAGE=0.1500E-02 PERCENT ERROR= 0.0									
R02121	MANE	1.00	29.28	479.00	4.15	1.00	29.28	479.00	4.15
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9502E+01 EXCESS=0.0000E+00 OUTFLOW=0.9488E+01 BASIN STORAGE=0.1569E-01 PERCENT ERROR= 0.0									
R0215	MANE	0.39	2.21	477.56	4.19	1.00	2.21	478.00	4.19
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7157E+00 EXCESS=0.0000E+00 OUTFLOW=0.7154E+00 BASIN STORAGE=0.2385E-03 PERCENT ERROR= 0.0									

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA2\2-YEAR25.OUT  
Data File: C:\WINDOWS\TEMP\vbh003B.TMP

\*\*\*\*\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* MAY 1991 \*  
\* VERSION 4.0.1E \*  
\* RUN DATE 09/29/1999 TIME 10:06:29 \*  
\*\*\*\*\*

\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
\*\*\*\*\*

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X   X   XXXXXXXX   XXXXX   X
X   X   X           X   X   XX
X   X   X           X           X
XXXXXXXX XXXX   X           XXXXX   X
X   X   X           X           X
X   X   X           X   X   X
X   X   XXXXXXXX   XXXXX   XXX

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Full Microcomputer Implementation  
by  
Haestad Methods, Inc.

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subbasin 2 - 25 Year Storm									
2	IT	1	1440								
3	IO	5	0								
4	KK	021222									
5	KM	SCS 24 Hour Type IA Rainfall Subbasin 2.02.01.02.02.02									
6	KO	22									
7	BA	.0255									
8	PB	7									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026

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 \* \*  
 871 KK \* 2.0 \*  
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873 KO OUTPUT CONTROL VARIABLES  
 IPRINT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT									
021222	21.	7.95	7.	3.	3.	0.03			
ROUTED TO									
R21222	21.	7.95	7.	3.	3.	0.03			
HYDROGRAPH AT									
021221	0.	7.92	0.	0.	0.	0.00			
2 COMBINED AT									
021221	21.	7.95	7.	3.	3.	0.03			
ROUTED TO									
R21221	21.	7.95	7.	3.	3.	0.03			
HYDROGRAPH AT									
02123	12.	7.95	4.	2.	2.	0.01			
ROUTED TO									
R02123	12.	7.95	4.	2.	2.	0.01			
HYDROGRAPH AT									
02122	1.	7.95	0.	0.	0.	0.00			
3 COMBINED AT									
02122p	35.	7.95	11.	6.	6.	0.04			
ROUTED TO									
R02122	35.	7.95	11.	6.	6.	0.04			
HYDROGRAPH AT									
02121	1.	7.95	0.	0.	0.	0.00			
2 COMBINED AT									
02121p	36.	7.95	12.	6.	6.	0.04			
ROUTED TO									
R02121	36.	7.98	12.	6.	6.	0.04			
HYDROGRAPH AT									
0215	3.	7.95	1.	0.	0.	0.00			
ROUTED TO									
R0215	3.	7.95	1.	0.	0.	0.00			
HYDROGRAPH AT									
020104	1.	7.95	0.	0.	0.	0.00			
2 COMBINED AT									
0214p	4.	7.95	1.	1.	1.	0.00			
ROUTED TO									
R0214	4.	7.98	1.	1.	1.	0.00			
HYDROGRAPH AT									
0213	11.	7.95	4.	2.	2.	0.01			
2 COMBINED AT									
0213p	15.	7.95	5.	2.	2.	0.02			
ROUTED TO									
R0213	15.	7.97	5.	2.	2.	0.02			
HYDROGRAPH AT									
0212	7.	7.95	2.	1.	1.	0.01			
3 COMBINED AT									
0212p	57.	7.98	19.	9.	9.	0.07			

ROUTED TO R0212	57.	7.98	19.	9.	9.	0.07
HYDROGRAPH AT 0211	8.	7.95	3.	1.	1.	0.01
2 COMBINED AT 0211p	65.	7.98	21.	11.	11.	0.08

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ROUTED TO R0211	65.	8.02	21.	11.	11.	0.08
HYDROGRAPH AT 0225	14.	8.10	5.	3.	3.	0.02
ROUTED TO R0225	14.	8.12	5.	3.	3.	0.02
HYDROGRAPH AT 0224	3.	7.98	1.	1.	1.	0.01
2 COMBINED AT 0224p	17.	8.07	6.	3.	3.	0.03
ROUTED TO R0224	17.	8.10	6.	3.	3.	0.03
HYDROGRAPH AT 0223	2.	7.97	1.	0.	0.	0.00
2 COMBINED AT 0223p	18.	8.07	7.	3.	3.	0.03
ROUTED TO R0223	18.	8.08	7.	3.	3.	0.03
HYDROGRAPH AT 0222	1.	7.97	0.	0.	0.	0.00
2 COMBINED AT 0222p	19.	8.07	7.	4.	4.	0.03
ROUTED TO R0222	19.	8.27	7.	4.	4.	0.03
HYDROGRAPH AT 0221	13.	8.20	5.	3.	3.	0.02
2 COMBINED AT 0221p	32.	8.23	12.	6.	6.	0.06
ROUTED TO R0221	32.	8.27	12.	6.	6.	0.06
HYDROGRAPH AT 02413	1.	7.95	0.	0.	0.	0.00
ROUTED TO R02413	1.	7.95	0.	0.	0.	0.00
HYDROGRAPH AT 02412	2.	7.95	1.	0.	0.	0.00
ROUTED TO R02412	2.	8.02	1.	0.	0.	0.00
HYDROGRAPH AT 02411	2.	7.95	1.	0.	0.	0.00
ROUTED TO R02411	2.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 0241	26.	8.10	9.	5.	5.	0.03
4 COMBINED AT 0241p	31.	8.07	11.	5.	5.	0.04
ROUTED TO R241	31.	8.10	11.	5.	5.	0.04
HYDROGRAPH AT 025	11.	7.95	3.	2.	2.	0.01
ROUTED TO R025	11.	7.95	3.	2.	2.	0.01
HYDROGRAPH AT 024	13.	8.00	4.	2.	2.	0.02
3 COMBINED AT 024p	54.	8.05	19.	9.	9.	0.07
ROUTED TO R024	54.	8.07	19.	9.	9.	0.07
HYDROGRAPH AT 023	18.	8.05	6.	3.	3.	0.02
2 COMBINED AT 023p	72.	8.07	25.	12.	12.	0.09
ROUTED TO R023	71.	8.10	25.	12.	12.	0.09

022	11.	8.13	5.	2.	2.	0.02
3 COMBINED AT 022p	112.	8.13	42.	21.	21.	0.17
ROUTED TO R022	112.	8.17	42.	21.	21.	0.17
HYDROGRAPH AT 021	10.	8.00	3.	2.	2.	0.01
3 COMBINED AT 021p	181.	8.10	66.	33.	33.	0.26
ROUTED TO R021	180.	8.12	66.	33.	33.	0.26
HYDROGRAPH AT 2.04	5.	7.97	2.	1.	1.	0.01

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ROUTED TO R04	5.	7.98	2.	1.	1.	0.01
HYDROGRAPH AT 2.03	12.	7.97	4.	2.	2.	0.02
HYDROGRAPH AT WS4	2752.	8.25	1277.	638.	638.	5.22
3 COMBINED AT 2.03	2762.	8.25	1283.	641.	641.	5.24
ROUTED TO R03	2749.	8.33	1282.	637.	637.	5.24
HYDROGRAPH AT 2.02	5.	8.07	2.	1.	1.	0.01
3 COMBINED AT 2.02	2902.	8.32	1350.	671.	671.	5.51
ROUTED TO R02	2892.	8.37	1350.	668.	668.	5.51
HYDROGRAPH AT 01172	2.	7.95	1.	0.	0.	0.00
ROUTED TO R01172	2.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 01171	9.	7.95	3.	2.	2.	0.01
2 COMBINED AT 01171p	12.	7.95	4.	2.	2.	0.01
ROUTED TO R01171	12.	7.97	4.	2.	2.	0.01
HYDROGRAPH AT 0118	4.	7.95	1.	1.	1.	0.01
ROUTED TO R0118	4.	7.98	1.	1.	1.	0.01
HYDROGRAPH AT 0117	16.	7.95	5.	3.	3.	0.02
3 COMBINED AT 0117p	32.	7.97	10.	5.	5.	0.04
ROUTED TO R0117	32.	7.97	10.	5.	5.	0.04
HYDROGRAPH AT 0116	1.	6.63	0.	0.	0.	0.00
2 COMBINED AT 0116p	32.	7.97	11.	5.	5.	0.04
ROUTED TO R0116	32.	7.97	11.	5.	5.	0.04
HYDROGRAPH AT 0115	0.	6.60	0.	0.	0.	0.00
2 COMBINED AT 0115p	32.	7.97	11.	5.	5.	0.04
ROUTED TO R0115	32.	8.00	11.	5.	5.	0.04
HYDROGRAPH AT 0114	23.	6.65	7.	3.	3.	0.02
2 COMBINED AT 0114p	38.	8.00	18.	9.	9.	0.06
ROUTED TO R0114	38.	8.08	18.	8.	8.	0.06
HYDROGRAPH AT 0161	13.	6.65	4.	2.	2.	0.01
ROUTED TO R0161	13.	6.65	4.	2.	2.	0.01
HYDROGRAPH AT 017	15.	7.95	5.	2.	2.	0.02
ROUTED TO R017	15.	7.97	5.	2.	2.	0.02
HYDROGRAPH AT 016	6.	7.95	2.	1.	1.	0.01
3 COMBINED AT						



016P	24.	7.95	11.	5.	5.	0.04
ROUTED TO R016	24.	7.95	11.	5.	5.	0.04
HYDROGRAPH AT 015	8.	7.95	3.	1.	1.	0.01
2 COMBINED AT 015p	32.	7.95	13.	6.	6.	0.05
ROUTED TO R015	32.	7.97	13.	6.	6.	0.05
HYDROGRAPH AT 014	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 014p	33.	7.97	14.	7.	7.	0.05

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ROUTED TO R014	33.	7.97	14.	7.	7.	0.05
HYDROGRAPH AT 013	4.	7.95	1.	1.	1.	0.00
2 COMBINED AT 013p	37.	7.97	15.	7.	7.	0.05
ROUTED TO R013	37.	7.98	15.	7.	7.	0.05
HYDROGRAPH AT 0122	2.	7.97	1.	0.	0.	0.00
ROUTED TO R0122	2.	7.98	1.	0.	0.	0.00
HYDROGRAPH AT 0121	1.	7.97	0.	0.	0.	0.00
2 COMBINED AT 0121p	3.	7.98	1.	0.	0.	0.00
ROUTED TO R0121	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 012	6.	7.97	2.	1.	1.	0.01
3 COMBINED AT 012p	45.	7.98	17.	9.	9.	0.06
ROUTED TO R012	45.	8.12	17.	9.	9.	0.06
HYDROGRAPH AT 0113	3.	7.98	1.	0.	0.	0.00
ROUTED TO R0113	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 0112	2.	7.98	1.	0.	0.	0.00
2 COMBINED AT 0112p	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0112	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 0111	1.	7.97	0.	0.	0.	0.00
2 COMBINED AT 0111p	6.	8.00	2.	1.	1.	0.01
ROUTED TO R0111	6.	8.05	2.	1.	1.	0.01
HYDROGRAPH AT 011	4.	7.97	1.	1.	1.	0.01
4 COMBINED AT 011p	93.	8.08	38.	19.	19.	0.14
ROUTED TO R11	92.	8.13	38.	19.	19.	0.14
HYDROGRAPH AT 2.01	28.	8.10	10.	5.	5.	0.04
3 COMBINED AT 2.01	2986.	8.35	1395.	692.	692.	5.69
ROUTED TO R01	2985.	8.37	1395.	691.	691.	5.69
HYDROGRAPH AT 2.0	266.	9.28	169.	83.	83.	0.83
2 COMBINED AT 2.0	3143.	8.38	1561.	775.	775.	6.52

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R21222	MANE	0.19	21.13	477.31	5.01	1.00	21.13	477.00	5.01

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA2\2-YR100.OUT  
Data File: C:\WINDOWS\TEMP\vbh364E.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 09/29/1999 TIME 13:17:13 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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::
:: Full Microcomputer Implementation ::
:: by ::
:: Haestad Methods, Inc. ::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KN.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subbasin 2 - 100 Year Storm									
2	IT	1			1440						
3	IO	5	0								
4	KK	021222									
5	KM	SCS 24 Hour Type IA Rainfall Subbasin 2.02.01.02.02.02									
6	KO				22						
7	BA	.0255									
8	PB	9.5									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026

K:\RICKJ\GHEC1\99205301\AREA2\2-YR100.OUT  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				24-HOUR	72-HOUR				
HYDROGRAPH AT 021222	31.	7.95	10.	5.	5.	0.03			
ROUTED TO R21222	31.	7.95	10.	5.	5.	0.03			
HYDROGRAPH AT 021221	1.	7.92	0.	0.	0.	0.00			
2 COMBINED AT 021221	32.	7.95	10.	5.	5.	0.03			
ROUTED TO R21221	32.	7.95	10.	5.	5.	0.03			
HYDROGRAPH AT 02123	18.	7.93	6.	3.	3.	0.01			
ROUTED TO R02123	18.	7.95	6.	3.	3.	0.01			
HYDROGRAPH AT 02122	2.	7.93	1.	0.	0.	0.00			
3 COMBINED AT 02122p	52.	7.95	17.	8.	8.	0.04			
ROUTED TO R02122	52.	7.95	17.	8.	8.	0.04			
HYDROGRAPH AT 02121	2.	7.93	1.	0.	0.	0.00			
2 COMBINED AT 02121p	54.	7.95	17.	9.	9.	0.04			
ROUTED TO R02121	53.	7.97	17.	9.	9.	0.04			
HYDROGRAPH AT 0215	4.	7.93	1.	1.	1.	0.00			
ROUTED TO R0215	4.	7.95	1.	1.	1.	0.00			
HYDROGRAPH AT 020104	1.	7.93	0.	0.	0.	0.00			
2 COMBINED AT 0214p	5.	7.95	2.	1.	1.	0.00			
ROUTED TO R0214	5.	7.97	2.	1.	1.	0.00			
HYDROGRAPH AT 0213	16.	7.93	5.	3.	3.	0.01			
2 COMBINED AT 0213p	21.	7.95	7.	3.	3.	0.02			
ROUTED TO R0213	21.	7.95	7.	3.	3.	0.02			
HYDROGRAPH AT 0212	10.	7.95	3.	2.	2.	0.01			
3 COMBINED AT 0212p	85.	7.97	28.	14.	14.	0.07			
ROUTED TO R0212	85.	7.97	28.	14.	14.	0.07			
HYDROGRAPH AT 0211	12.	7.95	4.	2.	2.	0.01			
2 COMBINED AT 0211p	96.	7.97	31.	16.	16.	0.08			
ROUTED TO R0211	96.	8.00	31.	16.	16.	0.08			
HYDROGRAPH AT 0225	22.	8.08	8.	4.	4.	0.02			
ROUTED TO R0225	22.	8.10	8.	4.	4.	0.02			
HYDROGRAPH AT 0224	5.	7.97	2.	1.	1.	0.01			

0224p	27.	8.07	10.	5.	5.	0.03
ROUTED TO R0224	27.	8.08	10.	5.	5.	0.03
HYDROGRAPH AT 0223	3.	7.95	1.	0.	0.	0.00
2 COMBINED AT 0223p	30.	8.07	11.	5.	5.	0.03
ROUTED TO R0223	30.	8.07	11.	5.	5.	0.03
HYDROGRAPH AT 0222	2.	7.95	1.	0.	0.	0.00
2 COMBINED AT 0222p	31.	8.07	11.	6.	6.	0.03

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ROUTED TO R0222	31.	8.23	11.	6.	6.	0.03
HYDROGRAPH AT 0221	21.	8.20	8.	4.	4.	0.02
2 COMBINED AT 0221p	52.	8.22	19.	10.	10.	0.06
ROUTED TO R0221	52.	8.23	19.	10.	10.	0.06
HYDROGRAPH AT 02413	2.	7.93	1.	0.	0.	0.00
ROUTED TO R02413	2.	7.93	1.	0.	0.	0.00
HYDROGRAPH AT 02412	3.	7.93	1.	0.	0.	0.00
ROUTED TO R02412	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 02411	3.	7.93	1.	0.	0.	0.00
ROUTED TO R02411	3.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 0241	39.	8.10	14.	7.	7.	0.03
4 COMBINED AT 0241p	46.	8.07	16.	8.	8.	0.04
ROUTED TO R241	46.	8.10	16.	8.	8.	0.04
HYDROGRAPH AT 025	15.	7.93	5.	2.	2.	0.01
ROUTED TO R025	15.	7.95	5.	2.	2.	0.01
HYDROGRAPH AT 024	20.	7.98	7.	3.	3.	0.02
3 COMBINED AT 024p	79.	8.03	28.	14.	14.	0.07
ROUTED TO R024	79.	8.07	28.	14.	14.	0.07
HYDROGRAPH AT 023	27.	8.05	9.	5.	5.	0.02
2 COMBINED AT 023p	107.	8.05	37.	18.	18.	0.09
ROUTED TO R023	106.	8.08	37.	18.	18.	0.09
HYDROGRAPH AT 022	20.	8.12	7.	3.	3.	0.02
3 COMBINED AT 022p	173.	8.12	63.	31.	31.	0.17
ROUTED TO R022	173.	8.15	63.	31.	31.	0.17
HYDROGRAPH AT 021	15.	7.98	5.	2.	2.	0.01
3 COMBINED AT 021p	275.	8.08	99.	49.	49.	0.26
ROUTED TO R021	275.	8.10	99.	49.	49.	0.26
HYDROGRAPH AT 2.04	8.	7.95	3.	1.	1.	0.01
ROUTED TO R04	8.	7.97	3.	1.	1.	0.01
HYDROGRAPH AT 2.03	18.	7.95	6.	3.	3.	0.02
HYDROGRAPH AT WS4	4322.	8.25	1937.	962.	962.	5.22
3 COMBINED AT 2.03	4338.	8.25	1945.	966.	966.	5.24

ROUTED TO R03	4326.	8.30	1945.	961.	961.	5.24
HYDROGRAPH AT 2.02	4.	20.42	4.	1.	1.	0.01
3 COMBINED AT 2.02	4559.	8.28	2044.	1012.	1012.	5.51
ROUTED TO R02	4545.	8.33	2044.	1008.	1008.	5.51
HYDROGRAPH AT 01172	1.	20.35	1.	1.	1.	0.00
ROUTED TO R01172	1.	20.42	1.	1.	1.	0.00
HYDROGRAPH AT 01171	6.	20.42	5.	2.	2.	0.01

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2 COMBINED AT 01171p	7.	20.42	7.	3.	3.	0.01
ROUTED TO R01171	7.	20.40	7.	3.	3.	0.01
HYDROGRAPH AT 0118	3.	20.37	3.	1.	1.	0.01
ROUTED TO R0118	3.	20.42	3.	1.	1.	0.01
HYDROGRAPH AT 0117	9.	20.40	8.	4.	4.	0.02
3 COMBINED AT 0117p	19.	20.42	17.	8.	8.	0.04
ROUTED TO R0117	19.	20.40	17.	8.	8.	0.04
HYDROGRAPH AT 0116	2.	6.63	1.	0.	0.	0.00
2 COMBINED AT 0116p	19.	20.03	18.	8.	8.	0.04
ROUTED TO R0116	19.	20.03	18.	8.	8.	0.04
HYDROGRAPH AT 0115	0.	6.62	0.	0.	0.	0.00
2 COMBINED AT 0115p	19.	20.03	18.	8.	8.	0.04
ROUTED TO R0115	19.	20.08	18.	8.	8.	0.04
HYDROGRAPH AT 0114	34.	6.63	10.	5.	5.	0.02
2 COMBINED AT 0114p	37.	6.65	21.	13.	13.	0.06
ROUTED TO R0114	37.	6.73	21.	13.	13.	0.06
HYDROGRAPH AT 0161	19.	6.63	6.	3.	3.	0.01
ROUTED TO R0161	19.	6.65	6.	3.	3.	0.01
HYDROGRAPH AT 017	22.	7.95	7.	4.	4.	0.02
ROUTED TO R017	22.	7.95	7.	4.	4.	0.02
HYDROGRAPH AT 016	8.	7.93	3.	1.	1.	0.01
3 COMBINED AT 016p	35.	7.93	15.	7.	7.	0.04
ROUTED TO R016	35.	7.95	15.	7.	7.	0.04
HYDROGRAPH AT 015	12.	7.95	4.	2.	2.	0.01
2 COMBINED AT 015p	47.	7.95	19.	9.	9.	0.05
ROUTED TO R015	47.	7.95	19.	9.	9.	0.05
HYDROGRAPH AT 014	2.	7.93	1.	0.	0.	0.00
2 COMBINED AT 014p	49.	7.95	20.	10.	10.	0.05
ROUTED TO R014	49.	7.97	20.	10.	10.	0.05
HYDROGRAPH AT 013	6.	7.95	2.	1.	1.	0.00
2 COMBINED AT 013p	55.	7.95	22.	11.	11.	0.05
ROUTED TO R013	55.	7.97	22.	11.	11.	0.05



HYDROGRAPH AT 0122	3.	7.95	1.	0.	0.	0.00
ROUTED TO R0122	3.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 0121	1.	7.95	0.	0.	0.	0.00
2 COMBINED AT 0121p	4.	7.97	1.	1.	1.	0.00
ROUTED TO R0121	4.	7.98	1.	1.	1.	0.00
HYDROGRAPH AT 012	9.	7.95	3.	1.	1.	0.01
3 COMBINED AT 012p	67.	7.97	26.	13.	13.	0.06

K:\RICKJ\GHEC1\99205301\AREA2\2-YR100.OUT

ROUTED TO R012	67.	8.10	26.	13.	13.	0.06
HYDROGRAPH AT 0113	4.	7.97	1.	1.	1.	0.00
ROUTED TO R0113	4.	7.98	1.	1.	1.	0.00
HYDROGRAPH AT 0112	4.	7.97	1.	1.	1.	0.00
2 COMBINED AT 0112p	8.	7.97	3.	1.	1.	0.01
ROUTED TO R0112	8.	7.97	3.	1.	1.	0.01
HYDROGRAPH AT 0111	2.	7.95	1.	0.	0.	0.00
2 COMBINED AT 0111p	10.	7.97	3.	2.	2.	0.01
ROUTED TO R0111	10.	8.03	3.	2.	2.	0.01
HYDROGRAPH AT 011	6.	7.95	2.	1.	1.	0.01
4 COMBINED AT 011p	96.	8.07	49.	28.	28.	0.14
ROUTED TO R11	96.	8.10	49.	28.	28.	0.14
HYDROGRAPH AT 2.01	17.	23.98	16.	7.	7.	0.04
3 COMBINED AT 2.01	4627.	8.32	2095.	1043.	1043.	5.69
ROUTED TO R01	4625.	8.33	2095.	1042.	1042.	5.69
HYDROGRAPH AT 2.0	436.	9.23	269.	131.	131.	0.83
2 COMBINED AT 2.0	4890.	8.35	2359.	1174.	1174.	6.52

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			VOLUME
						DT	PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R21222	MANE	0.17	31.42	477.01	7.39	1.00	31.42	477.00	7.39
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1006E+02 EXCESS=0.0000E+00 OUTFLOW=0.1006E+02 BASIN STORAGE=0.1410E-02 PERCENT ERROR= 0.0									
R21221	MANE	0.16	31.95	477.05	7.40	1.00	31.95	477.00	7.40
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1023E+02 EXCESS=0.0000E+00 OUTFLOW=0.1022E+02 BASIN STORAGE=0.1362E-02 PERCENT ERROR= 0.0									
R02123	MANE	0.19	18.00	476.38	7.61	1.00	18.00	477.00	7.61
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5761E+01 EXCESS=0.0000E+00 OUTFLOW=0.5760E+01 BASIN STORAGE=0.8856E-03 PERCENT ERROR= 0.0									
R02122	MANE	0.15	51.85	477.04	7.48	1.00	51.85	477.00	7.48
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1660E+02 EXCESS=0.0000E+00 OUTFLOW=0.1659E+02 BASIN STORAGE=0.2151E-02 PERCENT ERROR= 0.0									
R02121	MANE	1.00	53.49	478.00	7.47	1.00	53.49	478.00	7.47
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1713E+02 EXCESS=0.0000E+00 OUTFLOW=0.1711E+02 BASIN STORAGE=0.2257E-01 PERCENT ERROR= 0.0									
R0215	MANE	0.34	4.02	476.55	7.53	1.00	4.02	477.00	7.53
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1286E+01 EXCESS=0.0000E+00 OUTFLOW=0.1285E+01 BASIN STORAGE=0.3456E-03 PERCENT ERROR= 0.0									

HEC1 S/N: 1343001909

HMVersion: 6.33

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Data File: C:\WINDOWS\TEMP\vbh332F.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 08/03/1999 TIME 10:27:05 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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::::::::::::::::::::::::::::::::::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
::: :::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID HVL SWMP - Subasin 3 - 10 Year Storm
2 IT 1 1440
3 IO 5 0
4 KK 0204
5 KM SCS 24 Hour Type IA Rainfall HVL SWMP - 3.02.04 Subbasin
6 KO 22
7 BA .02
8 PB 6
9 IN 6
10 PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776
11 PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695
12 PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880
13 PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229
14 PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159
15 PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049
16 PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127
17 PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.31142 0.31549 0.31976 0.32425
18 PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296
19 PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184

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HYDROGRAPH AT 0201	1.	7.90	0.	0.	0.	0.00
2 COMBINED AT P0201	24.	7.92	8.	4.	4.	0.03
ROUTED TO R0201	24.	7.92	8.	4.	4.	0.03
HYDROGRAPH AT 0200	1196.	8.45	579.	290.	290.	3.55
3 COMBINED AT P0200	1217.	8.45	594.	298.	298.	3.64
ROUTED TO R0200	1217.	8.47	594.	298.	298.	3.64
HYDROGRAPH AT 010101	6.	7.90	2.	1.	1.	0.01
ROUTED TO R10101	6.	7.90	2.	1.	1.	0.01
HYDROGRAPH AT 0101	1.	7.93	0.	0.	0.	0.00
2 COMBINED AT P0101	7.	7.90	2.	1.	1.	0.01
ROUTED TO R10101	7.	7.90	2.	1.	1.	0.01
HYDROGRAPH AT 0102	5.	7.92	2.	1.	1.	0.01
ROUTED TO R0102	5.	7.95	2.	1.	1.	0.01
HYDROGRAPH AT 0100	6.	8.02	2.	1.	1.	0.01
4 COMBINED AT P0100	1225.	8.47	600.	301.	301.	3.67
ROUTED TO R01	1225.	8.47	600.	301.	301.	3.67
HYDROGRAPH AT 0000	8.	7.93	3.	1.	1.	0.01
2 COMBINED AT 3.0	1228.	8.47	602.	302.	302.	3.67

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)
							PEAK (CFS)	TIME TO PEAK (MIN)	
R0204	MANE	1.00	8.83	480.00	2.93	1.00	8.83	480.00	2.93
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3135E+01 EXCESS=0.0000E+00 OUTFLOW=0.3124E+01 BASIN STORAGE=0.1189E-01 PERCENT ERROR= 0.0									
R20301	MANE	1.00	3.96	478.00	3.12	1.00	3.96	478.00	3.12
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1369E+01 EXCESS=0.0000E+00 OUTFLOW=0.1367E+01 BASIN STORAGE=0.2901E-02 PERCENT ERROR= 0.0									
R0203	MANE	0.76	15.09	479.88	3.02	1.00	15.09	480.00	3.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5295E+01 EXCESS=0.0000E+00 OUTFLOW=0.5291E+01 BASIN STORAGE=0.4014E-02 PERCENT ERROR= 0.0									
R0202	MANE	1.00	23.01	484.00	3.15	1.00	23.01	484.00	3.15
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8025E+01 EXCESS=0.0000E+00 OUTFLOW=0.7979E+01 BASIN STORAGE=0.5150E-01 PERCENT ERROR= -0.1									
R20111	MANE	0.89	1.59	473.95	4.51	1.00	1.59	474.00	4.51
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5057E+00 EXCESS=0.0000E+00 OUTFLOW=0.5053E+00 BASIN STORAGE=0.3683E-03 PERCENT ERROR= 0.0									

HEC1 S/N: 1343001909

HMVersion: 6.33

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Data File: C:\WINDOWS\TEMP\vbh1c48.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 09/29/1999 TIME 10:17:28 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

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THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
1	ID	HVL SWMP - Subasin 3 - 25 Year Storm									
2	IT	1 1440									
3	IO	5 0									
4	KK	0204									
5	KM	SCS 24 Hour Type IA Rainfall HVL SWMP - 3.02.04 Subbasin									
6	KO	22									
7	BA	.02									
8	PB	7									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01560	0.01776
11	PC	0.0200	0.02276	0.02560	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026



P0200	1605.	8.43	762.	380.	380.	3.64
ROUTED TO R0200	1605.	8.45	762.	380.	380.	3.64
HYDROGRAPH AT 010101	7.	7.90	2.	1.	1.	0.01



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ROUTED TO R10101	7.	7.90	2.	1.	1.	0.01
HYDROGRAPH AT 0101	1.	7.93	0.	0.	0.	0.00
2 COMBINED AT P0101	8.	7.90	3.	1.	1.	0.01
ROUTED TO R10101	8.	7.90	3.	1.	1.	0.01
HYDROGRAPH AT 0102	7.	7.92	2.	1.	1.	0.01
ROUTED TO R0102	7.	7.93	2.	1.	1.	0.01
HYDROGRAPH AT 0100	8.	8.02	3.	1.	1.	0.01
4 COMBINED AT P0100	1615.	8.45	770.	384.	384.	3.67
ROUTED TO R01	1614.	8.47	770.	383.	383.	3.67
HYDROGRAPH AT 0000	5.	7.95	2.	1.	1.	0.01
HYDROGRAPH AT WS2	3143.	8.38	1561.	775.	775.	6.52
3 COMBINED AT 3.0	4748.	8.42	2332.	1159.	1159.	10.19

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO		VOLUME (IN)
							COMPUTATION PEAK (CFS)	INTERVAL TIME TO PEAK (MIN)	
R0204	MANE	1.00	11.71	479.00	3.76	1.00	11.71	479.00	3.76
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4019E+01 EXCESS=0.0000E+00 OUTFLOW=0.4007E+01 BASIN STORAGE=0.1374E-01 PERCENT ERROR= 0.0									
R20301	MANE	1.00	5.18	477.00	3.97	1.00	5.18	477.00	3.97
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1741E+01 EXCESS=0.0000E+00 OUTFLOW=0.1738E+01 BASIN STORAGE=0.3332E-02 PERCENT ERROR= 0.0									
R0203	MANE	0.71	19.85	479.41	3.86	1.00	19.84	479.00	3.86
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6761E+01 EXCESS=0.0000E+00 OUTFLOW=0.6757E+01 BASIN STORAGE=0.4630E-02 PERCENT ERROR= 0.0									
R0202	MANE	1.00	30.06	480.00	4.00	1.00	30.06	480.00	4.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1019E+02 EXCESS=0.0000E+00 OUTFLOW=0.1013E+02 BASIN STORAGE=0.5911E-01 PERCENT ERROR= -0.1									
R20111	MANE	0.85	1.93	473.67	5.47	1.00	1.93	474.00	5.47
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6134E+00 EXCESS=0.0000E+00 OUTFLOW=0.6130E+00 BASIN STORAGE=0.4166E-03 PERCENT ERROR= 0.0									
R20102	MANE	0.94	8.93	474.84	5.32	1.00	8.93	475.00	5.32
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2839E+01 EXCESS=0.0000E+00 OUTFLOW=0.2837E+01 BASIN STORAGE=0.2240E-02 PERCENT ERROR= 0.0									
R20101	MANE	0.31	28.42	474.73	5.20	1.00	28.42	475.00	5.20
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9049E+01 EXCESS=0.0000E+00 OUTFLOW=0.9046E+01 BASIN STORAGE=0.2411E-02 PERCENT ERROR= 0.0									
R0201	MANE	0.80	29.60	475.31	5.20	1.00	29.60	475.00	5.20



K:\RICKJ\GHECI\99205301\AREA3\3-YR100.OUT  
 TIMINT 0.017 TIME INTERVAL IN HOURS

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 \* \* \* \* \*  
 683 KK \* 3.0 \*  
 \* \* \* \* \*  
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685 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD		BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR			
HYDROGRAPH AT 0204	19.	7.93	6.	3.	3.	0.02		
ROUTED TO R0204	19.	7.97	6.	3.	3.	0.02		
HYDROGRAPH AT 020301	8.	7.92	3.	1.	1.	0.01		
ROUTED TO R20301	8.	7.95	3.	1.	1.	0.01		
HYDROGRAPH AT 0203	5.	7.90	2.	1.	1.	0.00		
3 COMBINED AT P0203	32.	7.95	11.	5.	5.	0.03		
ROUTED TO R0203	32.	7.97	11.	5.	5.	0.03		
HYDROGRAPH AT 0202	16.	7.90	5.	3.	3.	0.01		
2 COMBINED AT P0202	49.	7.92	16.	8.	8.	0.05		
ROUTED TO R0202	49.	7.98	16.	8.	8.	0.05		
HYDROGRAPH AT 020111	3.	7.80	1.	0.	0.	0.00		
ROUTED TO R20111	3.	7.82	1.	0.	0.	0.00		
HYDROGRAPH AT 020102	13.	7.90	4.	2.	2.	0.01		
ROUTED TO R20102	13.	7.92	4.	2.	2.	0.01		
HYDROGRAPH AT 020101	26.	7.90	8.	4.	4.	0.02		
3 COMBINED AT P20101	42.	7.90	13.	7.	7.	0.03		
ROUTED TO R20101	42.	7.90	13.	7.	7.	0.03		
HYDROGRAPH AT 0201	2.	7.90	1.	0.	0.	0.00		
2 COMBINED AT P0201	43.	7.90	14.	7.	7.	0.03		
ROUTED TO R0201	43.	7.92	14.	7.	7.	0.03		
HYDROGRAPH AT 0200	2587.	8.43	1173.	580.	580.	3.55		

P0200	2628.	8.42	1202.	595.	595.	3.64
ROUTED TO R0200	2627.	8.43	1202.	594.	594.	3.64
HYDROGRAPH AT 010101	11.	7.80	3.	2.	2.	0.01

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ROUTED TO R10101	11.	7.80	3.	2.	2.	0.01
HYDROGRAPH AT 0101	1.	7.93	0.	0.	0.	0.00
2 COMBINED AT P0101	12.	7.90	4.	2.	2.	0.01
ROUTED TO R10101	12.	7.90	4.	2.	2.	0.01
HYDROGRAPH AT 0102	10.	7.92	3.	2.	2.	0.01
ROUTED TO R0102	10.	7.93	3.	2.	2.	0.01
HYDROGRAPH AT 0100	13.	8.00	4.	2.	2.	0.01
4 COMBINED AT P0100	2643.	8.43	1213.	600.	600.	3.67
ROUTED TO R01	2642.	8.45	1213.	600.	600.	3.67
HYDROGRAPH AT 0000	8.	7.93	3.	1.	1.	0.01
HYDROGRAPH AT Node79	4890.	8.35	2359.	1174.	1174.	6.52
3 COMBINED AT 3.0	7509.	8.40	3574.	1775.	1775.	10.20

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)	
							PEAK (CFS)	TIME TO PEAK (MIN)		
R0204	MANE	1.00	19.35	478.00	5.94	1.00	19.35	478.00	5.94	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6354E+01 EXCESS=0.0000E+00 OUTFLOW=0.6338E+01 BASIN STORAGE=0.1802E-01 PERCENT ERROR= 0.0										
R20301	MANE	1.00	8.37	477.00	6.20	1.00	8.37	477.00	6.20	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2717E+01 EXCESS=0.0000E+00 OUTFLOW=0.2714E+01 BASIN STORAGE=0.4326E-02 PERCENT ERROR= 0.0										
R0203	MANE	0.62	32.40	477.98	6.07	1.00	32.40	478.00	6.07	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1062E+02 EXCESS=0.0000E+00 OUTFLOW=0.1062E+02 BASIN STORAGE=0.6056E-02 PERCENT ERROR= 0.0										
R0202	MANE	1.00	48.59	479.00	6.23	1.00	48.59	479.00	6.23	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1585E+02 EXCESS=0.0000E+00 OUTFLOW=0.1578E+02 BASIN STORAGE=0.7662E-01 PERCENT ERROR= -0.1										
R20111	MANE	0.78	2.79	468.85	7.91	1.00	2.79	469.00	7.91	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8860E+00 EXCESS=0.0000E+00 OUTFLOW=0.8856E+00 BASIN STORAGE=0.5294E-03 PERCENT ERROR= 0.0										
R20102	MANE	0.86	12.98	474.53	7.74	1.00	12.98	475.00	7.74	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4129E+01 EXCESS=0.0000E+00 OUTFLOW=0.4126E+01 BASIN STORAGE=0.2845E-02 PERCENT ERROR= 0.0										
R20101	MANE	0.28	41.65	474.34	7.61	1.00	41.65	474.00	7.61	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1323E+02 EXCESS=0.0000E+00 OUTFLOW=0.1323E+02 BASIN STORAGE=0.3064E-02 PERCENT ERROR= 0.0										
R0201	MANE	0.71	43.40	474.23	7.60	1.00	43.40	475.00	7.60	

HEC1 S/N: 1343001909

HMVersion: 6.33

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Data File: C:\WINDOWS\TEMP\vbh1533.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 07/27/1999 TIME 13:29:50 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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: Full Microcomputer Implementation :
: by :
: Haestad Methods, Inc. :
: :
: :

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.37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID HVL SWMP - Subbasin 4 - 10 Year Storm
2	IT 5 283
3	IO 5 0
4	KK 0181
5	KM SCS 24 Hour Type IA Rainfall Subbasin 4.01.08.01
6	KO 22
7	BA .0081
8	PB 6
9	IN 6
10	PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776
11	PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695
12	PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880
13	PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229
14	PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159
15	PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049
16	PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127
17	PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.31142 0.35469 0.37876 0.40255
18	PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296
19	PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184

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QSCAL      0.  HYDROGRAPH PLOT SCALE
IPNCH      0   PUNCH COMPUTED HYDROGRAPH
IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
ISAV1      1   FIRST ORDINATE PUNCHED OR SAVED
ISAV2     283  LAST ORDINATE PUNCHED OR SAVED
TIMINT     0.083 TIME INTERVAL IN HOURS
  
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*****
*                               *
* 2879 KK      4.11             *
*                               *
*****
  
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2881 KO      OUTPUT CONTROL VARIABLES
              IPRNT      5   PRINT CONTROL
              IPLOT      0   PLOT CONTROL
              QSCAL      0.  HYDROGRAPH PLOT SCALE
              IPNCH      0   PUNCH COMPUTED HYDROGRAPH
              IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
              ISAV1      1   FIRST ORDINATE PUNCHED OR SAVED
              ISAV2     283  LAST ORDINATE PUNCHED OR SAVED
              TIMINT     0.083 TIME INTERVAL IN HOURS
  
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*****
*                               *
* 2912 KK      HVLAKE          *
*                               *
*****
  
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2914 KO      OUTPUT CONTROL VARIABLES
              IPRNT      5   PRINT CONTROL
              IPLOT      0   PLOT CONTROL
              QSCAL      0.  HYDROGRAPH PLOT SCALE
              IPNCH      0   PUNCH COMPUTED HYDROGRAPH
              IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
              ISAV1      1   FIRST ORDINATE PUNCHED OR SAVED
              ISAV2     283  LAST ORDINATE PUNCHED OR SAVED
              TIMINT     0.083 TIME INTERVAL IN HOURS
  
```

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
24-HOUR	72-HOUR								
HYDROGRAPH AT									
0181	4.	8.00	1.	1.	1.	1.	0.01		
ROUTED TO									
R0181	4.	8.00	1.	1.	1.	1.	0.01		
HYDROGRAPH AT									
018	323.	8.25	139.	70.	70.	70.	0.86		
2 COMBINED AT									
018p	326.	8.25	140.	71.	71.	71.	0.86		
ROUTED TO									
R018	326.	8.25	140.	71.	71.	71.	0.86		
HYDROGRAPH AT									
017	2.	8.00	1.	0.	0.	0.	0.01		
2 COMBINED AT									
017p	327.	8.25	141.	71.	71.	71.	0.87		
ROUTED TO									
R017	327.	8.25	141.	71.	71.	71.	0.87		
HYDROGRAPH AT									
016	2.	8.00	1.	0.	0.	0.	0.00		

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2 COMBINED AT 016p	328.	8.25	141.	72.	72.	0.87
ROUTED TO R016	328.	8.25	141.	72.	72.	0.87
HYDROGRAPH AT 015	2.	8.00	1.	0.	0.	0.00
2 COMBINED AT 015p	329.	8.25	142.	72.	72.	0.88
ROUTED TO R015	329.	8.25	142.	72.	72.	0.88
HYDROGRAPH AT 0141	7.	8.00	2.	1.	1.	0.01
ROUTED TO R0141	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 014	16.	8.00	5.	3.	3.	0.02
3 COMBINED AT 014p	344.	8.25	150.	76.	76.	0.90
ROUTED TO R014	344.	8.25	150.	76.	76.	0.90
HYDROGRAPH AT 0135	31.	8.00	11.	5.	5.	0.03
ROUTED TO R0135	31.	8.00	11.	5.	5.	0.03
HYDROGRAPH AT 01341	4.	8.00	1.	1.	1.	0.00
ROUTED TO R01341	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 01342	19.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 0134	12.	8.00	4.	2.	2.	0.01
4 COMBINED AT 0134p	67.	8.00	22.	11.	11.	0.07
ROUTED TO R0134	67.	8.00	22.	11.	11.	0.07
HYDROGRAPH AT 0133	19.	8.00	6.	3.	3.	0.02
2 COMBINED AT 0133p	86.	8.00	29.	14.	14.	0.08
ROUTED TO R0133	86.	8.00	29.	14.	14.	0.08
HYDROGRAPH AT 01321	5.	8.00	1.	1.	1.	0.00
ROUTED TO R01321	5.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0132	13.	8.00	4.	2.	2.	0.01
3 COMBINED AT 0132p	103.	8.00	34.	17.	17.	0.10
ROUTED TO R0132	103.	8.00	34.	17.	17.	0.10
HYDROGRAPH AT 0131	20.	8.00	7.	3.	3.	0.02
2 COMBINED AT 0131p	123.	8.00	41.	21.	21.	0.12
ROUTED TO R0131	122.	8.00	41.	21.	21.	0.12
HYDROGRAPH AT 013	12.	8.00	4.	2.	2.	0.01
3 COMBINED AT 013p	448.	8.08	194.	99.	99.	1.03
ROUTED TO						



R013	447.	8.17	194.	99.	99.	1.03
HYDROGRAPH AT 0122	29.	8.00	9.	5.	5.	0.02
ROUTED TO R0122	29.	8.00	9.	5.	5.	0.02
HYDROGRAPH AT 0121	15.	8.00	5.	3.	3.	0.01
2 COMBINED AT 0121p	44.	8.00	15.	7.	7.	0.04
ROUTED TO R0121	44.	8.00	15.	7.	7.	0.04
HYDROGRAPH AT 012	18.	8.00	6.	3.	3.	0.02

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3 COMBINED AT 012p	503.	8.08	214.	109.	109.	1.09
ROUTED TO R012	501.	8.08	214.	109.	109.	1.09
HYDROGRAPH AT 0111	14.	8.00	5.	2.	2.	0.01
HYDROGRAPH AT 011	11.	8.00	4.	2.	2.	0.01
3 COMBINED AT 011p	524.	8.08	222.	113.	113.	1.11
ROUTED TO R011	520.	8.08	222.	113.	113.	1.11
HYDROGRAPH AT 1052	15.	8.00	5.	2.	2.	0.02
ROUTED TO R1052	15.	8.00	5.	2.	2.	0.02
HYDROGRAPH AT 1051	5.	8.00	2.	1.	1.	0.01
2 COMBINED AT 1051p	19.	8.00	6.	3.	3.	0.03
ROUTED TO R1051	19.	8.00	6.	3.	3.	0.03
HYDROGRAPH AT 107	2.	8.00	1.	0.	0.	0.00
ROUTED TO R107	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 106	30.	8.00	10.	5.	5.	0.05
2 COMBINED AT 106p	32.	8.00	11.	6.	6.	0.06
ROUTED TO R106	32.	8.00	11.	6.	6.	0.06
HYDROGRAPH AT 105	10.	8.00	3.	2.	2.	0.02
3 COMBINED AT 105p	61.	8.00	21.	10.	10.	0.11
ROUTED TO R105	61.	8.00	21.	10.	10.	0.11
HYDROGRAPH AT 1043	1.	8.00	0.	0.	0.	0.00
ROUTED TO R1043	1.	8.00	0.	0.	0.	0.00
HYDROGRAPH AT 1042	6.	8.00	2.	1.	1.	0.01
2 COMBINED AT 1043p	8.	8.00	3.	1.	1.	0.01
ROUTED TO R1042	8.	8.00	3.	1.	1.	0.01
HYDROGRAPH AT 1041	2.	8.00	1.	0.	0.	0.00
2 COMBINED AT 1041p	9.	8.00	3.	2.	2.	0.01
ROUTED TO R1041	9.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 104	7.	8.00	2.	1.	1.	0.01
3 COMBINED AT 104p	77.	8.00	26.	13.	13.	0.13
ROUTED TO R104	76.	8.00	26.	13.	13.	0.13
HYDROGRAPH AT 103	6.	8.00	2.	1.	1.	0.01

103p	82.	8.00	28.	14.	14.	0.14
ROUTED TO R103	82.	8.00	28.	14.	14.	0.14
HYDROGRAPH AT 1021	1.	8.00	0.	0.	0.	0.00
ROUTED TO R1021	1.	8.00	0.	0.	0.	0.00
HYDROGRAPH AT 102	9.	8.00	3.	1.	1.	0.01
3 COMBINED AT 102p	92.	8.00	31.	16.	16.	0.16
ROUTED TO R102	92.	8.00	31.	16.	16.	0.16

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HYDROGRAPH AT 10121	2.	8.00	1.	0.	0.	0.00
ROUTED TO R10121	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 10122	5.	8.00	2.	1.	1.	0.00
ROUTED TO R10122	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 1012	9.	8.00	3.	1.	1.	0.01
3 COMBINED AT 1012p	16.	8.00	5.	3.	3.	0.02
ROUTED TO R1012	16.	8.00	5.	3.	3.	0.02
HYDROGRAPH AT 1011	11.	8.00	4.	2.	2.	0.01
ROUTED TO R1011	11.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 101	23.	8.00	8.	4.	4.	0.02
4 COMBINED AT 101p	142.	8.00	48.	24.	24.	0.20
ROUTED TO R101	142.	8.00	48.	24.	24.	0.20
HYDROGRAPH AT 026	1.	8.00	0.	0.	0.	0.00
ROUTED TO R026	1.	8.08	0.	0.	0.	0.00
HYDROGRAPH AT 025	5.	8.00	2.	1.	1.	0.01
2 COMBINED AT 025p	6.	8.00	2.	1.	1.	0.01
ROUTED TO R025	6.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 0241	4.	8.00	1.	1.	1.	0.01
ROUTED TO R0241	4.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 024	13.	8.00	4.	2.	2.	0.03
3 COMBINED AT 024p	23.	8.00	8.	4.	4.	0.05
ROUTED TO R024	23.	8.00	8.	4.	4.	0.05
HYDROGRAPH AT 0231	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0231	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 023	42.	8.00	14.	7.	7.	0.04
3 COMBINED AT 023p	67.	8.00	23.	12.	12.	0.09
ROUTED TO R023	67.	8.00	23.	12.	12.	0.09
HYDROGRAPH AT 022	59.	8.00	20.	10.	10.	0.05
2 COMBINED AT 022p	126.	8.00	42.	21.	21.	0.14
ROUTED TO R022	126.	8.00	42.	21.	21.	0.14
HYDROGRAPH AT 021	72.	8.00	24.	12.	12.	0.07
2 COMBINED AT						

021p	198.	8.00	66.	33.	33.	0.21
ROUTED TO R021	198.	8.00	66.	33.	33.	0.21
HYDROGRAPH AT 116	11.	8.00	4.	2.	2.	0.02
ROUTED TO R116	11.	8.00	4.	2.	2.	0.02
HYDROGRAPH AT 115	7.	8.00	2.	1.	1.	0.01
2 COMBINED AT 115p	18.	8.00	6.	3.	3.	0.03
ROUTED TO R115	18.	8.00	6.	3.	3.	0.03

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HYDROGRAPH AT 114	8.	8.00	3.	1.	1.	0.01
2 COMBINED AT 114p	26.	8.00	9.	4.	4.	0.05
ROUTED TO R114	26.	8.00	9.	4.	4.	0.05
HYDROGRAPH AT 1132	2.	8.00	1.	0.	0.	0.00
ROUTED TO R1132	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1131	1.	8.00	0.	0.	0.	0.00
2 COMBINED AT 1131p	3.	8.00	1.	1.	1.	0.01
ROUTED TO R1131	3.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 113	2.	8.00	1.	0.	0.	0.00
3 COMBINED AT 113p	31.	8.00	11.	5.	5.	0.06
ROUTED TO R113	31.	8.00	11.	5.	5.	0.06
HYDROGRAPH AT 1121	8.	8.00	3.	1.	1.	0.02
ROUTED TO R1121	8.	8.00	3.	1.	1.	0.02
HYDROGRAPH AT 112	1.	8.00	0.	0.	0.	0.00
3 COMBINED AT 112p	41.	8.00	14.	7.	7.	0.07
ROUTED TO R112	41.	8.00	14.	7.	7.	0.07
HYDROGRAPH AT 111	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1111	2.	8.00	1.	0.	0.	0.00
3 COMBINED AT 111p	45.	8.00	16.	8.	8.	0.08
ROUTED TO R111	45.	8.00	16.	8.	8.	0.08
HYDROGRAPH AT 043	23.	8.00	8.	4.	4.	0.04
HYDROGRAPH AT 0431	13.	8.00	4.	2.	2.	0.02
2 COMBINED AT 043p	36.	8.00	12.	6.	6.	0.06
ROUTED TO R043	36.	8.00	12.	6.	6.	0.06
HYDROGRAPH AT 042	34.	8.00	11.	6.	6.	0.05
2 COMBINED AT 042p	70.	8.00	23.	12.	12.	0.11
ROUTED TO R042	70.	8.00	23.	12.	12.	0.11
HYDROGRAPH AT 0411	10.	8.00	3.	2.	2.	0.01
ROUTED TO R0411	10.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 041	55.	8.00	18.	9.	9.	0.08
3 COMBINED AT 041p	134.	8.00	45.	23.	23.	0.21
ROUTED TO						

R041	114.	8.00	45.	23.	23.	0.21
HYDROGRAPH AT 031	2.	8.00	1.	0.	0.	0.00
ROUTED TO R031	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 0501	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0501	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 0601	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0601	5.	8.00	2.	1.	1.	0.01

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HYDROGRAPH AT 0701	4.	8.00	1.	1.	1.	0.01
ROUTED TO R0701	4.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 0801	4.	8.00	1.	1.	1.	0.00
ROUTED TO R0801	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0901	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0901	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.01	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.04	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 4.02	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 4.03	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.05	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.06	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.07	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.08	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 4.09	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.10	16.	8.00	5.	3.	3.	0.01
HYDROGRAPH AT 4.11	6.	8.00	2.	1.	1.	0.01
22 COMBINED AT HVLAKE	1098.	8.00	423.	215.	215.	

1.94

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0181	MANE	0.92	4.12	480.16	3.26	5.00	4.11	480.00	3.27
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1411E+01 EXCESS=0.0000E+00 OUTFLOW=0.1410E+01 BASIN STORAGE=0.1270E-02 PERCENT ERROR= 0.0									
R018	MANE	0.24	325.94	494.88	3.00	5.00	325.94	495.00	3.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1380E+03 EXCESS=0.0000E+00 OUTFLOW=0.1380E+03 BASIN STORAGE=0.3455E-01 PERCENT ERROR= 0.0									
R017	MANE	0.46	327.31	494.88	3.00	5.00	327.31	495.00	3.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1388E+03 EXCESS=0.0000E+00 OUTFLOW=0.1388E+03 BASIN STORAGE=0.6635E-01 PERCENT ERROR= 0.0									
R016	MANE	0.26	328.36	495.24	3.00	5.00	328.33	495.00	3.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1394E+03 EXCESS=0.0000E+00 OUTFLOW=0.1394E+03 BASIN STORAGE=0.3874E-01 PERCENT ERROR= 0.0									
R015	MANE	0.19	329.29	495.12	2.99	5.00	329.25	495.00	3.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1399E+03 EXCESS=0.0000E+00 OUTFLOW=0.1399E+03 BASIN STORAGE=0.2812E-01 PERCENT ERROR= 0.0									



HEC1 S/N: 1343001909

HMVersion: 6.33

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Data File: C:\WINDOWS\TEMP\~vbh2A78.TMP

\*\*\*\*\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* MAY 1991 \*  
\* VERSION 4.0.1E \*  
\* RUN DATE 09/29/1999 TIME 09:54:02 \*  
\*\*\*\*\*

\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
\*\*\*\*\*

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X   X  XXXXXXX  XXXXX   X
X   X X         X   X   XX
X   X X         X       X
XXXXXXX XXXX   X       XXXXX X
X   X X         X       X
X   X X         X   X   X
X   X XXXXXXX  XXXXX   XXXX

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Full Microcomputer Implementation  
by  
Haestad Methods, Inc.

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10	
1	ID	HVL SWMP - Subbasin 4 - 25 Year Storm										
2	IT	5				283						
3	IO	5		0								
4	KK	0181										
5	KM	SCS 24 Hour Type IA Rainfall Subbasin 4.01.08.01										
6	KO	22										
7	BA	.0081										
8	FB	7										
9	IN	6										
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776	
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695	
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880	
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229	
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159	
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049	
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127	
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255	
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296	
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184	
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956	
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026	

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2914 KO            OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	283	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.083	TIME INTERVAL IN HOURS

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3061 KK            \*    HVLAKE    \*

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3063 KO            OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	283	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.083	TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				24-HOUR	72-HOUR				
HYDROGRAPH AT									
0181	5.	8.00	2.	1.	1.	0.01			
ROUTED TO									
R0181	5.	8.00	2.	1.	1.	0.01			
HYDROGRAPH AT									
018	427.	8.25	178.	90.	90.	0.86			
2 COMBINED AT									
018p	431.	8.17	180.	91.	91.	0.86			
ROUTED TO									
R018	430.	8.25	180.	91.	91.	0.86			
HYDROGRAPH AT									
017	3.	8.00	1.	1.	1.	0.01			
2 COMBINED AT									
017p	432.	8.25	181.	91.	91.	0.87			
ROUTED TO									
R017	432.	8.25	181.	91.	91.	0.87			
HYDROGRAPH AT									
016	2.	8.00	1.	0.	0.	0.00			
2 COMBINED AT									
016p	434.	8.25	182.	92.	92.	0.87			
ROUTED TO									
R016	434.	8.25	182.	92.	92.	0.87			
HYDROGRAPH AT									
015	2.	8.00	1.	0.	0.	0.00			
2 COMBINED AT									
015p	435.	8.25	183.	92.	92.	0.88			
ROUTED TO									
R015	435.	8.25	183.	92.	92.	0.88			
HYDROGRAPH AT									
0141	7.	8.00	2.	1.	1.	0.01			
ROUTED TO									
R0141	7.	8.00	2.	1.	1.	0.01			
HYDROGRAPH AT									
014	16.	8.00	5.	3.	3.	0.02			
3 COMBINED AT									
014p	450.	8.25	190.	96.	96.	0.90			

ROUTED TO  
R014

450.

8.25

190.

96.

96.

0.90

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HYDROGRAPH AT 0135	31.	8.00	11.	5.	5.	0.03
ROUTED TO R0135	31.	8.00	11.	5.	5.	0.03
HYDROGRAPH AT 01341	4.	8.00	1.	1.	1.	0.00
ROUTED TO R01341	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 01342	19.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 0134	12.	8.00	4.	2.	2.	0.01
4 COMBINED AT 0134p	67.	8.00	22.	11.	11.	0.07
ROUTED TO R0134	67.	8.00	22.	11.	11.	0.07
HYDROGRAPH AT 0133	19.	8.00	6.	3.	3.	0.02
2 COMBINED AT 0133p	86.	8.00	29.	14.	14.	0.08
ROUTED TO R0133	86.	8.00	29.	14.	14.	0.08
HYDROGRAPH AT 01321	5.	8.00	1.	1.	1.	0.00
ROUTED TO R01321	5.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0132	13.	8.00	4.	2.	2.	0.01
3 COMBINED AT 0132p	103.	8.00	34.	17.	17.	0.10
ROUTED TO R0132	103.	8.00	34.	17.	17.	0.10
HYDROGRAPH AT 0131	20.	8.00	7.	3.	3.	0.02
2 COMBINED AT 0131p	123.	8.00	41.	21.	21.	0.12
ROUTED TO R0131	122.	8.00	41.	21.	21.	0.12
HYDROGRAPH AT 013	12.	8.00	4.	2.	2.	0.01
3 COMBINED AT 013p	554.	8.17	235.	119.	119.	1.03
ROUTED TO R013	554.	8.17	235.	119.	119.	1.03
HYDROGRAPH AT 0122	29.	8.00	9.	5.	5.	0.02
ROUTED TO R0122	29.	8.00	9.	5.	5.	0.02
HYDROGRAPH AT 0121	15.	8.00	5.	3.	3.	0.01
2 COMBINED AT 0121p	44.	8.00	15.	7.	7.	0.04
ROUTED TO R0121	44.	8.00	15.	7.	7.	0.04
HYDROGRAPH AT 012	18.	8.00	6.	3.	3.	0.02
3 COMBINED AT 012p	605.	8.08	255.	129.	129.	1.09
ROUTED TO R012	603.	8.08	255.	129.	129.	1.09
HYDROGRAPH AT 0111	14.	8.00	5.	2.	2.	0.01
HYDROGRAPH AT 011	11.	8.00	4.	2.	2.	0.01

3 COMBINED AT 011p	625.	8.08	263.	133.	133.	1.11
ROUTED TO R011	620.	8.08	263.	133.	133.	1.11
HYDROGRAPH AT 1052	18.	8.00	6.	3.	3.	0.02
ROUTED TO R1052	18.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 1051	6.	8.00	2.	1.	1.	0.01
2 COMBINED AT 1051p	24.	8.00	8.	4.	4.	0.03
ROUTED TO R1051	24.	8.00	8.	4.	4.	0.03

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HYDROGRAPH AT 107	3.	8.00	1.	1.	1.	0.00
ROUTED TO R107	3.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 106	38.	8.00	13.	6.	6.	0.05
2 COMBINED AT 106p	41.	8.00	14.	7.	7.	0.06
ROUTED TO R106	41.	8.00	14.	7.	7.	0.06
HYDROGRAPH AT 105	13.	8.00	4.	2.	2.	0.02
3 COMBINED AT 105p	77.	8.00	26.	13.	13.	0.11
ROUTED TO R105	77.	8.00	26.	13.	13.	0.11
HYDROGRAPH AT 1043	2.	8.00	1.	0.	0.	0.00
ROUTED TO R1043	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1042	8.	8.00	3.	1.	1.	0.01
2 COMBINED AT 1043p	10.	8.00	3.	2.	2.	0.01
ROUTED TO R1042	10.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 1041	2.	8.00	1.	0.	0.	0.00
2 COMBINED AT 1041p	11.	8.00	4.	2.	2.	0.01
ROUTED TO R1041	11.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 104	8.	8.00	3.	1.	1.	0.01
3 COMBINED AT 104p	97.	8.00	33.	16.	16.	0.13
ROUTED TO R104	97.	8.00	33.	16.	16.	0.13
HYDROGRAPH AT 103	7.	8.00	2.	1.	1.	0.01
2 COMBINED AT 103p	104.	8.00	35.	18.	18.	0.14
ROUTED TO R103	104.	8.00	35.	18.	18.	0.14
HYDROGRAPH AT 1021	2.	8.00	1.	0.	0.	0.00
ROUTED TO R1021	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 102	11.	8.00	4.	2.	2.	0.01
3 COMBINED AT 102p	116.	8.00	39.	20.	20.	0.16
ROUTED TO R102	116.	8.00	39.	20.	20.	0.16
HYDROGRAPH AT 10121	3.	8.00	1.	1.	1.	0.00
ROUTED TO R10121	3.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 10122	3.	8.00	1.	1.	1.	0.00
ROUTED TO R10122	3.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 1012	3.	8.00	1.	1.	1.	0.00

3 COMBINED AT 1012p	12.	8.00	4.	2.	2.	0.02
ROUTED TO R1012	12.	8.00	4.	2.	2.	0.02
HYDROGRAPH AT 1011	7.	8.00	2.	1.	1.	0.01
ROUTED TO R1011	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 101	15.	8.00	5.	3.	3.	0.02
4 COMBINED AT 101p	150.	8.00	51.	26.	26.	0.20
ROUTED TO R101	150.	8.00	51.	26.	26.	0.20

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HYDROGRAPH AT 026	2.	8.00	1.	0.	0.	0.00
ROUTED TO R026	1.	8.08	1.	0.	0.	0.00
HYDROGRAPH AT 025	7.	8.00	2.	1.	1.	0.01
2 COMBINED AT 025p	8.	8.00	3.	1.	1.	0.01
ROUTED TO R025	8.	8.00	3.	1.	1.	0.01
HYDROGRAPH AT 0241	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0241	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 024	17.	8.00	6.	3.	3.	0.03
3 COMBINED AT 024p	30.	8.00	10.	5.	5.	0.05
ROUTED TO R024	30.	8.00	10.	5.	5.	0.05
HYDROGRAPH AT 0231	3.	8.00	1.	1.	1.	0.00
ROUTED TO R0231	3.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 023	26.	8.00	9.	5.	5.	0.04
3 COMBINED AT 023p	59.	8.00	20.	10.	10.	0.09
ROUTED TO R023	59.	8.00	20.	10.	10.	0.09
HYDROGRAPH AT 022	38.	8.00	13.	6.	6.	0.05
2 COMBINED AT 022p	96.	8.00	33.	17.	17.	0.14
ROUTED TO R022	96.	8.00	33.	17.	17.	0.14
HYDROGRAPH AT 021	46.	8.00	16.	8.	8.	0.07
2 COMBINED AT 021p	143.	8.00	48.	24.	24.	0.21
ROUTED TO R021	142.	8.00	48.	24.	24.	0.21
HYDROGRAPH AT 116	14.	8.00	5.	2.	2.	0.02
ROUTED TO R116	14.	8.00	5.	2.	2.	0.02
HYDROGRAPH AT 115	9.	8.00	3.	1.	1.	0.01
2 COMBINED AT 115p	23.	8.00	8.	4.	4.	0.03
ROUTED TO R115	23.	8.00	8.	4.	4.	0.03
HYDROGRAPH AT 114	11.	8.00	4.	2.	2.	0.01
2 COMBINED AT 114p	33.	8.00	11.	6.	6.	0.05
ROUTED TO R114	33.	8.00	11.	6.	6.	0.05
HYDROGRAPH AT 1132	3.	8.00	1.	0.	0.	0.00
ROUTED TO R1132	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1131	1.	8.00	0.	0.	0.	0.00



2 COMBINED AT 1131p	4.	8.00	1.	1.	1.	0.01
ROUTED TO R1131	4.	8.00	1.	1.	1.	0.01
HYDROGRAPH AT 113	3.	8.00	1.	1.	1.	0.00
3 COMBINED AT 113p	40.	8.00	14.	7.	7.	0.06
ROUTED TO R113	40.	8.00	14.	7.	7.	0.06
HYDROGRAPH AT 1121	11.	8.00	4.	2.	2.	0.02
ROUTED TO R1121	11.	8.00	4.	2.	2.	0.02

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HYDROGRAPH AT 112	2.	8.00	1.	0.	0.	0.00
3 COMBINED AT 112p	53.	8.00	18.	9.	9.	0.07
ROUTED TO R112	52.	8.00	18.	9.	9.	0.07
HYDROGRAPH AT 111	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1111	3.	8.00	1.	0.	0.	0.00
3 COMBINED AT 111p	58.	8.00	20.	10.	10.	0.08
ROUTED TO R111	58.	8.00	20.	10.	10.	0.08
HYDROGRAPH AT 043	28.	8.00	9.	5.	5.	0.04
HYDROGRAPH AT 0431	16.	8.00	5.	3.	3.	0.02
2 COMBINED AT 043p	45.	8.00	15.	7.	7.	0.06
ROUTED TO R043	44.	8.00	15.	7.	7.	0.06
HYDROGRAPH AT 042	43.	8.00	14.	7.	7.	0.05
2 COMBINED AT 042p	87.	8.00	29.	15.	15.	0.11
ROUTED TO R042	87.	8.00	29.	15.	15.	0.11
HYDROGRAPH AT 0411	12.	8.00	4.	2.	2.	0.01
ROUTED TO R0411	12.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 041	68.	8.00	22.	11.	11.	0.08
3 COMBINED AT 041p	167.	8.00	55.	28.	28.	0.21
ROUTED TO R041	167.	8.00	55.	28.	28.	0.21
HYDROGRAPH AT 031	3.	8.00	1.	0.	0.	0.00
ROUTED TO R031	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 0501	2.	8.00	1.	0.	0.	0.00
ROUTED TO R0501	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 0601	6.	8.00	2.	1.	1.	0.01
ROUTED TO R0601	6.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 0701	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0701	5.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 0801	5.	8.00	1.	1.	1.	0.00
ROUTED TO R0801	5.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0901	7.	8.00	2.	1.	1.	0.01
ROUTED TO R0901	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.01	6.	8.00	2.	1.	1.	0.01

HYDROGRAPH AT 4.04	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 4.02	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 4.03	6.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.05	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.06	6.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.07	6.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 4.08	5.	8.00	1.	1.	1.	0.00

HYDROGRAPH AT 4.09	9.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 4.10	11.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 4.11	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT WSS	1783.	8.33	811.	405.	405.	3.56
23 COMBINED AT HVLAKE	2752.	8.25	1277.	642.	642.	5.50

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0181	MANE	0.86	5.33	480.30	4.13	5.00	5.32	480.00	4.13
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1785E+01 EXCESS=0.0000E+00 OUTFLOW=0.1784E+01 BASIN STORAGE=0.1461E-02 PERCENT ERROR= 0.0									
R018	MANE	0.22	430.75	490.49	3.83	5.00	430.48	495.00	3.83
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1763E+03 EXCESS=0.0000E+00 OUTFLOW=0.1763E+03 BASIN STORAGE=0.3978E-01 PERCENT ERROR= 0.0									
R017	MANE	0.43	432.46	494.83	3.83	5.00	432.40	495.00	3.83
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1773E+03 EXCESS=0.0000E+00 OUTFLOW=0.1773E+03 BASIN STORAGE=0.7639E-01 PERCENT ERROR= 0.0									
R016	MANE	0.24	433.84	495.00	3.83	5.00	433.84	495.00	3.83
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1781E+03 EXCESS=0.0000E+00 OUTFLOW=0.1780E+03 BASIN STORAGE=0.4451E-01 PERCENT ERROR= 0.0									
R015	MANE	0.17	435.11	494.96	3.83	5.00	435.11	495.00	3.83
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1788E+03 EXCESS=0.0000E+00 OUTFLOW=0.1787E+03 BASIN STORAGE=0.3231E-01 PERCENT ERROR= 0.0									
R0141	MANE	2.67	7.43	480.58	6.37	5.00	7.41	480.00	6.38
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2420E+01 EXCESS=0.0000E+00 OUTFLOW=0.2415E+01 BASIN STORAGE=0.5921E-02 PERCENT ERROR= 0.0									
R014	MANE	0.71	450.57	491.39	3.88	5.00	450.19	495.00	3.89
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1865E+03 EXCESS=0.0000E+00 OUTFLOW=0.1864E+03 BASIN STORAGE=0.1466E+00 PERCENT ERROR= 0.0									
R0135	MANE	0.70	31.36	480.52	6.06	5.00	31.36	480.00	6.06
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1031E+02 EXCESS=0.0000E+00 OUTFLOW=0.1030E+02 BASIN STORAGE=0.6670E-02 PERCENT ERROR= 0.0									
R01341	MANE	2.20	4.46	479.88	7.24	5.00	4.46	480.00	7.24
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1432E+01 EXCESS=0.0000E+00 OUTFLOW=0.1429E+01 BASIN STORAGE=0.2681E-02 PERCENT ERROR= 0.0									
R0134	MANE	0.39	66.91	480.20	6.26	5.00	66.90	480.00	6.26
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2187E+02 EXCESS=0.0000E+00 OUTFLOW=0.2186E+02 BASIN STORAGE=0.7826E-02 PERCENT ERROR= 0.0									

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   MAY 1991
*   VERSION 4.0.1E
*
* RUN DATE 09/29/1999 TIME 13:11:09
*
*****
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
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X   X   XXXXXXX   XXXXX   X
X   X   X   X   X   X   XX
X   X   X   X   X   X   X
XXXXXXXX XXXX   X   XXXXX   X
X   X   X   X   X   X   X
X   X   X   X   X   X   X
X   X   XXXXXXX   XXXXX   XXX
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::::::::::::::::::::::::::::::::::::
:::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
:::
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::::::::::::::::::::::::::::::::::::
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID.....1.....2.....3..	4.....5.....6.....7.....8.....9.....10
1	ID HVL SWMP - Subbasin 4 -100 Year Storm	
2	IT 5	283
3	IO 5 0	
4	KK 0181	
5	KM SCS 24 Hour Type IA Rainfall Subbasin 4.01.08.01	
6	KO	22
7	BA .0081	
8	PB 9.5	
9	IN 6	
10	PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776	
11	PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695	
12	PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880	
13	PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229	
14	PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159	
15	PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049	
16	PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127	
17	PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.33142 0.35469 0.37876 0.40255	
18	PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296	
19	PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184	
20	PC 0.5770 0.58198 0.58685 0.59163 0.59635 0.60100 0.60576 0.61044 0.61504 0.61956	
21	PC 0.6240 0.62836 0.63264 0.63684 0.64096 0.64500 0.64889 0.65272 0.65651 0.66026	

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2914 KO            OUTPUT CONTROL VARIABLES

          IPRNT            5    PRINT CONTROL

          IPLOT            0    PLOT CONTROL

          QSCAL            0.    HYDROGRAPH PLOT SCALE

          IPNCH            0    PUNCH COMPUTED HYDROGRAPH

          IOUT            22    SAVE HYDROGRAPH ON THIS UNIT

          ISAV1            1    FIRST ORDINATE PUNCHED OR SAVED

          ISAV2            283    LAST ORDINATE PUNCHED OR SAVED

          TIMINT            0.083    TIME INTERVAL IN HOURS

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3061 KK            HVLAKE

\*\*\*\*\*

3063 KO            OUTPUT CONTROL VARIABLES

          IPRNT            5    PRINT CONTROL

          IPLOT            0    PLOT CONTROL

          QSCAL            0.    HYDROGRAPH PLOT SCALE

          IPNCH            0    PUNCH COMPUTED HYDROGRAPH

          IOUT            22    SAVE HYDROGRAPH ON THIS UNIT

          ISAV1            1    FIRST ORDINATE PUNCHED OR SAVED

          ISAV2            283    LAST ORDINATE PUNCHED OR SAVED

          TIMINT            0.083    TIME INTERVAL IN HOURS

RUNOFF SUMMARY

FLOW IN CUBIC FEET PER SECOND

TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT									
0181	8.	8.00	3.	1.	1.	0.01			
ROUTED TO									
R0181	8.	8.00	3.	1.	1.	0.01			
HYDROGRAPH AT									
018	705.	8.17	282.	141.	141.	0.86			
2 COMBINED AT									
018p	711.	8.17	285.	143.	143.	0.86			
ROUTED TO									
R018	710.	8.17	285.	143.	143.	0.86			
HYDROGRAPH AT									
017	5.	8.00	2.	1.	1.	0.01			
2 COMBINED AT									
017p	714.	8.17	287.	144.	144.	0.87			
ROUTED TO									
R017	712.	8.17	287.	143.	143.	0.87			
HYDROGRAPH AT									
016	4.	8.00	1.	1.	1.	0.00			
2 COMBINED AT									
016p	715.	8.17	288.	144.	144.	0.87			
ROUTED TO									
R016	714.	8.17	288.	144.	144.	0.87			
HYDROGRAPH AT									
015	3.	8.00	1.	1.	1.	0.00			
2 COMBINED AT									
015p	716.	8.17	289.	145.	145.	0.88			
ROUTED TO									
R015	716.	8.17	289.	145.	145.	0.88			
HYDROGRAPH AT									
0141	7.	8.00	2.	1.	1.	0.01			
ROUTED TO									
R0141	7.	8.00	2.	1.	1.	0.01			
HYDROGRAPH AT									
014	16.	8.00	5.	3.	3.	0.02			
3 COMBINED AT									
014p	734.	8.17	297.	149.	149.	0.90			

ROUTED TO  
R014

731. 8.17

297.

149.

149.

0.90

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HYDROGRAPH AT 0135	31.	8.00	11.	5.	5.	0.03
ROUTED TO R0135	31.	8.00	11.	5.	5.	0.03
HYDROGRAPH AT 01341	4.	8.00	1.	1.	1.	0.00
ROUTED TO R01341	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 01342	19.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 0134	12.	8.00	4.	2.	2.	0.01
4 COMBINED AT 0134p	67.	8.00	22.	11.	11.	0.07
ROUTED TO R0134	67.	8.00	22.	11.	11.	0.07
HYDROGRAPH AT 0133	19.	8.00	6.	3.	3.	0.02
2 COMBINED AT 0133p	86.	8.00	29.	14.	14.	0.08
ROUTED TO R0133	86.	8.00	29.	14.	14.	0.08
HYDROGRAPH AT 01321	5.	8.00	1.	1.	1.	0.00
ROUTED TO R01321	5.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0132	13.	8.00	4.	2.	2.	0.01
3 COMBINED AT 0132p	103.	8.00	34.	17.	17.	0.10
ROUTED TO R0132	103.	8.00	34.	17.	17.	0.10
HYDROGRAPH AT 0131	20.	8.00	7.	3.	3.	0.02
2 COMBINED AT 0131p	123.	8.00	41.	21.	21.	0.12
ROUTED TO R0131	122.	8.00	41.	21.	21.	0.12
HYDROGRAPH AT 013	12.	8.00	4.	2.	2.	0.01
3 COMBINED AT 013p	837.	8.17	342.	171.	171.	1.03
ROUTED TO R013	836.	8.17	342.	171.	171.	1.03
HYDROGRAPH AT 0122	29.	8.00	9.	5.	5.	0.02
ROUTED TO R0122	29.	8.00	9.	5.	5.	0.02
HYDROGRAPH AT 0121	15.	8.00	5.	3.	3.	0.01
2 COMBINED AT 0121p	44.	8.00	15.	7.	7.	0.04
ROUTED TO R0121	44.	8.00	15.	7.	7.	0.04
HYDROGRAPH AT 012	18.	8.00	6.	3.	3.	0.02
3 COMBINED AT 012p	883.	8.17	362.	182.	182.	1.09
ROUTED TO R012	882.	8.17	362.	181.	181.	1.09
HYDROGRAPH AT 0111	14.	8.00	5.	2.	2.	0.01
HYDROGRAPH AT 011	11.	8.00	4.	2.	2.	0.01



3 COMBINED AT 011p	900.	8.17	370.	186.	186.	1.11
ROUTED TO R011	900.	8.17	370.	186.	186.	1.11
HYDROGRAPH AT 1052	28.	8.00	9.	5.	5.	0.02
ROUTED TO R1052	28.	8.00	9.	5.	5.	0.02
HYDROGRAPH AT 1051	9.	8.00	3.	1.	1.	0.01
2 COMBINED AT 1051p	36.	8.00	12.	6.	6.	0.03
ROUTED TO R1051	36.	8.00	12.	6.	6.	0.03

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HYDROGRAPH AT 107	5.	8.00	2.	1.	1.	0.00
ROUTED TO R107	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 106	59.	8.00	19.	10.	10.	0.05
2 COMBINED AT 106p	63.	8.00	21.	11.	11.	0.06
ROUTED TO R106	63.	8.00	21.	11.	11.	0.06
HYDROGRAPH AT 105	20.	8.00	7.	3.	3.	0.02
3 COMBINED AT 105p	119.	8.00	39.	20.	20.	0.11
ROUTED TO R105	119.	8.00	39.	20.	20.	0.11
HYDROGRAPH AT 1043	3.	8.00	1.	0.	0.	0.00
ROUTED TO R1043	3.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 1042	12.	8.00	4.	2.	2.	0.01
2 COMBINED AT 1043p	14.	8.00	5.	2.	2.	0.01
ROUTED TO R1042	14.	8.00	5.	2.	2.	0.01
HYDROGRAPH AT 1041	3.	8.00	1.	0.	0.	0.00
2 COMBINED AT 1041p	17.	8.00	6.	3.	3.	0.01
ROUTED TO R1041	17.	8.00	6.	3.	3.	0.01
HYDROGRAPH AT 104	13.	8.00	4.	2.	2.	0.01
3 COMBINED AT 104p	149.	8.00	49.	25.	25.	0.13
ROUTED TO R104	149.	8.00	49.	25.	25.	0.13
HYDROGRAPH AT 103	11.	8.00	4.	2.	2.	0.01
2 COMBINED AT 103p	160.	8.00	53.	27.	27.	0.14
ROUTED TO R103	159.	8.00	53.	27.	27.	0.14
HYDROGRAPH AT 1021	3.	8.00	1.	0.	0.	0.00
ROUTED TO R1021	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 102	17.	8.00	6.	3.	3.	0.01
3 COMBINED AT 102p	179.	8.00	59.	30.	30.	0.16
ROUTED TO R102	179.	8.00	59.	30.	30.	0.16
HYDROGRAPH AT 10121	5.	8.00	2.	1.	1.	0.00
ROUTED TO R10121	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 10122	5.	8.00	2.	1.	1.	0.00
ROUTED TO R10122	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 1012	9.	8.00	3.	1.	1.	0.01

3 COMBINED AT 1012p	18.	8.00	6.	3.	3.	0.02
ROUTED TO R1012	18.	8.00	6.	3.	3.	0.02
HYDROGRAPH AT 1011	11.	8.00	4.	2.	2.	0.01
ROUTED TO R1011	11.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 101	23.	8.00	8.	4.	4.	0.02
4 COMBINED AT 101p	231.	8.00	77.	38.	38.	0.20
ROUTED TO R101	231.	8.00	77.	38.	38.	0.20

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HYDROGRAPH AT 026	2.	8.00	1.	0.	0.	0.00
ROUTED TO R026	2.	8.00	1.	0.	0.	0.00
HYDROGRAPH AT 025	11.	8.00	4.	2.	2.	0.01
2 COMBINED AT 025p	13.	8.00	4.	2.	2.	0.01
ROUTED TO R025	13.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT 0241	8.	8.00	3.	1.	1.	0.01
ROUTED TO R0241	8.	8.00	3.	1.	1.	0.01
HYDROGRAPH AT 024	26.	8.00	9.	4.	4.	0.03
3 COMBINED AT 024p	48.	8.00	16.	8.	8.	0.05
ROUTED TO R024	47.	8.00	16.	8.	8.	0.05
HYDROGRAPH AT 0231	5.	8.00	2.	1.	1.	0.00
ROUTED TO R0231	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 023	42.	8.00	14.	7.	7.	0.04
3 COMBINED AT 023p	94.	8.00	31.	16.	16.	0.09
ROUTED TO R023	94.	8.00	31.	16.	16.	0.09
HYDROGRAPH AT 022	59.	8.00	20.	10.	10.	0.05
2 COMBINED AT 022p	153.	8.00	51.	26.	26.	0.14
ROUTED TO R022	153.	8.00	51.	26.	26.	0.14
HYDROGRAPH AT 021	72.	8.00	24.	12.	12.	0.07
2 COMBINED AT 021p	225.	8.00	75.	38.	38.	0.21
ROUTED TO R021	224.	8.00	75.	38.	38.	0.21
HYDROGRAPH AT 116	22.	8.00	7.	4.	4.	0.02
ROUTED TO R116	22.	8.00	7.	4.	4.	0.02
HYDROGRAPH AT 115	13.	8.00	4.	2.	2.	0.01
2 COMBINED AT 115p	35.	8.00	12.	6.	6.	0.03
ROUTED TO R115	35.	8.00	12.	6.	6.	0.03
HYDROGRAPH AT 114	16.	8.00	5.	3.	3.	0.01
2 COMBINED AT 114p	51.	8.00	17.	9.	9.	0.05
ROUTED TO R114	51.	8.00	17.	9.	9.	0.05
HYDROGRAPH AT 1132	5.	8.00	2.	1.	1.	0.00
ROUTED TO R1132	5.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 1131	2.	8.00	1.	0.	0.	0.00

2 COMBINED AT 1131p	7.	8.00	2.	1.	1.	0.01
ROUTED TO R1131	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 113	5.	8.00	2.	1.	1.	0.00
3 COMBINED AT 113p	63.	8.00	21.	10.	10.	0.06
ROUTED TO R113	63.	8.00	21.	10.	10.	0.06
HYDROGRAPH AT 1121	17.	8.00	6.	3.	3.	0.02
ROUTED TO R1121	17.	8.00	6.	3.	3.	0.02

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HYDROGRAPH AT 112	2.	8.00	1.	0.	0.	0.00
3 COMBINED AT 112p	82.	8.00	27.	14.	14.	0.07
ROUTED TO R112	82.	8.00	27.	14.	14.	0.07
HYDROGRAPH AT 111	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 1111	4.	8.00	1.	1.	1.	0.00
3 COMBINED AT 111p	90.	8.00	30.	15.	15.	0.08
ROUTED TO R111	90.	8.00	30.	15.	15.	0.08
HYDROGRAPH AT 043	43.	8.00	14.	7.	7.	0.04
HYDROGRAPH AT 0431	24.	8.00	8.	4.	4.	0.02
2 COMBINED AT 043p	67.	8.00	22.	11.	11.	0.06
ROUTED TO R043	67.	8.00	22.	11.	11.	0.06
HYDROGRAPH AT 042	64.	8.00	21.	11.	11.	0.05
2 COMBINED AT 042p	131.	8.00	43.	22.	22.	0.11
ROUTED TO R042	131.	8.00	43.	22.	22.	0.11
HYDROGRAPH AT 0411	18.	8.00	6.	3.	3.	0.01
ROUTED TO R0411	18.	8.00	6.	3.	3.	0.01
HYDROGRAPH AT 041	102.	8.00	34.	17.	17.	0.08
3 COMBINED AT 041p	251.	8.00	83.	42.	42.	0.21
ROUTED TO R041	251.	8.00	83.	41.	41.	0.21
HYDROGRAPH AT 031	4.	8.00	1.	1.	1.	0.00
ROUTED TO R031	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0501	4.	8.00	1.	1.	1.	0.00
ROUTED TO R0501	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 0601	9.	8.00	3.	2.	2.	0.01
ROUTED TO R0601	9.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 0701	7.	7.92	2.	1.	1.	0.01
ROUTED TO R0701	7.	8.00	2.	1.	1.	0.01
HYDROGRAPH AT 0801	7.	7.92	2.	1.	1.	0.00
ROUTED TO R0801	7.	7.92	2.	1.	1.	0.00
HYDROGRAPH AT 0901	10.	8.00	3.	2.	2.	0.01
ROUTED TO R0901	10.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 4.01	10.	8.00	3.	2.	2.	0.01

HYDROGRAPH AT 4.04	4.	8.00	1.	1.	1.	0.00
HYDROGRAPH AT 4.02	6.	8.00	2.	1.	1.	0.00
HYDROGRAPH AT 4.03	9.	8.00	3.	1.	1.	0.01
HYDROGRAPH AT 4.05	10.	8.00	3.	2.	2.	0.01
HYDROGRAPH AT 4.06	9.	7.92	3.	1.	1.	0.01
HYDROGRAPH AT 4.07	9.	7.92	3.	2.	2.	0.01
HYDROGRAPH AT 4.08	7.	7.92	2.	1.	1.	0.00

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HYDROGRAPH AT 4.09	14.	8.00	5.	2.	2.	0.01
HYDROGRAPH AT 4.10	16.	8.00	5.	3.	3.	0.01
HYDROGRAPH AT 4.11	11.	8.00	4.	2.	2.	0.01
HYDROGRAPH AT WSS	2859.	8.33	1258.	627.	627.	3.56
23 COMBINED AT HVLAKE	4322.	8.25	1937.	969.	969.	5.50

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

INSTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO		VOLUME (IN)
							COMPUTATION PEAK (CFS)	INTERVAL TIME TO PEAK (MIN)	
R0181	MANE	0.77	8.48	479.79	6.38	5.00	8.48	480.00	6.38
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2760E+01 EXCESS=0.0000E+00 OUTFLOW=0.2758E+01 BASIN STORAGE=0.1905E-02 PERCENT ERROR= 0.0									
R018	MANE	0.20	711.30	490.23	6.02	5.00	710.36	490.00	6.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2772E+03 EXCESS=0.0000E+00 OUTFLOW=0.2771E+03 BASIN STORAGE=0.5181E-01 PERCENT ERROR= 0.0									
R017	MANE	0.37	714.01	490.41	6.02	5.00	712.18	490.00	6.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2788E+03 EXCESS=0.0000E+00 OUTFLOW=0.2787E+03 BASIN STORAGE=0.9948E-01 PERCENT ERROR= 0.0									
R016	MANE	0.21	714.98	490.43	6.02	5.00	713.87	490.00	6.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2800E+03 EXCESS=0.0000E+00 OUTFLOW=0.2799E+03 BASIN STORAGE=0.5776E-01 PERCENT ERROR= 0.0									
R015	MANE	0.15	716.41	490.19	6.02	5.00	715.55	490.00	6.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2810E+03 EXCESS=0.0000E+00 OUTFLOW=0.2810E+03 BASIN STORAGE=0.4193E-01 PERCENT ERROR= 0.0									
R0141	MANE	2.67	7.43	480.58	6.37	5.00	7.41	480.00	6.38
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2420E+01 EXCESS=0.0000E+00 OUTFLOW=0.2415E+01 BASIN STORAGE=0.5921E-02 PERCENT ERROR= 0.0									
R014	MANE	0.61	733.47	491.19	6.02	5.00	730.58	490.00	6.02
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2888E+03 EXCESS=0.0000E+00 OUTFLOW=0.2886E+03 BASIN STORAGE=0.1866E+00 PERCENT ERROR= 0.0									
R0135	MANE	0.70	31.36	480.52	6.06	5.00	31.36	480.00	6.06
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1031E+02 EXCESS=0.0000E+00 OUTFLOW=0.1030E+02 BASIN STORAGE=0.6670E-02 PERCENT ERROR= 0.0									
R01341	MANE	2.20	4.46	479.88	7.24	5.00	4.46	480.00	7.24
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1432E+01 EXCESS=0.0000E+00 OUTFLOW=0.1429E+01 BASIN STORAGE=0.2681E-02 PERCENT ERROR= 0.0									
R0134	MANE	0.39	66.91	480.20	6.26	5.00	66.90	480.00	6.26
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2187E+02 EXCESS=0.0000E+00 OUTFLOW=0.2186E+02 BASIN STORAGE=0.7826E-02 PERCENT ERROR= 0.0									



HEC1 S/N: 1343001909

HMVersion: 6.33 Data File: C:\WINDOWS\TEMP\vbh3B03.TMP

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FLOOD HYDROGRAPH PACKAGE (HEC-1)
MAY 1991
VERSION 4.0.1E
RUN DATE 07/21/1999 TIME 11:22:53

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

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Full Microcomputer Implementation
by
Haestad Methods, Inc.

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

Table with columns: LINE, ID, and numerical values. Includes subbasin information and a grid of numerical data for lines 10-19.

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152 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD		BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
24-HOUR	72-HOUR							
HYDROGRAPH AT 0200	656.	8.42	297.	147.	147.	1.46		
ROUTED TO R0200	655.	8.47	297.	146.	146.	1.46		
HYDROGRAPH AT 0102	40.	7.92	13.	7.	7.	0.07		
2 COMBINED AT P0102	672.	8.45	310.	153.	153.	1.53		
ROUTED TO R0102	672.	8.53	310.	152.	152.	1.53		
HYDROGRAPH AT 0101	4.	7.90	1.	1.	1.	0.01		
ROUTED TO R0101	4.	7.93	1.	1.	1.	0.01		
HYDROGRAPH AT 0000	95.	8.47	50.	26.	26.	0.40		
3 COMBINED AT 5.0	768.	8.53	360.	179.	179.			

1.94

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)
							PEAK (CFS)	TIME TO PEAK (MIN)	
R0200	MANE	1.00	655.44	508.00	3.72	1.00	655.44	508.00	3.72

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2911E+03 EXCESS=0.0000E+00 OUTFLOW=0.2903E+03 BASIN STORAGE=0.8654E+00 PERCENT ERROR= 0.0

R0102 MANE 1.00 671.83 512.00 3.70 1.00 671.83 512.00 3.70

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3035E+03 EXCESS=0.0000E+00 OUTFLOW=0.3022E+03 BASIN STORAGE=0.1480E+01 PERCENT ERROR= 0.0

R0101 MANE 1.00 3.78 476.00 3.21 1.00 3.78 476.00 3.21

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1285E+01 EXCESS=0.0000E+00 OUTFLOW=0.1283E+01 BASIN STORAGE=0.2649E-02 PERCENT ERROR= 0.0

\*\*\* NORMAL END OF HEC-1 \*\*\*

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA5\5-YEAR25.OUT  
Data File: C:\WINDOWS\TEMP\vbh1005.TMP

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\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* MAY 1991 \*  
\* VERSION 4.0.1E \*  
\* RUN DATE 09/29/1999 TIME 09:46:30 \*  
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\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
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:: Full Microcomputer Implementation ::  
:: by ::  
:: Haestad Methods, Inc. ::  
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.....

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

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HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
1 ID HVL SWMP - Subbasing 5 - 25 Year Storm  
2 IT 1 1440  
3 IO 5 0  
4 KK 0200  
5 KM SCS 24 Hour Type IA Rainfall Subbasin 5.02.00  
6 KO 22  
7 BA 1.4641  
8 PB 7  
9 IN 6  
10 PC 0.0000 0.00224 0.00432 0.00628 0.00816 0.01000 0.01184 0.01372 0.01568 0.01776  
11 PC 0.0200 0.02276 0.02568 0.02872 0.03184 0.03500 0.03797 0.04095 0.04394 0.04695  
12 PC 0.0500 0.05315 0.05633 0.05954 0.06276 0.06600 0.06920 0.07240 0.07560 0.07880  
13 PC 0.0820 0.08514 0.08829 0.09147 0.09471 0.09800 0.10147 0.10502 0.10862 0.11229  
14 PC 0.1160 0.11969 0.12342 0.12721 0.13107 0.13500 0.13901 0.14310 0.14729 0.15159  
15 PC 0.1560 0.16059 0.16530 0.17011 0.17501 0.18000 0.18494 0.18999 0.19517 0.20049  
16 PC 0.2060 0.21196 0.21808 0.22432 0.23064 0.23700 0.24285 0.24878 0.25490 0.26127  
17 PC 0.2680 0.27517 0.28287 0.29118 0.30019 0.31000 0.33142 0.35469 0.37876 0.40255  
18 PC 0.4250 0.43936 0.45168 0.46232 0.47164 0.48000 0.48904 0.49752 0.50548 0.51296  
19 PC 0.5200 0.52664 0.53292 0.53888 0.54456 0.55000 0.55564 0.56116 0.56656 0.57184  
20 PC 0.5770 0.58198 0.58685 0.59163 0.59635 0.60100 0.60576 0.61044 0.61504 0.61956  
21 PC 0.6240 0.62836 0.63264 0.63684 0.64096 0.64500 0.64889 0.65272 0.65651 0.66026

K:\RICKJ\GHEC1\99205301\AREA5\5-YEAR25.OUT  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

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301 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT 0200	828.	8.42	369.	182.	182.	1.46			
ROUTED TO R0200	828.	8.45	369.	182.	182.	1.46			
HYDROGRAPH AT 0102	51.	7.92	17.	8.	8.	0.07			
HYDROGRAPH AT WS 6	904.	8.17	358.	179.	179.	1.62			
3 COMBINED AT P0102	1653.	8.28	743.	370.	370.	3.15			
ROUTED TO R0102	1652.	8.35	743.	368.	368.	3.15			
HYDROGRAPH AT 0101	5.	7.90	2.	1.	1.	0.01			
ROUTED TO R0101	5.	7.93	2.	1.	1.	0.01			
HYDROGRAPH AT 0000	134.	8.45	67.	34.	34.	0.40			
3 COMBINED AT 5.0	1785.	8.35	811.	403.	403.	3.56			

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME	
						DT	PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0200	MANE	1.00	827.61	507.00	4.62	1.00	827.61	507.00	4.62

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3614E+03 EXCESS=0.0000E+00 OUTFLOW=0.3605E+03 BASIN STORAGE=0.9863E+00 PERCENT ERROR= 0.0

R0102 MANE 1.00 1652.03 501.00 4.34 1.00 1652.03 501.00 4.34

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7326E+03 EXCESS=0.0000E+00 OUTFLOW=0.7301E+03 BASIN STORAGE=0.2836E+01 PERCENT ERROR= 0.0

R0101 MANE 1.00 4.91 476.00 4.06 1.00 4.91 476.00 4.06

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1629E+01 EXCESS=0.0000E+00 OUTFLOW=0.1626E+01 BASIN STORAGE=0.3052E-02 PERCENT ERROR= 0.0

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREAS\5-YR100.OUT  
Data File: C:\WINDOWS\TEMP\vbh1C00.TMP

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\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* MAY 1991 \*  
\* VERSION 4.0.1E \*  
\* RUN DATE 09/29/1999 TIME 13:07:31 \*  
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\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
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X   X  X      X   X      XX
X   X  X      X   X      X
XXXXXXX XXXX  X   XXXXX  X
X   X  X      X   X      X
X   X  X      X   X      X
X   X  XXXXXXX  XXXXX      XXX

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Full Microcomputer Implementation  
by  
Haestad Methods, Inc.

37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subbasin 5 - 100 Year Storm									
2	IT	1 1440									
3	IO	5 0									
4	KK	0200									
5	KM	SCS 24 Hour Type IA Rainfall Subbasin 5.02.00									
6	KO	22									
7	BA	1.4641									
8	PB	9.5									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026

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IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

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 \* 5.0 \*  
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301 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK 6-HOUR	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				24-HOUR	72-HOUR				
HYDROGRAPH AT 0200	1268.	8.40	555.	274.	274.	1.46			
ROUTED TO R0200	1267.	8.43	555.	273.	273.	1.46			
HYDROGRAPH AT 0102	77.	7.92	25.	12.	12.	0.07			
HYDROGRAPH AT WS6	1487.	8.15	565.	281.	281.	1.62			
3 COMBINED AT P0102	2626.	8.25	1144.	567.	567.	3.15			
ROUTED TO R0102	2624.	8.30	1144.	565.	565.	3.15			
HYDROGRAPH AT 0101	8.	7.90	3.	1.	1.	0.01			
ROUTED TO R0101	8.	7.92	3.	1.	1.	0.01			
HYDROGRAPH AT 0000	239.	8.43	112.	56.	56.	0.40			
3 COMBINED AT 5.0	2860.	8.32	1258.	622.	622.	3.56			

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)
							PEAK (CFS)	TIME TO PEAK (MIN)	
R0200	MANE	1.00	1267.08	506.00	6.93	1.00	1267.08	506.00	6.93

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5423E+03 EXCESS=0.0000E+00 OUTFLOW=0.5412E+03 BASIN STORAGE=0.1266E+01 PERCENT ERROR= 0.0

R0102	MANE	1.00	2624.39	498.00	6.66	1.00	2624.39	498.00	6.66
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CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1124E+04 EXCESS=0.0000E+00 OUTFLOW=0.1120E+04 BASIN STORAGE=0.3671E+01 PERCENT ERROR= 0.0

R0101	MANE	1.00	7.86	475.00	6.31	1.00	7.86	475.00	6.31
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CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2529E+01 EXCESS=0.0000E+00 OUTFLOW=0.2525E+01 BASIN STORAGE=0.3984E-02 PERCENT ERROR= 0.0







ROUTED TO R0300	199.	8.25	83.	42.	42.	0.54
HYDROGRAPH AT 0203	4.	8.00	1.	1.	1.	0.01
ROUTED TO R0203	4.	8.03	1.	1.	1.	0.01

K:\RICKJ\GHEC1\99205301\AREA6\6-00.OUT

HYDROGRAPH AT 0202	2.	8.00	1.	0.	0.	0.00
2 COMBINED AT P0202	5.	8.02	2.	1.	1.	0.01
ROUTED TO R0202	5.	8.02	2.	1.	1.	0.01
HYDROGRAPH AT 0201	2.	7.98	1.	0.	0.	0.00
HYDROGRAPH AT 020101	1.	8.98	1.	0.	0.	0.00
3 COMBINED AT P0201	8.	8.02	3.	2.	2.	0.02
ROUTED TO R0201	8.	8.08	3.	2.	2.	0.02
HYDROGRAPH AT 0200	43.	8.00	15.	7.	7.	0.08
2 COMBINED AT P0200	51.	8.00	18.	9.	9.	0.10
ROUTED TO R0200	51.	8.08	18.	9.	9.	0.10
HYDROGRAPH AT 0102	2.	7.95	1.	0.	0.	0.00
ROUTED TO R0102	2.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 0101	2.	7.95	1.	0.	0.	0.00
2 COMBINED AT P0101	4.	7.97	1.	1.	1.	0.01
ROUTED TO R0101	4.	8.03	1.	1.	1.	0.01
HYDROGRAPH AT 0100	20.	7.97	7.	3.	3.	0.03
2 COMBINED AT P0100	24.	7.97	8.	4.	4.	0.04
ROUTED TO R0100	24.	8.05	8.	4.	4.	0.04
HYDROGRAPH AT 0000	420.	8.18	170.	86.	86.	1.05
4 COMBINED AT 6.0	683.	8.18	279.	141.	141.	1.72

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		
							PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)
R0601	MANE	1.00	0.66	481.00	3.26	1.00	0.66	481.00	3.26
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2267E+00 EXCESS=0.0000E+00 OUTFLOW=0.2263E+00 BASIN STORAGE=0.4231E-03 PERCENT ERROR= 0.0									
R0602	MANE	0.99	8.07	480.71	3.03	1.00	8.07	481.00	3.04
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2851E+01 EXCESS=0.0000E+00 OUTFLOW=0.2849E+01 BASIN STORAGE=0.2803E-02 PERCENT ERROR= 0.0									
R0600	MANE	1.00	12.74	493.00	3.06	1.00	12.74	493.00	3.06
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4467E+01 EXCESS=0.0000E+00 OUTFLOW=0.4395E+01 BASIN STORAGE=0.8313E-01 PERCENT ERROR= -0.2									
R0500	MANE	0.50	140.10	491.91	2.90	1.00	140.10	492.00	2.90
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5733E+02 EXCESS=0.0000E+00 OUTFLOW=0.5730E+02 BASIN STORAGE=0.3125E-01 PERCENT ERROR= 0.0									
R0400	MANE	1.00	141.88	496.00	2.88	1.00	141.88	496.00	2.88
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5733E+02 EXCESS=0.0000E+00 OUTFLOW=0.5730E+02 BASIN STORAGE=0.3125E-01 PERCENT ERROR= 0.0									

HEC1 S/N: 1343001909

HMVersion: 6.33

K:\RICKJ\GHEC1\99205301\AREA6\6-YEAR25.OUT  
Data File: C:\WINDOWS\TEMP\vbh180P.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 09/29/1999 TIME 09:28:34 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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*****
*****
Full Microcomputer Implementation
by
Haestad Methods, Inc.
*****
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE PORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
1	ID	HVL SWMP - Subasin 6 - 25 Year Storm									
2	IT	1		1440							
3	IO	5		0							
4	KK	0601									
5	KM	SCS 24 Hour Type IA Rainfall - Subbasin 6.06.01									
6	KO	22									
7	BA	.0013									
8	PB	7									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026

728 KK \*\*\*\*\*  
 \* 6.0 \*  
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730 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IFNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 1440 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT 0.017 TIME INTERVAL IN HOURS

OPERATION	STATION	PEAK FLOW	RUNOFF SUMMARY			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
			TIME OF PEAK 6-HOUR	FLOW IN CUBIC FEET PER SECOND				
				AVERAGE FLOW	FOR MAXIMUM PERIOD			
HYDROGRAPH AT 0601	1.	7.97	0.	0.	0.	0.00		
ROUTED TO R0601	1.	8.00	0.	0.	0.	0.00		
HYDROGRAPH AT 0602	11.	8.00	4.	2.	2.	0.02		
ROUTED TO R0602	11.	8.00	4.	2.	2.	0.02		
HYDROGRAPH AT 0600	5.	7.98	2.	1.	1.	0.01		
3 COMBINED AT P0600	17.	8.00	6.	3.	3.	0.03		
ROUTED TO R0600	17.	8.20	6.	3.	3.	0.03		
HYDROGRAPH AT 0500	170.	8.18	68.	34.	34.	0.34		
2 COMBINED AT P0500	187.	8.18	74.	37.	37.	0.37		
ROUTED TO R0500	187.	8.18	74.	37.	37.	0.37		
HYDROGRAPH AT 0400	3.	8.02	1.	1.	1.	0.01		
2 COMBINED AT P0400	189.	8.18	75.	38.	38.	0.38		
ROUTED TO R0400	189.	8.25	75.	37.	37.	0.38		
HYDROGRAPH AT 030301	29.	7.98	10.	5.	5.	0.04		
ROUTED TO R030301	29.	7.98	10.	5.	5.	0.04		
HYDROGRAPH AT 0303	10.	7.97	3.	2.	2.	0.02		
2 COMBINED AT P0303	39.	7.98	13.	7.	7.	0.06		
ROUTED TO R0303	39.	8.08	13.	7.	7.	0.06		
HYDROGRAPH AT 0302	6.	7.97	2.	1.	1.	0.01		
ROUTED TO R0302	6.	8.05	2.	1.	1.	0.01		
HYDROGRAPH AT 0301	0.	7.93	0.	0.	0.	0.00		
ROUTED TO R0301	0.	8.05	0.	0.	0.	0.00		
HYDROGRAPH AT 0300	48.	8.03	17.	9.	9.	0.10		
5 COMBINED AT P0300	266	8.17	107	54	54	0.54		

ROUTED TO R0300	266.	8.22	107.	54.	54.	0.54
HYDROGRAPH AT 0203	5.	8.00	2.	1.	1.	0.01
ROUTED TO R0203	5.	8.02	2.	1.	1.	0.01

K:\RICKJ\GHEC1\99205301\AREA6\6-YEAR25.OUT

HYDROGRAPH AT 0202	2.	7.98	1.	0.	0.	0.00
2 COMBINED AT P0202	7.	8.00	2.	1.	1.	0.01
ROUTED TO R0202	7.	8.02	2.	1.	1.	0.01
HYDROGRAPH AT 0201	3.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 020101	1.	8.97	1.	0.	0.	0.00
3 COMBINED AT P0201	10.	8.02	4.	2.	2.	0.02
ROUTED TO R0201	10.	8.07	4.	2.	2.	0.02
HYDROGRAPH AT 0200	56.	7.98	19.	9.	9.	0.08
2 COMBINED AT P0200	66.	8.00	23.	11.	11.	0.10
ROUTED TO R0200	66.	8.07	23.	11.	11.	0.10
HYDROGRAPH AT 0102	2.	7.95	1.	0.	0.	0.00
ROUTED TO R0102	2.	7.97	1.	0.	0.	0.00
HYDROGRAPH AT 0101	3.	7.95	1.	0.	0.	0.00
2 COMBINED AT P0101	5.	7.95	2.	1.	1.	0.01
ROUTED TO R0101	5.	8.03	2.	1.	1.	0.01
HYDROGRAPH AT 0100	25.	7.95	8.	4.	4.	0.03
2 COMBINED AT P0100	30.	7.97	10.	5.	5.	0.04
ROUTED TO R0100	30.	8.03	10.	5.	5.	0.04
HYDROGRAPH AT 0000	554.	8.18	218.	110.	110.	1.05
4 COMBINED AT 6.0	904.	8.17	358.	179.	179.	1.72

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO		VOLUME (IN)
							COMPUTATION PEAK (CFS)	INTERVAL TIME TO PEAK (MIN)	
R0601	MANE	1.00	0.85	480.00	4.13	1.00	0.85	480.00	4.13
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2867E+00 EXCESS=0.0000E+00 OUTFLOW=0.2862E+00 BASIN STORAGE=0.4859E-03 PERCENT ERROR= 0.0									
R0602	MANE	0.92	10.62	480.51	3.87	1.00	10.61	480.00	3.87
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3640E+01 EXCESS=0.0000E+00 OUTFLOW=0.3637E+01 BASIN STORAGE=0.3232E-02 PERCENT ERROR= 0.0									
R0600	MANE	1.00	16.68	492.00	3.90	1.00	16.68	492.00	3.90
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5684E+01 EXCESS=0.0000E+00 OUTFLOW=0.5603E+01 BASIN STORAGE=0.9490E-01 PERCENT ERROR= -0.2									
R0500	MANE	0.46	186.92	491.45	3.72	1.00	186.87	491.00	3.72
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7356E+02 EXCESS=0.0000E+00 OUTFLOW=0.7352E+02 BASIN STORAGE=0.3587E-01 PERCENT ERROR= 0.0									
R0400	MANE	1.00	189.30	495.00	3.70	1.00	189.30	495.00	3.70
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7463E+02 EXCESS=0.0000E+00 OUTFLOW=0.7426E+02 BASIN STORAGE=0.4378E+00 PERCENT ERROR= -0.1									

HEC1 S/N: 1343001909

HMVersion: 6.33

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Data File: C:\WINDOWS\TEMP\vbh0A1D.TMP

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   MAY 1991 *
*   VERSION 4.0.1E *
* RUN DATE 09/29/1999 TIME 13:04:22 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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: Full Microcomputer Implementation :
: by :
: Haestad Methods, Inc. :
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37 Brookside Road \* Waterbury, Connecticut 06708 \* (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HVL SWMP - Subbasin 6 - 100 Year Storm									
2	IT	1 1440									
3	IO	5 0									
4	KK	0601									
5	KM	SCS 24 Hour Type IA Rainfall - Subbasin 6.06.01									
6	KO	22									
7	BA	.0013									
8	PB	9.5									
9	IN	6									
10	PC	0.0000	0.00224	0.00432	0.00628	0.00816	0.01000	0.01184	0.01372	0.01568	0.01776
11	PC	0.0200	0.02276	0.02568	0.02872	0.03184	0.03500	0.03797	0.04095	0.04394	0.04695
12	PC	0.0500	0.05315	0.05633	0.05954	0.06276	0.06600	0.06920	0.07240	0.07560	0.07880
13	PC	0.0820	0.08514	0.08829	0.09147	0.09471	0.09800	0.10147	0.10502	0.10862	0.11229
14	PC	0.1160	0.11969	0.12342	0.12721	0.13107	0.13500	0.13901	0.14310	0.14729	0.15159
15	PC	0.1560	0.16059	0.16530	0.17011	0.17501	0.18000	0.18494	0.18999	0.19517	0.20049
16	PC	0.2060	0.21196	0.21808	0.22432	0.23064	0.23700	0.24285	0.24878	0.25490	0.26127
17	PC	0.2680	0.27517	0.28287	0.29118	0.30019	0.31000	0.33142	0.35469	0.37876	0.40255
18	PC	0.4250	0.43936	0.45168	0.46232	0.47164	0.48000	0.48904	0.49752	0.50548	0.51296
19	PC	0.5200	0.52664	0.53292	0.53888	0.54456	0.55000	0.55564	0.56116	0.56656	0.57184
20	PC	0.5770	0.58198	0.58685	0.59163	0.59635	0.60100	0.60576	0.61044	0.61504	0.61956
21	PC	0.6240	0.62836	0.63264	0.63684	0.64096	0.64500	0.64889	0.65272	0.65651	0.66026





ROUTED TO R0300	446.	8.18	171.	85.	85.	0.54
HYDROGRAPH AT 0203	8.	7.97	3.	1.	1.	0.01
ROUTED TO R0203	8.	8.00	3.	1.	1.	0.01

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HYDROGRAPH AT 0202	4.	7.97	1.	1.	1.	0.00
2 COMBINED AT P0202	12.	7.98	4.	2.	2.	0.01
ROUTED TO R0202	12.	7.98	4.	2.	2.	0.01
HYDROGRAPH AT 0201	4.	7.95	1.	1.	1.	0.00
HYDROGRAPH AT 020101	2.	8.92	1.	1.	1.	0.00
3 COMBINED AT P0201	17.	8.00	7.	3.	3.	0.02
ROUTED TO R0201	17.	8.05	7.	3.	3.	0.02
HYDROGRAPH AT 0200	88.	7.95	29.	14.	14.	0.08
2 COMBINED AT P0200	105.	7.97	35.	18.	18.	0.10
ROUTED TO R0200	105.	8.05	35.	18.	18.	0.10
HYDROGRAPH AT 0102	3.	7.93	1.	0.	0.	0.00
ROUTED TO R0102	3.	7.95	1.	0.	0.	0.00
HYDROGRAPH AT 0101	4.	7.95	1.	1.	1.	0.00
2 COMBINED AT P0101	7.	7.95	2.	1.	1.	0.01
ROUTED TO R0101	7.	8.02	2.	1.	1.	0.01
HYDROGRAPH AT 0100	37.	7.95	12.	6.	6.	0.03
2 COMBINED AT P0100	44.	7.95	14.	7.	7.	0.04
ROUTED TO R0100	44.	8.02	14.	7.	7.	0.04
HYDROGRAPH AT 0000	908.	8.17	345.	172.	172.	1.05
4 COMBINED AT 6.0	1487.	8.15	565.	281.	281.	1.72

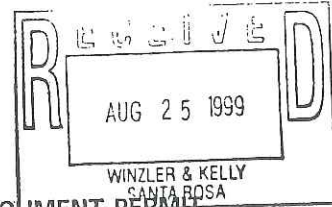
SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			VOLUME
						DT	PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
R0601	MANE	1.00	1.36	479.00	6.38	1.00	1.36	479.00	6.38
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4432E+00 EXCESS=0.0000E+00 OUTFLOW=0.4427E+00 BASIN STORAGE=0.6309E-03 PERCENT ERROR= 0.0									
R0602	MANE	0.81	17.34	479.13	6.08	1.00	17.34	479.00	6.08
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5715E+01 EXCESS=0.0000E+00 OUTFLOW=0.5711E+01 BASIN STORAGE=0.4224E-02 PERCENT ERROR= 0.0									
R0600	MANE	1.00	27.04	489.00	6.11	1.00	27.04	489.00	6.11
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8876E+01 EXCESS=0.0000E+00 OUTFLOW=0.8773E+01 BASIN STORAGE=0.1217E+00 PERCENT ERROR= -0.2									
R0500	MANE	0.39	311.46	490.44	5.89	1.00	311.34	491.00	5.89
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1164E+03 EXCESS=0.0000E+00 OUTFLOW=0.1164E+03 BASIN STORAGE=0.4642E-01 PERCENT ERROR= 0.0									
R0400	MANE	1.00	315.50	494.00	5.87	1.00	315.50	494.00	5.87
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1164E+03 EXCESS=0.0000E+00 OUTFLOW=0.1164E+03 BASIN STORAGE=0.4642E-01 PERCENT ERROR= 0.0									

## **APPENDIX B - ENCROACHMENT STANDARDS**

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**INSTRUCTIONS FOR APPLYING FOR A DRIVEWAY ENCROACHMENT PERMIT**

**NON COUNTY-MAINTAINED ROADS**

A portion of the roads (streets and easements) in Lake County have not been taken into the County-maintained System and are therefore classified as Non County-maintained Roads. If your driveway will be constructed on a Non County-maintained road, you do not require an Encroachment Permit from the County and the Department of Public Works will sign your Building Permit Application check-off sheet as "Encroachment Permit Not Required".

**COUNTY-MAINTAINED ROADS**

On County-maintained roads, streets, highways and easements, encroachment permits are required as follows:

- Any new driveway construction
- Modular home lot preparations
- Replacement of modular homes
- Construction of dwellings or structures that exceed 500 square feet and require building permits.
- Construction of agricultural structures that exceed 500 square feet. There is no agricultural exemption.
- Additions to structures, including carports, that exceed 500 square feet and require building permits.

**INSTRUCTIONS FOR COMPLETING A DRIVEWAY ENCROACHMENT PERMIT APPLICATION**

- A. At the top of the application provide the owner's and contractor's name, address, site information, etc. as requested.
- B. Draw a location map, or provide written directions to the site, in the box on the right side of the application form (include nearest cross street and distance to the lot).
- C. Write the following information in the box entitled, "PLAN AND PROFILE" on the application form.
  1. **PLAN VIEW OF DRIVEWAY:** If your driveway intersects the County road at ninety degrees (90°) perpendicular to the County road, choose one of the three options shown on Drawing R9-7. Then write "R9-7, Option #1" (or #2 or #3) in the box entitled "Plan & Profile" on the left side of the Encroachment Permit Application.

- OR -

Drawing R9-9 shows two options for a driveway not intersecting the County road at 90°. One option is for driveways intersecting the road at an angle between 60° and 89°, and the other for intersecting the road at an angle between 91° and 120°. Either option may be used, provided the slope of the 20 feet long driveway encroachment is laid out perpendicular (90°) to the edge of the road as shown in the two examples on the back of Drawing R9-9. If you wish to use one of these two angle driveway options, write "R9-9, 60° Option" (or 70, 120 or whatever angle you wish to use) in the box entitled "Plan & Profile" on the left side of the Encroachment Permit Application.

2. **PROFILE (Elevations) OF DRIVEWAY:** Choose the profile that applies to your driveway from Standard Drawings R9-1A, R9-1D, R9-2A or R9-2D. In the box on the left side of the Encroachment Permit Application, write "R9-1A" (or R9-1D, 2A or 2D; the four Standard Drawings show the maximum slopes permitted by the County Standards).

Encroachment Instructions  
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3. **PAVING AND DRAINAGE:** Drawing R9-6 shows the County requirements for paving (including base/sand compaction and reinforcement details) and drainage culverts. If your driveway requires fill that will block an existing roadside drainage ditch or block any drainage that flows across the first 20 feet of your driveway, you may be required to install a culvert pipe. The minimum culvert diameter is 12 inches. A larger diameter culvert may be required, depending on the size of the upstream drainage area. The Inspector will determine the need for a culvert at the preliminary inspection.

D. Draw your actual driveway profile on the sheet provided. Start at the top edge of the existing pavement of the road along the profile of the existing ground, to a point 20 feet out from said edge of pavement of the road.

The profile you selected under Item C2 above was for either Standard Drawing R9-1A, R9-1D, R9-2A or R9-2D. *Those drawings show the maximum or steepest driveway slope permitted by the standards.* If you are using the steepest slope permitted, draw the slopes, distances and elevations shown on the profile drawing you chose; then draw the profile of the existing ground. If the slope of your driveway will be less than the steepest driveway slopes permitted, draw the profile of what your driveway slope will actually be. If you need to go to your building site and look at your driveway location in order to draw the profile of the existing ground and driveway, you may take the profile sheet with you. Public Works will review the completed profile sheet when you return to pay the Encroachment Permit fee.

The profile sheet also has sign-off lines for the local fire protection agency. If any part of the first twenty feet (20') of your driveway has a slope steeper than sixteen percent (16%) you will need the profile sheet signed off by:

1. The California Division of Forestry, if your proposed driveway encroachment is in the State (fire protection) responsibility area; and/or
2. One of the following Fire Protection Districts, dependent upon where your proposed driveway encroachment is located:

Clearlake Oaks-Glenhaven  
Kelseyville  
Lakeport County  
Lakeshore  
Lower Lake

Lucerne Park & Recreation  
Nice Community Service  
South Lake  
Upper Lake

3. You may sign off on the profile sheet if any part of the driveway slope in the first 20 feet will not exceed 16%, and Public Works will accept your signature in lieu of the California Division of Forestry or Fire Protection District sign-offs.

**IDENTIFY YOUR DRIVEWAY**

Drive a wood or metal stake at each side of your driveway approach and tie colored ribbon to the stakes, or mark location on the ground with paint. REMEMBER: A CLEAR LINE OF SITE AND VISIBILITY SHOULD BE A CONSIDERATION FOR YOUR DRIVEWAY LOCATION TO ALLOW FOR SAFE INGRESS AND EGRESS. Post the address of the property on the stakes or erect a sign to show the address and/or property owner's name. If you place an empty coffee can (with lid) or a similar container beside one of the stakes, the County Inspector will leave a card showing the date and results of each inspection. You may also phone (707) 263-2341 for information about your driveway inspection.

**OTHER STANDARDS AVAILABLE:**

- A. **Existing Curbs and Sidewalks:** If you are planning to construct a residential or commercial driveway across an existing curb, gutter and sidewalk, ask the Department of Public Works for a copy of Drawing R9-4C and R9-4NC.
- B. **Commercial Driveways:** If you are going to construct a commercial driveway, ask for a copy of Drawings R9-4C and R9-4NC. You can use those two standard drawings for most commercial driveways; but for the largest and busiest commercial driveways, additional width and other features to aid turning trucks will be required.
- C. **Setting Garages Closer to the Road:** Standard Drawing R9-17 shows an exception in the Zoning Ordinance that allows the front of your garage to be placed at your front property line, but no closer than 10' to the edge of pavement of the County road. **This exception is permitted:** (1) if the slope of the front half of the lot is greater than one vertical foot rise or fall in a horizontal distance of seven feet (7:1 or 14.2%); or 2) if the elevation of your lot at the front property line is five feet or more above or below the elevation of the pavement of the County road. For further details, ask the Department of Public Works for a copy of Drawing R9-17.

**APPROVAL OF WORK**

All driveway work within the right-of-way of any County road is subject to inspection and approval by an inspector of the Public Works Department. Unsatisfactory work is subject to correction by the County if not corrected by the Permittee within fourteen (14) days of notification. Corrective work will be done by private contractor and the contractor's costs will be charged to the permittee.

**NOTIFICATION FOR INSPECTION:** The Department of Public Works will inspect your driveway three times as follows: (Exception: When a culvert with headwalls is required, additional inspections may be necessary - see *Fees*, page 4.)

- 1) An inspection prior to the issuance of the Encroachment Permit to determine existing conditions and restrictions;
- 2) A pre-pave (asphalt concrete) or pre-pour (concrete) inspection; and
- 3) A final inspection to assure compliance with all regulations.

**First Inspection:** The \$100 Encroachment Permit fee cannot be paid nor the Encroachment Permit issued before the first inspection has been made to determine existing conditions and restrictions.

**Second Inspection:** The owner or builder must give the Department of Public Works **48 hours notice** before they want the pre-pave or pre-pour inspection to be made. Paving or concrete placement **shall not take place** until Public Works has inspected the fill, basework, drainage culvert (if required) and the formwork for the concrete driveway slab (if concrete is used) to determine: 1) that the driveway does not exceed the maximum slope permitted by the County Standards; and 2) to determine the driveway dimensions, configuration, baserock, etc. are as required by the County Standards. After this inspection, the Public Works Inspector will approve the pre-pave or pre-pour inspection. If the owner/builder places the asphalt or concrete pavement without an inspection, and the driveway does not meet County Standards, the Department of Public Works will not sign off (final) the driveway encroachment on the Building Department Inspection Record Card (in the Building Department's Office), and the occupancy of the house will, therefore, not be permitted.

Encroachment Instructions  
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**Third Inspection (Final):** The third and final inspection also requires the owner/builder give Public Works **48 hour notice** before they wish the inspection to be made. If this inspection determines that the first 20 feet of the driveway complies with the County Standards, Public Works will sign off on the Building Department Inspection Record Card. This Inspection Record Card is used to determine when the Occupancy Permit can be issued by the Building Department.

**NOTE:** If the owner or builder leaves a gap between the edge of road pavement and a concrete driveway slab they constructed, that gap must be filled with compacted Type B maximum 1/2" aggregate asphaltic concrete (hot mix) before Public Works will make the Final Inspection.

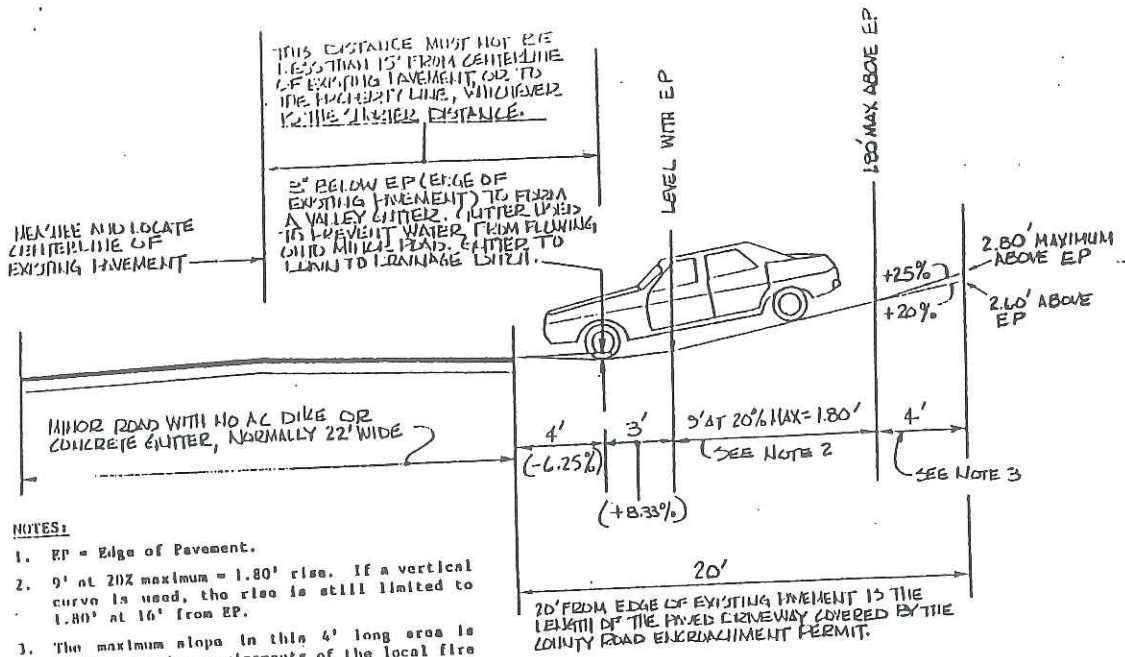
**FEES:** If reinspections or other additional inspections are necessary, each reinspection will be charged at the rate of one-third of the Encroachment Permit fee (i.e. if permit fee is \$100, reinspection fee would be \$33.33).

**SAFETY:** Adequate provisions shall be made by the permittee for the protection of the traveling public. Barricades shall be used and flashing yellow or red lights shall be in place between sunset and sunrise. Flagmen shall be employed if required by the particular work.

No materials shall be stored within three feet from the edge of the pavement or traveled way, unless specifically mentioned in the permit.

Upon determination of the inspector that a safety hazard exists to the public, the Permittee will be notified to correct said hazard within a twenty-four (24) hour period. If the hazard is not corrected within this time period, it will be done by the County and billed to the Permittee.



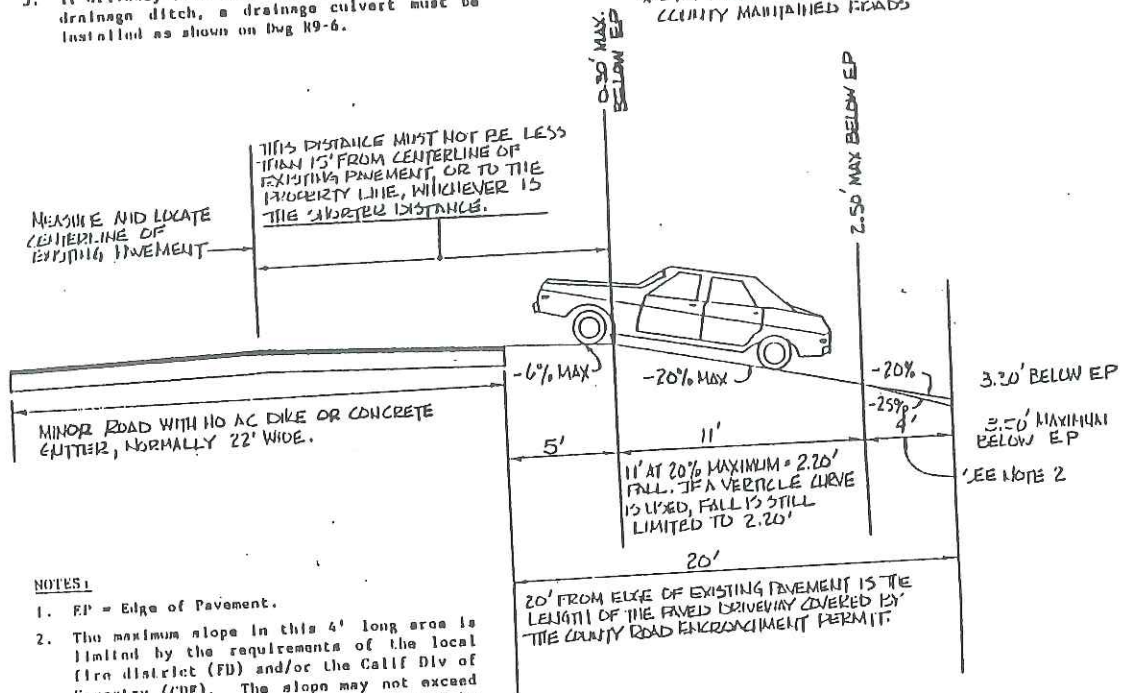


**NOTES:**

1. EP = Edge of Pavement.
2. 9' at 20% maximum = 1.80' rise. If a vertical curve is used, the rise is still limited to 1.80' at 16' from EP.
3. The maximum slope in this 4' long area is limited by the requirements of the local fire district (FD) and/or the Calif Div of Forestry (CDF). The slope may not exceed 20% unless a steeper slope is approved by the FD or CDF. In no case may the slope exceed 25% (1.0' rise in the 4' distance).
4. For driveway base and paving, see Dwg R9-6.
5. If driveway fill will block existing roadside drainage ditch, a drainage culvert must be installed as shown on Dwg R9-6.

COUNTY OF LAKE - DEPT. OF PUBLIC WORKS	9/01/92
* MINOR ROAD - ASCENDING DRIVEWAY NO AC DIKE OR CONCRETE GUTTER	DWG R9-1A

\* STANDARD FOR EXISTING COUNTY MAINTAINED ROADS

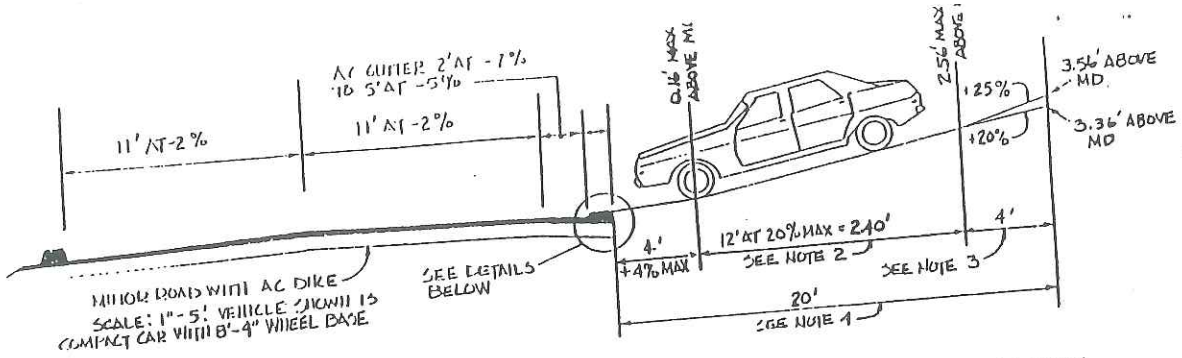


**NOTES:**

1. EP = Edge of Pavement.
2. The maximum slope in this 4' long area is limited by the requirements of the local fire district (FD) and/or the Calif Div of Forestry (CDF). The slope may not exceed 20% unless a steeper slope is approved by the FD or CDF. In no case may the slope exceed 25% (1.0' rise in the 4' distance).
3. For driveway base and paving, see DWG R9-6.
4. Rainfall runoff from the Minor Road will flow down the driveway shown above. It is the responsibility of the property owner and/or the builder to divert that water before it reaches the garage or residence.

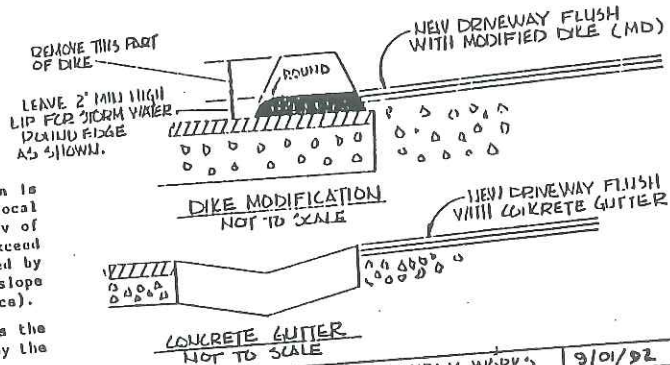
COUNTY OF LAKE - DEPT. OF PUBLIC WORKS	9/01/92
* MINOR ROAD - DESCENDING DRIVEWAY NO AC DIKE OR CONCRETE GUTTER	DWG R9-1B

\* STANDARD FOR EXISTING COUNTY MAINTAINED ROADS.

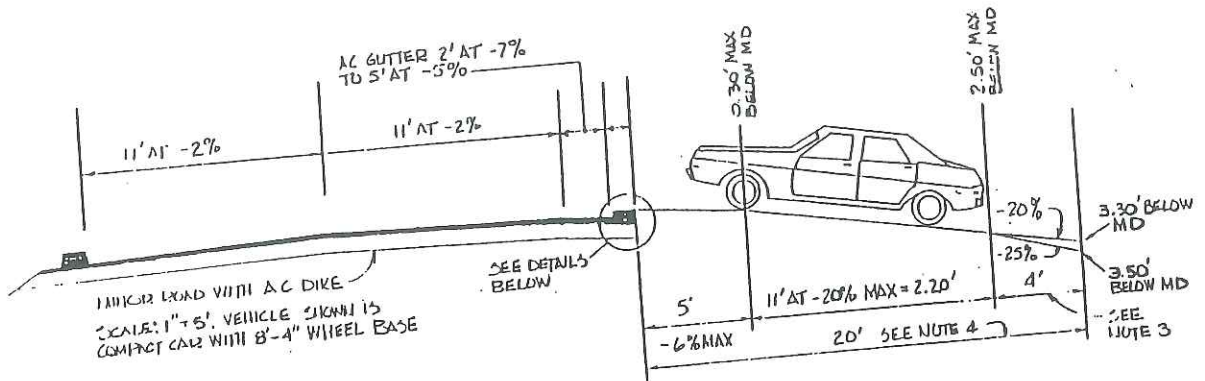


**NOTES:**

1. MD = Top of modified dike.
2. If a vertical curve is used, rise is still limited to 2.56' at 16' from dike.
3. The maximum slope in this 4' long area is limited by the requirements of the local fire district (FD) and/or the Calif Div of Forestry (CDF). The slope may not exceed 20% unless a steeper slope is approved by the FD or CDF. In no case may the slope exceed 25% (1.0' rise in the 4' distance).
4. 20' from edge of existing pavement is the length of the paved driveway covered by the County Road Encroachment Permit.
5. For driveway base and paving, see DWG R9-6.
6. If driveway fill will block existing roadside drainage ditch, a drainage culvert must be installed as shown on DWG R9-6.

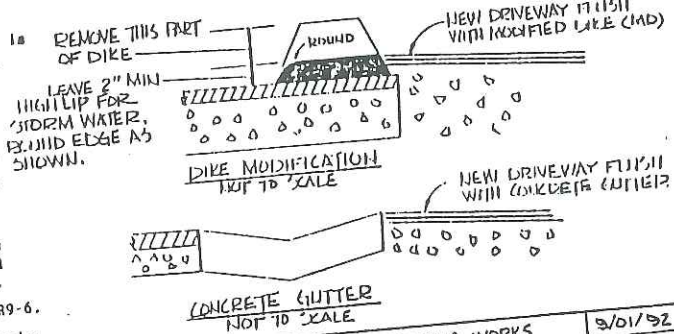


COUNTY OF LAKE - DEPT OF PUBLIC WORKS		9/01/92
* MINOR ROAD - ASCENDING DRIVEWAY WITH AC DIKE OR CONCRETE GUTTER		DWG R9-2A
* STANDARD FOR EXISTING COUNTY MAINTAINED ROADS		

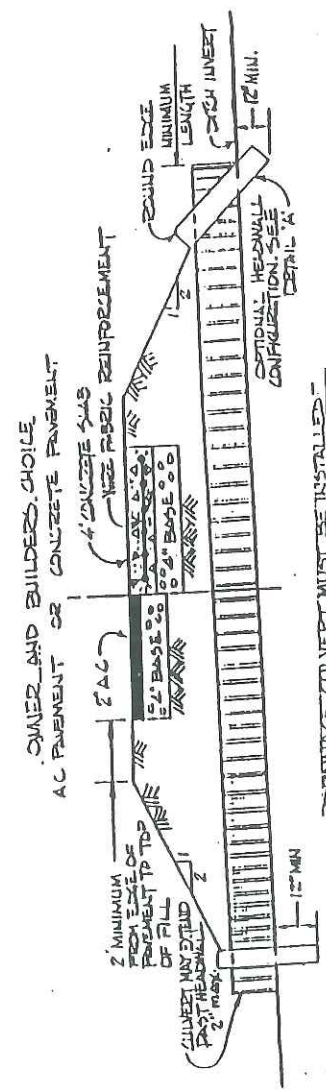


**NOTES:**

1. MD = Top of modified dike.
2. If a vertical curve is used, the fall is still limited to 2.50' at 16' from dike.
3. The maximum slope in this 4' long area is limited by the requirements of the local fire district (FD) and/or the Calif Div of Forestry (CDF). The slope may not exceed 20% unless a steeper slope is approved by the FD or CDF. In no case may the slope exceed 25% (1.0' rise in the 4' distance).
4. 20' from edge of existing pavement is the length of the paved driveway covered by the County Road Encroachment Permit.
5. For driveway base and paving, see DWG R9-6.
6. Be advised that during periods of peak rain-fall runoff, water will flow over the 2" high lip of the AC dike or over the driveway. It is the responsibility of the property owner and builder to divert that water before it reaches the garage or residence.

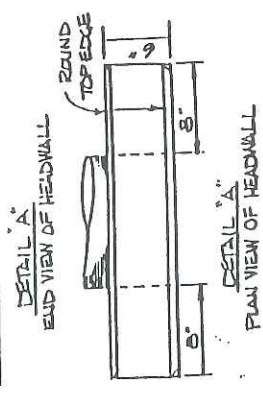
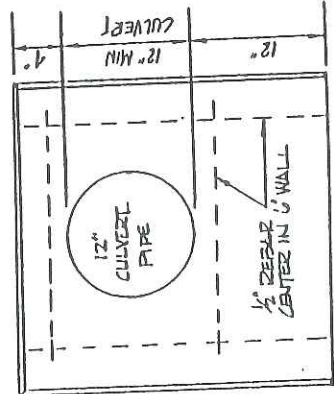


COUNTY OF LAKE - DEPT OF PUBLIC WORKS		9/01/92
* MINOR ROAD - DESCENDING DRIVEWAY WITH AC DIKE OR CONCRETE GUTTER		DWG R9-2B
* STANDARD FOR EXISTING COUNTY MAINTAINED ROADS		

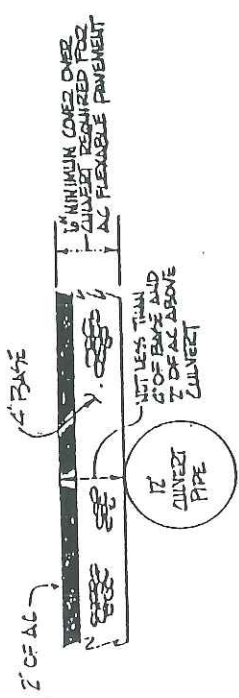


QUIER AND BUILDER CHOICE  
AC PAVEMENT OR CONCRETE PAVEMENT

- NOTES:
- Option: Use either 2" of AC and 4" base; or 4" concrete and 4" base.
  - Base: Class II or III roadbase; redrock sand acceptable under concrete; 3/4" maximum aggregate; 95% relative compaction suggested, 90% compaction required.
  - CONCRETE: 3/4" maximum aggregate; 5 sacks cement per cubic yard; 4 ounces air entraining agent per cubic yard. Protect concrete for 72 hours by covering when nighttime temperature will be below 32 degrees F.
  - WIRE FABRIC: Reinforce the first 20' of the 4" thick driveway slab with 6"x6"X10 gage welded wire fabric centered in slab.
  - AC: 2" thick asphaltic concrete surfacing; Type B with 1/2" maximum aggregate.
  - REBAR: 1/2" diameter grade 40 or grade 60. Install as shown. For convenience, each 1/2" diameter (#4) rebar may be replaced with two 3/8" diameter (#3) rebar.
  - CULVERT: 12" minimum diameter by 16 gage corrugated metal culvert pipe. A larger culvert diameter may be required, depending on the upstream drainage area.
  - HEADWALLS: Install ends of culvert pipe and headwalls at the center of the existing drainage swale or ditch; culvert invert to match invert of ditch or swale.
  - EARTH SURGRADE: No fill slopes steeper than 2 feet horizontal to one foot vertical; all fill compacted to minimum of 90% relative compaction; 95% compaction in the top 12" below the roadbase is recommended.



DETAIL A  
END VIEW OF HEADWALL



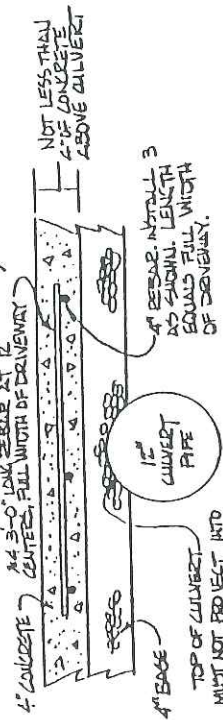
CULVERT UNDER AC PAVEMENT

WIRE FABRIC REINFORCEMENT REQUIRED REGARDLESS OF COVER SEE NOTE 4



CULVERT UNDER CONCRETE PAVEMENT

NOTE: IF DEPTH OF EXISTING DITCH WILL NOT PERMIT INSTALLATION OF 4" OF BASE ROCK ABOVE CULVERT, ADD #4 REBAR AS SHOWN BELOW



TOP OF CULVERT MUST NOT PROJECT INTO 4\"/>

DRAWING NOT TO SCALE

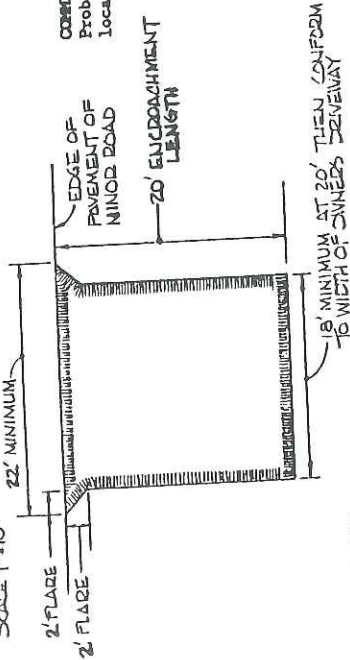
COUNTY OF LAKE - DEPT OF PUBLIC WORKS	3/10/92
RESIDENTIAL DRAINAGE PAVEMENT DRAINAGE CULVERT & HEADWALL	DWG R9-6

\*\* STANDARD FOR EXISTING COUNTRYMAINTAINED ROAD

\*\* ADS N-12 Pipe is acceptable in certain circumstances.

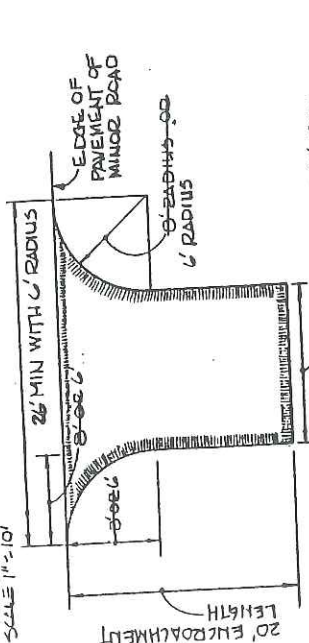
**DRIVEWAY DIMENSIONS FOR EXISTING MINOR ROADS**  
 One of the following three options may be used for a residential driveway encroachment intersecting a minor County road at a 90 degree angle.

**OPTION 1:**  
 SCALE 1" = 10'

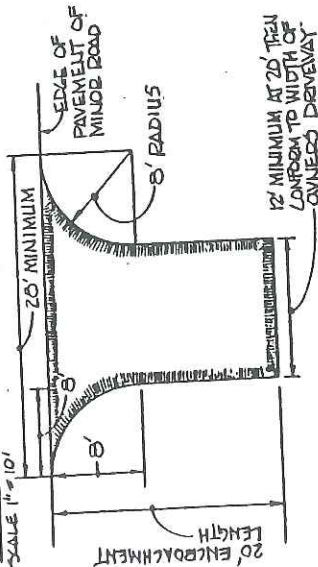


**COMMENTS FOR OPTION 1:**  
 Probably the best option for a two car garage located at the property setback line.

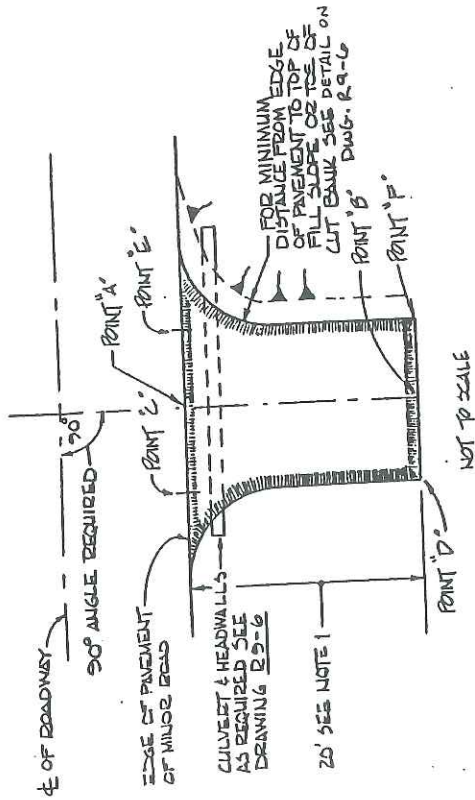
**OPTION 2:**  
 SCALE 1" = 10'



**OPTION 3:**  
 SCALE 1" = 10'

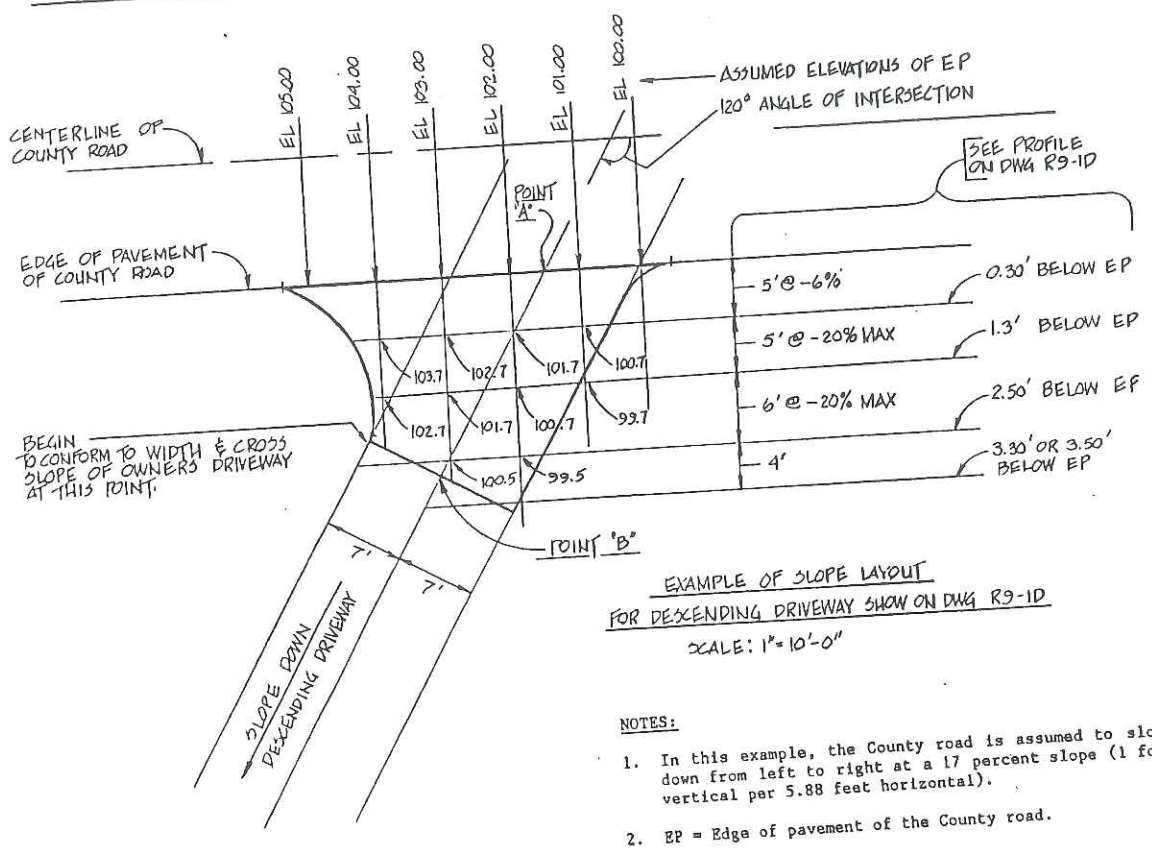
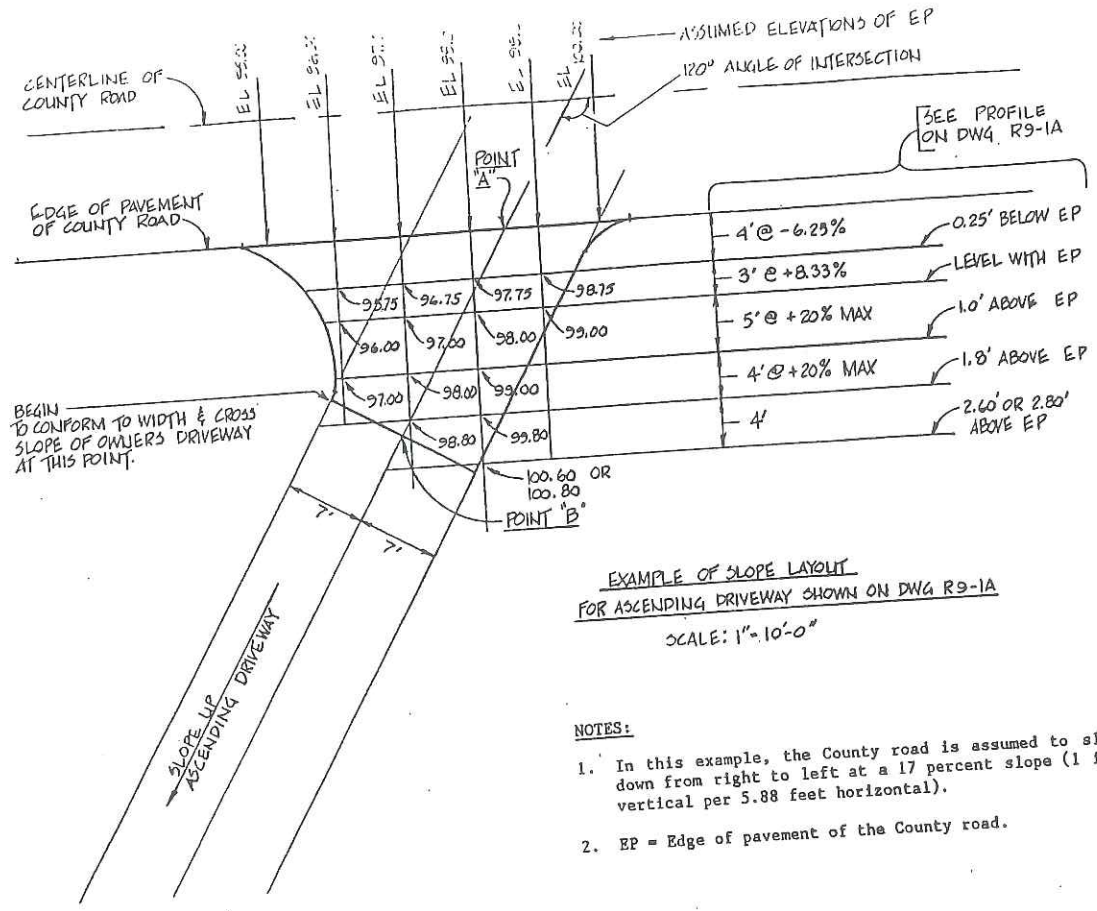


**COMMENTS FOR OPTION 3:**  
 1. 12 feet is the minimum driveway width permitted by any option.

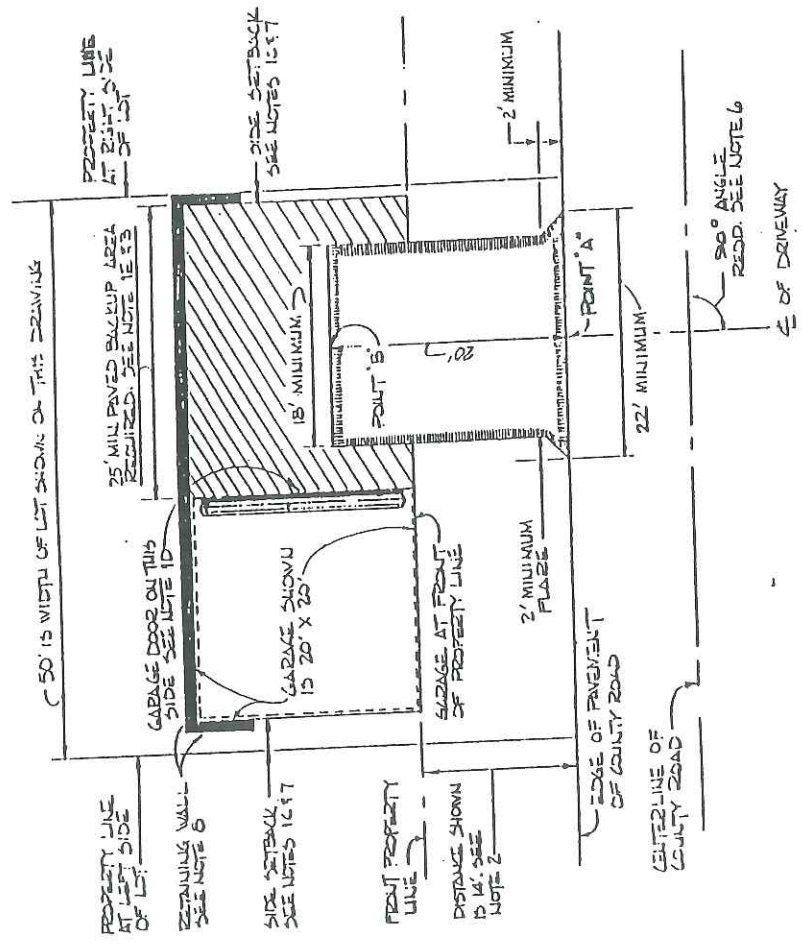


COUNTY OF LAKE - DEPT. OF PUBLIC WORKS	9/01/92
* DRIVEWAY INTERSECTING MINOR ROAD AT 90° ANGLE	DWG R-9-7
* STANDARD FOR EXISTING COUNTY MAINTAINED ROAD.	





NOTE: THIS EXCEPTION DOES NOT APPLY TO THE RESIDENCE. SEE NOTE 1B.



\* STANDARD FOR EXISTING COUNTY MAINTENANCE ROAD  
 COUNTY OF LAKE - DEPT. OF PUBLIC WORKS 9/01/82  
 \* MINOR ROAD ZONING EXCEPTION - GARAGE AT FRONT PROPERTY LINE.  
 DWG R9-17

SCALE: 1" = 10'-0"

NOTES:

1. Article 42 of the Lake County Zoning Ordinance allows a zoning exception for steep lots. The exception permits private garages, open parking platforms or outside staircases to be located at the front property line of the lot, provided the wall of the structure does not obstruct the sight distance thereby creating or increasing any traffic safety hazard. Article 42, as it applies to driveways and garages, can be summarized as follows:
  - A. The exception is permitted if the slope of the front half of the lot is greater than one foot rise or fall in a distance of seven feet (7:1 or 14.2%); or permitted if the elevation of the lot at the front property line is five feet or more above or below the established street elevation.
  - B. The exception allows a detached or attached private garage, open parking platform, or outside staircase to be built to the front property line. The staircase cannot be wider than 4 feet.
 

Note: This exception does not apply to the house which cannot be located closer to the front property line than the front setback line of the property.
  - C. The garage, parking platform or staircase cannot encroach on the setback required for the side yards.
  - D. The entrance to the garage or carport must be oriented towards one of the two side lot lines.
  - E. The entrance to the garage or carport must have a minimum backup area of twenty five feet (25').
  - F. The front wall of the garage (or parking platform or staircase) cannot obstruct the sight distance of a driver exiting the driveway. The sight distance required and the method by which the "unobstructed Sightline" is determined are shown on Dwg. R9-8. On that drawing, the "eye" of the driver is located 10 feet from the edge of pavement, and 3.5 feet high above the center of the driveway.
    - (1) If the front property line of the lot is less than 10 feet from the edge of pavement of the County road, the front wall of the garage, parking platform or staircase cannot be placed at the front property line. The garage will have to be constructed more distant from the road, and constructed at a distance from the edge of pavement that will permit the required minimum distances "TL" and "DP" on Dwg. R9-8 to be obtained.
    - (2) If the front property line is 10 feet or more from the edge of pavement of the County road, the Owner/Builder will demonstrate to the Department of Public Works that the front wall of the garage

will not obstruct the line of sight of a driver exiting the driveway to the point where the required minimum distances "DL" and "DR" cannot be obtained. Additionally, the Owner/Builder will demonstrate that the front wall will not obstruct the line of site of a driver exiting a driveway on one of the adjacent lots. That situation can occur when the lots and driveways are located on the inside of a horizontal curve in the County road.

2. The distance between the front property line of the lot and the edge of pavement varies throughout the County. If a 22 feet wide paved road is centered in a 50 feet wide road right-of-way, the distance between edge of pavement and property line is 14 feet ( $50' - 22' = 28'$ ;  $28' \div 2$  sides = 14'). However, there are lots within the County where the front property line is at, or within 2 or 3 feet of, the edge of pavement; while the front property line of other lots may be 20 feet from edge of pavement. Owner/Builder should measure the actual distance at their lot to determine the practicality of using this zoning exception.

3. The first 20 feet of driveway, measured along the driveway centerline between Points A and B, is the driveway encroachment area and it must be constructed as shown on this plan view and with driveway base rock and paving as required on Dwg. R9-6. The 25 feet paved backup area, described above in Item 1-2 and shown cross-hatched on the drawing, may be paved as Owner/Builder elect. The driveway widths shown on the drawing for the 20 feet long encroachment area are minimum widths and the Owner/Builder may elect to increase the driveway widths to facilitate entering and exiting the garage. The width of the 25 feet long paved backup area should not be less than the out-to-out width of the garage door(s).

4. The maximum driveway slope permitted in the first 20 feet of driveway encroachment is shown on Dwg. R9-1A and R9-1B. If the County road has an AC dike or concrete gutter, use Dwg. R9-2A or R9-2B. This maximum slope is measured along the driveway centerline between Points A and B. Install pavement, culvert and headwalls in the 20 feet long encroachment as required by Dwg. R9-6.

5. A two feet minimum distance between edge of driveway pavement and top of fill slope, or between edge of driveway pavement and toe of cut bank, is required.

6. The driveway shall be perpendicular to and intersect the County road at a 90 degree angle.

7. Owner/Builder to consult the County Planning Department for the side setback requirements. On the plan view shown on Dwg. R9-17, the side setbacks are: 1) the required minimum distance between the end of the garage and the left property line; and 2) the required minimum distance between the paved parking area and the right property line.

Note: Retaining walls are permitted on the property line.

Dwg. R9-17 shows a retaining wall under the back and side walls of the garage and along the back and side of the backup area. The design of retaining walls 4 feet and higher must be reviewed by the County Building Department.

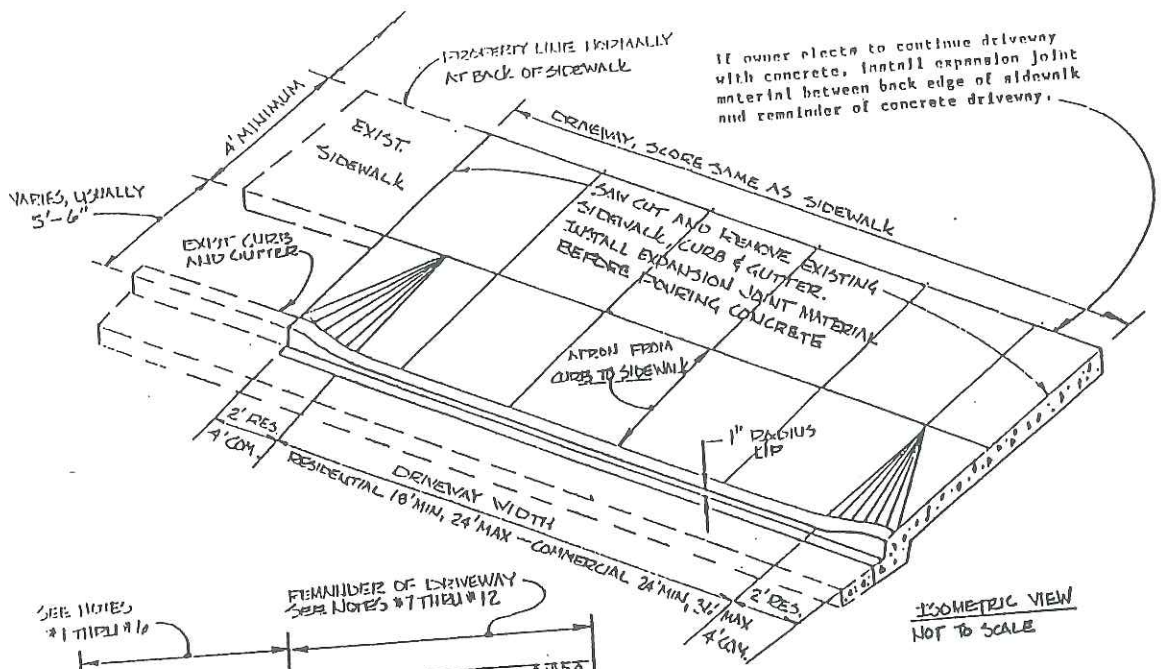
If the backup area and garage are located in cut, a 2:1 cut slope may be used in lieu of the retaining wall provided the toe of the cut bank is no closer to the wall of the garage than 5 feet. A lot wider than 50 feet will probably be needed to use cut slopes along the side property lines as the top of the cut bank must not be closer than 5 feet to a side property line.

If the backup area and garage are located on fill, a 2:1 fill slope may be used in lieu of the retaining wall provided the toe of the fill slope is no closer than 5 feet to a side property line.

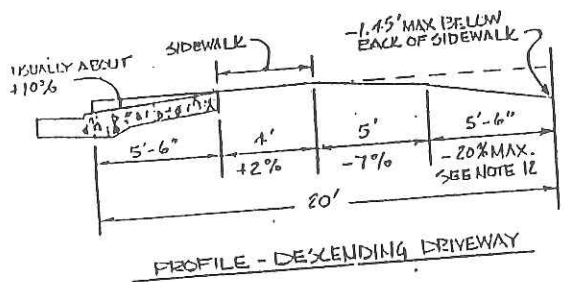
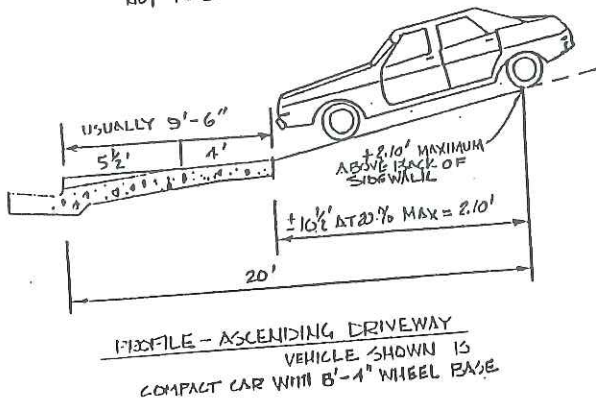
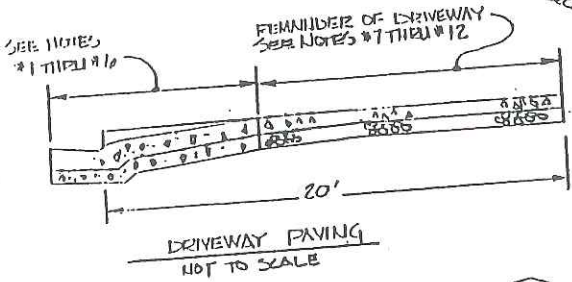
(continued)







If owner elects to continue driveway with concrete, install expansion joint material between back edge of sidewalk and remainder of concrete driveway.



**NOTES FOR CURB, GUTTER AND SIDEWALK AREA**

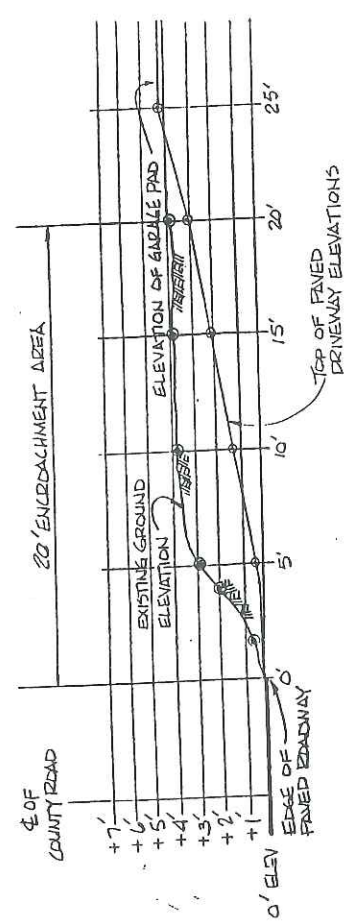
1. Saw cut face and top of curb, gutter and sidewalk to a minimum depth of 2".
2. Base is Class II roadbase, 3/4" maximum aggregate.
3. Driveway shall be 6" minimum thickness concrete for residential driveway and 8" minimum concrete for commercial driveway.
4. CONCRETE: 3/4" maximum aggregate; 5 sacks cement per cubic yard (cy); 4 ounces air entraining agent per cy. Protect concrete for 72 hours by covering when nighttime temperature will be below 32 degrees.
5. Reinforce curb, gutter and sidewalk with #3 bars 12" on center each way (OCEW) for residential driveway and #4 12" OCEW for commercial driveway.
6. Provide broom finish on ramp and sidewalk. Broom in direction parallel to curb.

**NOTES FOR "REMAINDER OF DRIVEWAY"**

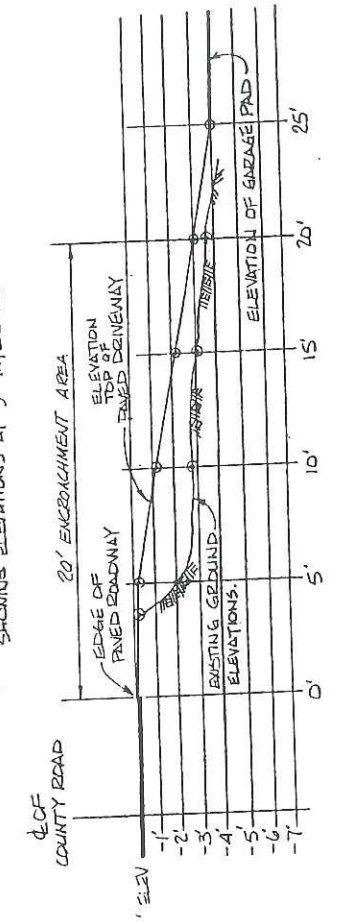
7. Option: Use either 2" of AC and 4" base; or 4" concrete and 4" base.
8. Base: Class II or III roadbase; 3/4" maximum aggregate. Red rock sand acceptable under concrete.
9. Concrete mix: Same as Note 4.
10. Reinforce 4" thick driveway slab with 6" x 6" x 10 gauge welded wire fabric centered in slab.
11. 2" thick asphalt concrete surfacing; Type B with 1/2" maximum aggregate.
12. If vertical curve is used, the fall is still limited to 1.45' at 20' distance from face of curb.

COUNTY OF LAKE - DEPT OF PUBLIC WORKS	9/01/92
* MINOR STREET NEW DRIVEWAY IN EXISTING, NONCONTIGUOUS CURB & SIDEWALK	DWG R9-4NC
* STANDARD FOR EXISTING COUNTY MAINTAINED STREETS	

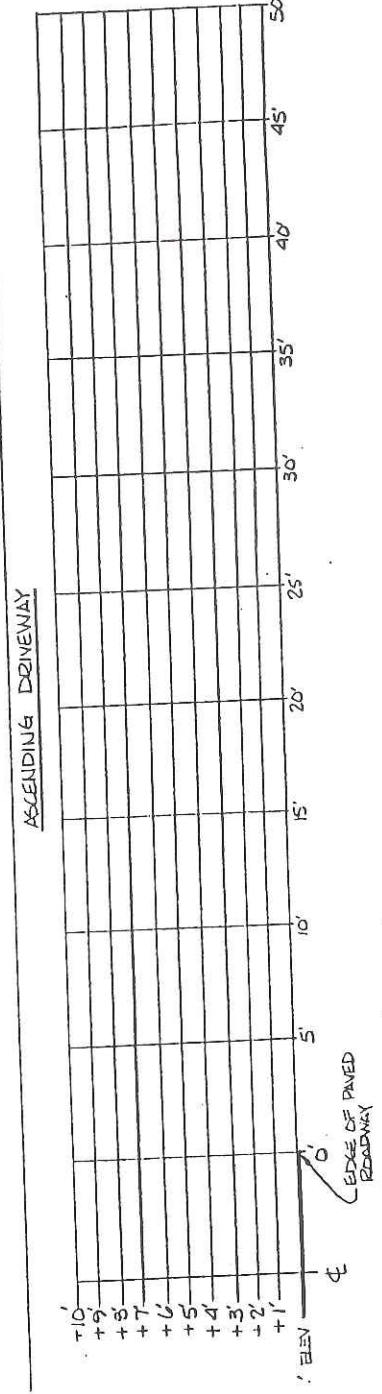
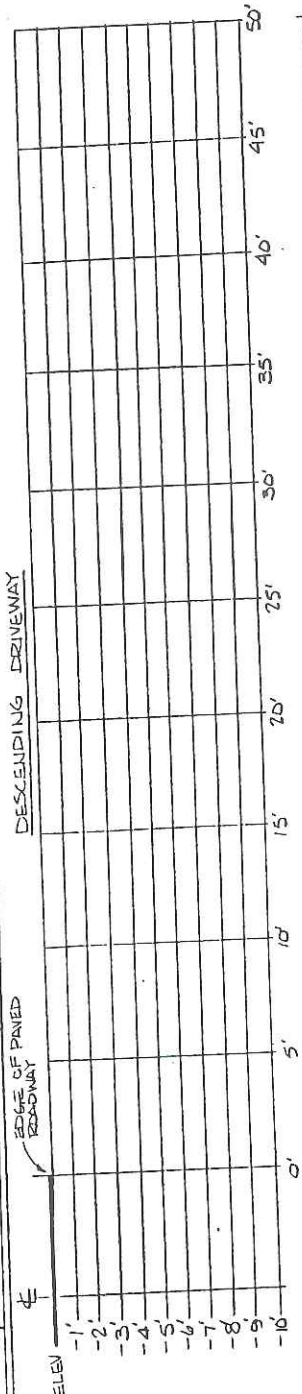
EXAMPLE OF ASCENDING DRIVEWAY  
SHOWING ELEVATIONS AT 5' INTERVALS



EXAMPLE OF DESCENDING DRIVEWAY  
SHOWING ELEVATIONS AT 5' INTERVALS



PLOT YOUR DRIVEWAY BELOW. SHOW EXISTING GROUND, DRIVEWAY SURFACE AND GARAGE PAD.



County Road No. \_\_\_\_\_ Enc. No. \_\_\_\_\_  
 A.P. No(s). \_\_\_\_\_  
 Name of Property Owner \_\_\_\_\_  
 Property Address: \_\_\_\_\_  
 Owner's Telephone No. \_\_\_\_\_  
 Profile Drawn By: \_\_\_\_\_  
 Title (Owner, Builder, Agent) \_\_\_\_\_  
 Telephone No. \_\_\_\_\_  
 Date: \_\_\_\_\_  
 CDF \_\_\_\_\_  
 Authorized Signature \_\_\_\_\_ Date \_\_\_\_\_  
 Fire Dept. \_\_\_\_\_ Date \_\_\_\_\_  
 Authorized Signature \_\_\_\_\_  
 DRIVEWAY SLOPE WILL NOT EXCEED 16%  
 Signature (Owner, Builder, Agent) \_\_\_\_\_ Date \_\_\_\_\_



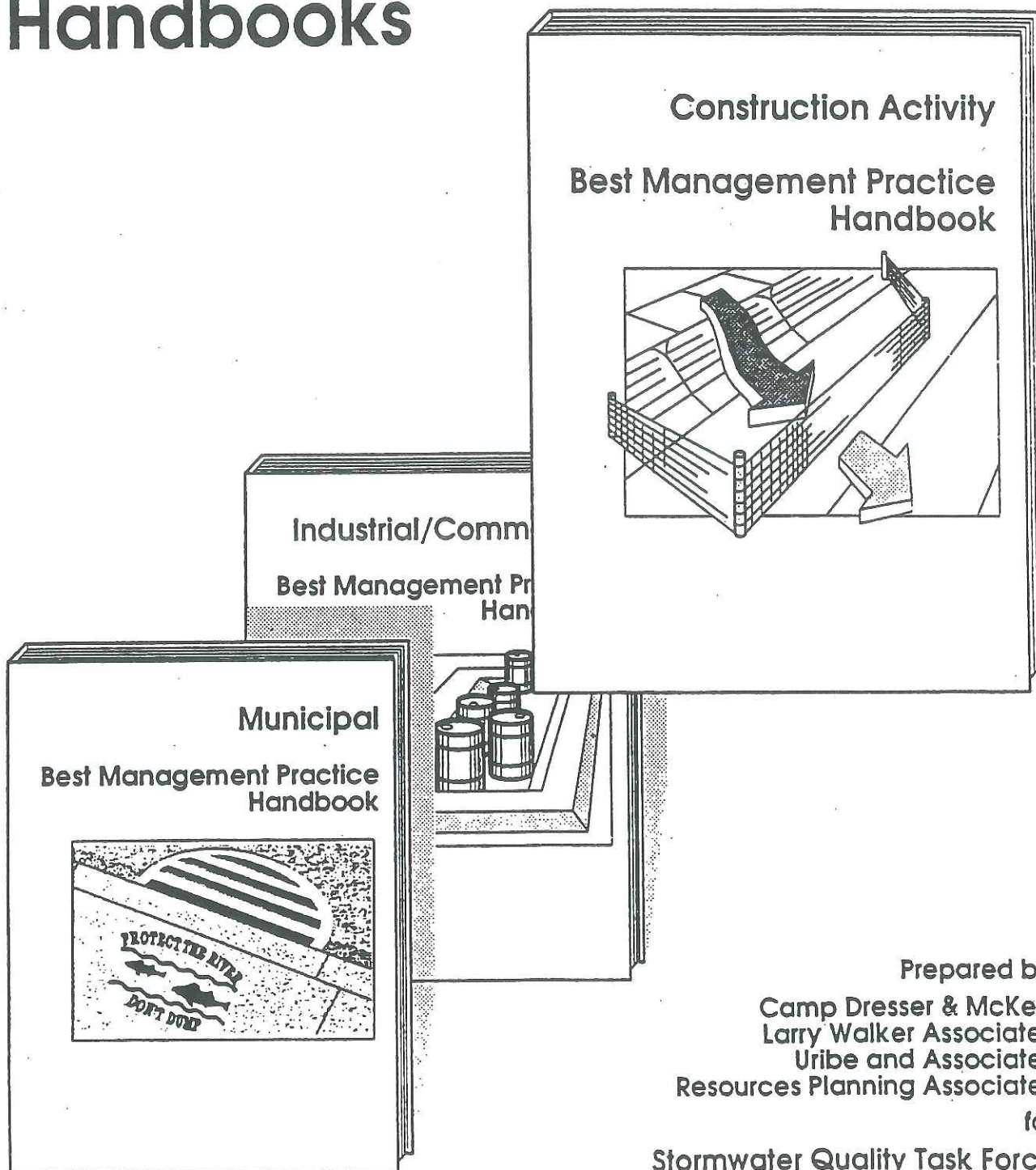
## **APPENDIX C - BEST MANAGEMENT PRACTICES**

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March, 1993

# California Storm Water Best Management Practice Handbooks



Prepared by  
Camp Dresser & McKee  
Larry Walker Associates  
Uribe and Associates  
Resources Planning Associates  
for  
Stormwater Quality Task Force

## 4. BMPs FOR CONTRACTOR ACTIVITIES

### INTRODUCTION

This chapter describes specific Best Management Practices (BMPs)

for common construction activities that may pollute storm water. Chapter 2 led you through the steps of identifying activities at your site that can pollute storm water, while Chapter 3 provided guidance on BMP selection. This chapter will provide a list of BMPs that can be used to fit your site's needs.

BMP fact sheets are provided for each of the contractor's activities, noted in the box, are consistent with Worksheet 4 in Chapter 2.

Each fact sheet contains a cover sheet with:

- A description of the BMP
- Approach
- Requirements
  - Costs, including capital costs, and operation and maintenance (O&M) costs
  - Maintenance (including administrative and staffing)
- Limitations
- References

The side bar presents information on which BMP objective applies, targeted constituents, and an indication of the level of effort and costs to implement. For some BMPs, further information is provided in additional sheets.

### Contractor Activities

#### Construction Practices

- CA1 Dewatering Operations
- CA2 Paving Operations
- CA3 Structure Construction and Painting

#### Material Management

- CA10 Material Delivery and Storage
- CA11 Material Use
- CA12 Spill Prevention and Control

#### Waste Management

- CA20 Solid Waste Management
- CA21 Hazardous Waste Management
- CA22 Contaminated Soil Management
- CA23 Concrete Waste Management
- CA24 Sanitary/Septic Waste Management

#### Vehicle and Equipment Management

- CA30 Vehicle and Equipment Cleaning
- CA31 Vehicle and Equipment Fueling
- CA32 Vehicle and Equipment Maintenance

#### Contractor Training

- CA40 Employee/Subcontractor Training

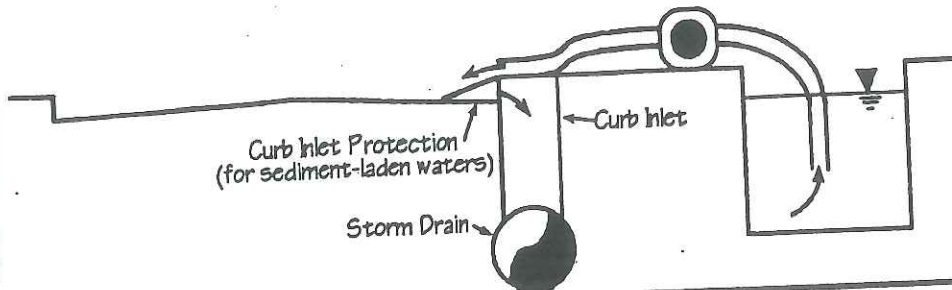
These BMP fact sheets are suitable for inclusion in many storm water pollution prevention plans for typical contractor activities. The BMPs listed are not an exhaustive list, nor will every BMP be appropriate for every situation. Therefore, suggested BMPs which are inappropriate may be deleted and additional BMPs for specific site conditions should be added. In addition, your selection and implementation of BMPs should be reviewed on a regular basis to match the changing conditions at construction sites.



TABLE 4.1 CONTRACTOR ACTIVITIES AND BMP OBJECTIVES

BMP CATEGORY	BMP OBJECTIVES							
	PRACTICE GOOD HOUSE-KEEPING	CONTAIN WASTE	MINIMIZE DISTURBED AREA	STABILIZE DISTURBED AREA	PROTECT SLOPES AND CHANNELS	CONTROL SITE PERIMETER	CONTROL INTERNAL EROSION	
	<b>Construction Practices</b>							
CA01	✓				✓	✓	✓	
CA02	✓							
CA03	✓			✓				
	<b>Material Management</b>							
CA10	✓							
CA11	✓							
CA12	✓							
	<b>Waste Management</b>							
CA20		✓						
CA21		✓						
CA22		✓	✓	✓				
CA23		✓						
CA24		✓						
	<b>Vehicle and Equipment Management</b>							
CA30	✓					✓	✓	
CA31	✓							
CA32	✓							
	<b>Contractor Training</b>							
CA40	✓	✓						

## ACTIVITY: DEWATERING OPERATIONS



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from dewatering operations by using sediment controls and by testing the groundwater for pollution.

### APPROACH

There are two general classes of pollutants that may result from dewatering operations; sediment, and toxics and petroleum products. A high sediment content in dewatering discharges is common because of the nature of the operation. On the other hand, toxics and petroleum products are not commonly found in dewatering discharges unless, the site or surrounding area has been used for light or heavy industrial activities, or the area has a history of groundwater contamination. The following steps will help reduce storm water pollution from dewatering discharges:

#### Sediment

- Use sediment controls to remove sediment from water generated by dewatering (See Sediment Trap (ESC 55) and Sediment Basin (ESC 56) in Chapter 5).
- Use filtration to remove sediment from a sediment trap or basin. Filtration can be achieved with:
  - Sump pit and a perforated or slit standpipe with holes and wrapped in filter fabric. The standpipe is surrounded by stones which filters the water as it collects in the pit before being pumped out. Wrapping the standpipe in filter fabric may require an increased suction inlet area to avoid clogging and unacceptable pump operation.
  - Floating suction hose to allow cleaner surface water to be pumped out.

#### Toxics and Petroleum Products

- In areas suspected of having groundwater pollution, sample the groundwater near the excavation site and have the water tested for known or suspected pollutants at a certified laboratory. Check with the Regional Water Quality Control Board and the local wastewater treatment plant for their requirements for dewatering, additional water quality tests, and disposal options.
- With a permit from the Regional Water Quality Control Board, you may be able to recycle/reuse pumped groundwater for landscape irrigation, or discharge to the storm sewer. With a permit from the local agency, you may be able to treat pumped groundwater and discharge it to the municipal wastewater treatment plant via the sanitary sewer.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### Objectives

Housekeeping Practices

Contain Waste

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

High  Low

CA1



## CONTRACTOR ACTIVITY: DEWATERING OPERATIONS (Continue)

### REQUIREMENTS

- Costs (Capital, O&M)
  - Sediment controls are low cost measures.
  - Treatment and/or discharge of polluted groundwater can be quite expensive.
- Maintenance
  - Maintain sediment controls and filters in good working order. (See Chapter 5 for details)
  - Inspect excavated areas daily for signs of contaminated water as evidenced by discoloration, oily sheen, or odors.

### LIMITATIONS

- The presence of contaminated water may indicate contaminated soil as well. See CA22 (Contaminated Soil Management) in this chapter for more information.

### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

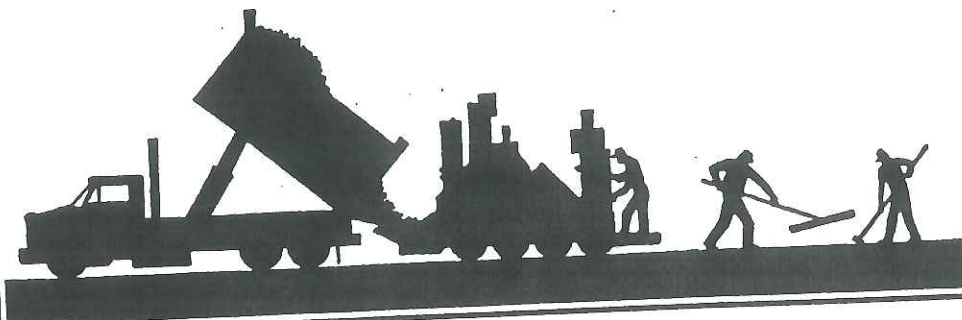
Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA1



## ACTIVITY: PAVING OPERATIONS

Graphic: North Central Texas COG, 1993



### DESCRIPTION

Prevent or reduce the discharge of pollutants from paving operations, using measures to prevent runoff and runoff pollution, properly disposing of wastes, and training employees and subcontractors.

### APPROACH

- Avoid paving during wet weather.
- Store materials away from drainage courses to prevent storm water runoff (see CA10 Material Delivery and Storage).
- Protect drainage courses, particularly in areas with a grade, by employing BMPs to divert runoff or trap/filter sediment (see Chapter 5).
- Leaks and spills from paving equipment can contain toxic levels of heavy metals and oil and grease. Place drip pans or absorbent materials under paving equipment when not in use. Clean up spills with absorbent materials rather than burying. See CA32 (Vehicle and Equipment Maintenance) and CA12 (Spill Prevention and Control) in this chapter.
- Cover catch basins and manholes when applying seal coat, tack coat, slurry seal, fog seal, etc.
- Shovel or vacuum saw-cut slurry and remove from site. Cover or barricade storm drains during saw cutting to contain slurry.
- If paving involves portland cement concrete, see CA23 (Concrete Waste Management) in this chapter.
- If paving involves asphaltic concrete, follow these steps:
  - Do not allow sand or gravel placed over new asphalt to wash into storm drains, streets, or creeks by sweeping. Properly dispose of this waste by referring to CA20 (Solid Waste Management) in this chapter.
  - Old asphalt must be disposed of properly. Collect and remove all broken asphalt from the site and recycle whenever possible.
  - If paving involves on-site mixing plant, follow the storm water permitting requirements for industrial activities.
- Train employees and subcontractors.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Inspect employees and subcontractors to ensure that measures are being followed.
  - Keep ample supplies of drip pans or absorbent materials on-site.

### LIMITATIONS

- There are no major limitations to this best management practice.

### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA2



Best Management Practices

## CONTRACTOR ACTIVITY: PAVING OPERATIONS (Continue)

### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

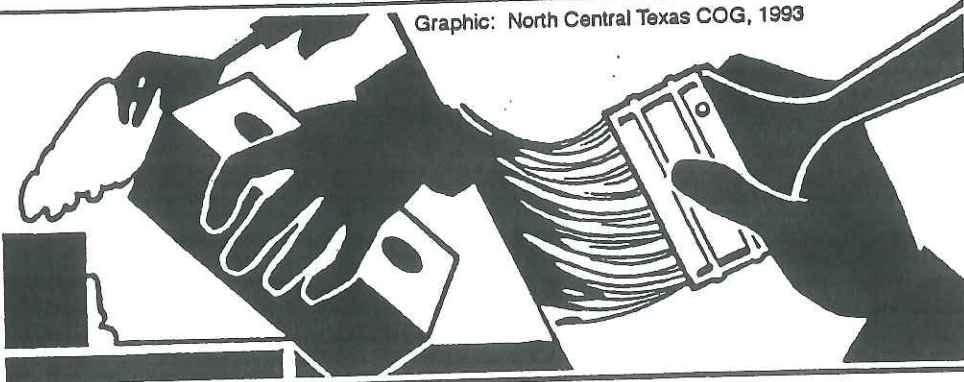
Hot-mix Asphalt Paving Handbook, U.S. Army Corps of Engineers, AC 150/5370-14, Appendix I, July 1991.

CA2



## ACTIVITY: STRUCTURE CONSTRUCTION AND PAINTING

Graphic: North Central Texas COG, 1993



### Objectives

**Housekeeping Practices**

Contain Waste

Minimize Disturbed Areas

**Stabilize Disturbed Areas**

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from structure construction and painting by enclosing or covering or berming building material storage areas, using good housekeeping practices, using safer alternative products, and training employees and subcontractors.

### APPROACH

- Keep the work site clean and orderly. Remove debris in a timely fashion. Sweep the area.
- Use soil erosion control techniques if bare ground is exposed (See Chapter 5).
- Buy recycled or less hazardous products to the maximum extent practicable.
- Conduct painting operations consistent with local air quality and OSHA regulations.
- Properly store paints and solvents. See CA10 (Material Delivery and Storage) in this chapter.
- Properly store and dispose waste materials generated from the activity. See the waste management BMPs (CA20 to CA24) in this chapter.
- Recycle residual paints, solvents, lumber, and other materials to the maximum extent practicable.
- Make sure that nearby storm drains are well marked to minimize the chance of inadvertent disposal of residual paints and other liquids.
- Clean the storm drain system in the immediate construction area after construction is completed.
- Educate employees who are doing the work.
- Inform subcontractors of company policy on these matters and include appropriate provisions in their contract to make certain proper housekeeping and disposal practices are implemented.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - These BMPs are generally of low to moderate cost.
- Maintenance
  - Maintenance should be minimal.

### LIMITATIONS

- Safer alternative products may not be available, suitable, or effective in every case.
- Hazardous waste that cannot be re-used or recycled must be disposed of by a licensed hazardous waste hauler.

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

High  Low

## CA3

Best Management Practices

## ACTIVITY: STRUCTURE CONSTRUCTION AND PAINTING (Continue)

- Be certain that actions to help storm water quality are consistent with Cal- and Fed-OSHA and air quality regulations.

Construction and painting activities can generate pollutants that can reach storm water if proper care is not taken. The sources of these contaminants may be solvents, paints, paint and varnish removers, finishing residues, spent thinners, soap cleaners, kerosene, asphalt and concrete materials, adhesive residues, and old asbestos insulation. For specific information on some of these wastes see the following BMPs in this chapter:

CA20 Solid Waste,  
CA21 Hazardous Waste, and  
CA23 Concrete Waste.

More specific information on structure construction practices is listed below.

### Erosion and Sediment Control

If the work involves exposing large areas of soil or if old buildings are being torn down and not replaced in the near future, employ the appropriate soil erosion and control techniques described in Chapter 5.

### Storm/Sanitary Sewer Connections

Carefully install all plumbing and drainage systems. Cross connections between the sanitary and storm drain systems, as well as any other connections into the drainage system from inside a building, are illegal. Color code or flag pipelines on the project site to prevent such connections, and train construction personnel.

### Painting

Local air pollution regulations may, in many areas of the state, specify painting procedures which if properly carried out are usually sufficient to protect storm water quality. These regulations may require that painting operations be properly enclosed or covered to avoid drift. Use temporary scaffolding to hang drop cloths or draperies to prevent drift. Application equipment that minimizes overspray also helps. When using sealants on wood, pavement, roofs, etc, quickly clean up spills. Remove excess liquid with absorbent material or rags.

If painting requires scraping or sand blasting of the existing surface, use a drop cloth to collect most of the chips. Dispose the residue properly. If the paint contains lead or tributyl tin, it is considered a hazardous waste. Refer to the waste management BMPs in this chapter for more information.

Mix paint indoors, in a containment area, or in a flat unpaved area not subject to significant erosion. Do so even during dry weather because cleanup of a spill will never be 100% effective. Dried paint will erode from sloped surfaces and be washed away by storms. If using water based paints, clean the application equipment in a sink that is connected to the sanitary sewer or in a containment area where the dried paint can be readily removed. Properly store leftover paints if they are to be kept for the next job, or dispose of properly.

### Roof work

When working on roofs, if small particles have accumulated in the gutter, either sweep out the gutter or wash the gutter and trap the particles at the outlet of the downspout. A sock or geofabric placed over the outlet may effectively trap the materials. If the downspout is lined tight, place a temporary plug at the first convenient point in the storm drain and pump out the water with a vacor truck, and clean the catch basin sump where you placed the plug.

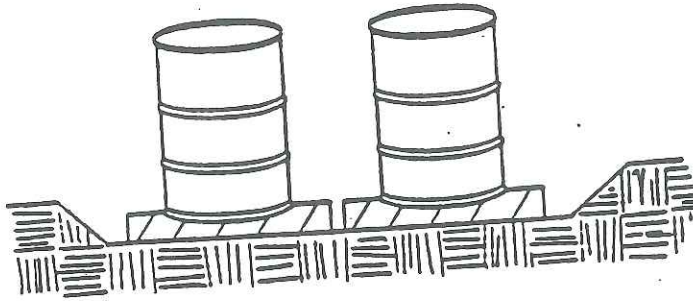
### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

CA3



## ACTIVITY: MATERIAL DELIVERY AND STORAGE



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from material delivery and storage by minimizing the storage of hazardous materials on-site, storing materials in a designated area, installing secondary containment, conducting regular inspections, and training employees and subcontractors.

This best management practice covers only material delivery and storage. For other information on materials, see CA11 (Material Use), or CA12 (Spill Prevention and Control). For information on wastes, see the waste management BMPs in this chapter.

### APPROACH

The following materials are commonly stored on construction sites:

- Soil,
- Pesticides and herbicides,
- Fertilizers,
- Detergents,
- Plaster or other products,
- Petroleum products such as fuel, oil, and grease, and
- Other hazardous chemicals such as acids, lime, glues, paints, solvents, and curing compounds.

Storage of these materials on-site can pose the following risks:

- Storm water pollution,
- Injury to workers or visitors,
- Groundwater pollution, and
- Soil contamination.

Therefore, the following steps should be taken to minimize your risk:

- Designate areas of the construction site for material delivery and storage.
  - Place near the construction entrances, away from waterways
  - Avoid transport near drainage paths or waterways
  - Surround with earth berms (see ESC30, Earth Dike.)
  - Place in an area which will be paved
- Storage of reactive, ignitable, or flammable liquids must comply with the fire codes of your area. Contact the local Fire Marshal to review site materials, quantities, and proposed storage area to determine specific requirements. See the Flammable and Combustible Liquid Code, NFPA30.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.
- Keep an accurate, up-to-date inventory of materials delivered and stored on-site.
- Keep your inventory down.

### Objectives

Housekeeping Practices

Contain Waste

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

Likely to Have Significant Impact

Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

High  Low

## CA10



March, 1993



## ACTIVITY: MATERIAL DELIVERY AND STORAGE (Continue)

- Minimize hazardous materials on-site storage.
- Handle hazardous materials as infrequently as possible.
- During the rainy season, consider storing materials in a covered area. Store materials in secondary containments such as an earthen dike, horse trough, or even a children's wading pool for non-reactive materials such as detergents, oil, grease, and paints. Small amounts of material may be secondarily contained in "bus boy" trays or concrete mixing trays.
- Do not store chemicals, drums, or bagged materials directly on the ground. Place these items on a pallet and, when possible, in secondary containment.
- If drums must be kept uncovered, store them at a slight angle to reduce ponding of rainwater on the lids and to reduce corrosion.
- Try to keep chemicals in their original containers, and keep them well labeled.
- Train employees and subcontractors.
- Employees trained in emergency spill cleanup procedures should be present when dangerous materials or liquid chemicals are unloaded.
- If significant residual materials remain on the ground after construction is complete, properly remove materials and any contaminated soil (See CA22). If the area is to be paved, pave as soon as materials are removed to stabilize the soil.

### REQUIREMENTS

- Cost (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Keep the designated storage area clean and well organized.
  - Conduct routine weekly inspections and check for external corrosion of material containers.
  - Keep an ample supply of spill cleanup materials near the storage area.

### LIMITATIONS

- Storage sheds often must meet building and fire code requirements.

### REFERENCES

Best Management Practices and Erosion Control Manual for Construction Sites; Flood Control District of Maricopa County, AZ, September 1992.

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

Coastal Nonpoint Pollution Control Program: Program Development and Approval Guidance, Working Group Working Paper; USEPA, April 1992.

Storm Water Management for Construction Activities; Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA10



## ACTIVITY: MATERIAL USE

Graphic: North Central Texas COG, 1993



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from material use by using alternative products, minimizing hazardous material use on-site, and training employees and subcontractors.

### APPROACH

The following materials are commonly used on construction sites:

- Pesticides and herbicides,
- Fertilizers,
- Detergents,
- Plaster and other products,
- Petroleum products such as fuel, oil, and grease, and
- Other hazardous chemicals such as acids, lime, glues, paints, solvents, and curing compounds.

Use of these materials on-site can pose the following risks:

- Storm water pollution,
- Injury to workers or visitors,
- Groundwater pollution, and
- Soil contamination.

Therefore, the following steps should be taken to minimize your risk:

- Use less hazardous, alternative materials as much as possible.
- Minimize use of hazardous materials on-site.
- Use materials only where and when needed to complete the construction activity.
- Follow manufacturer's instructions regarding uses, protective equipment, ventilation, flammability, and mixing of chemicals.
- Personnel who use pesticides should be trained in their use. The California Department of Pesticide Regulation and county agricultural commissioners license pesticide dealers, certify pesticide applicators, and conduct on-site inspections.
- Do not over-apply fertilizers, herbicides, and pesticides. Prepare only the amount needed. Follow the recommended usage instructions. Over-application is expensive and environmentally harmful. Unless on steep slopes, till fertilizers into the soil rather than hydroseeding. Apply surface dressings in several smaller applications, as opposed to one large application, to allow time for infiltration and to avoid excess material being carried off-site by runoff. Do not apply these chemicals just before it rains.
- Train employees and subcontractors in proper material use.

### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

High  Low

## CA11

Best Management Practices

## ACTIVITY: MATERIAL USE (Continue)

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Maintenance of this best management practice is minimal.

### LIMITATIONS

- Alternative materials may not be available, suitable, or effective in every case.

### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

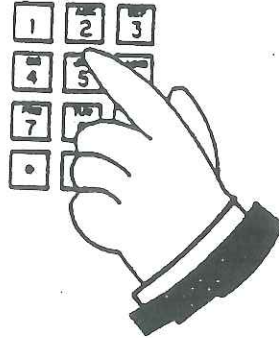
Coastal Nonpoint Pollution Control Program: Program Development and Approval Guidance, Working Group Working Paper; USEPA, April 1992.

Storm Water Management for Construction Activities; Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA11



## ACTIVITY: SPILL PREVENTION AND CONTROL



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from leaks and spills by reducing the chance for spills, stopping the source of spills, containing and cleaning up spills, properly disposing of spill materials, and training employees.

This best management practice covers only spill prevention and control. However, CA10 (Material Delivery and Storage) and CA11 (Material Use), also contain useful information, particularly on spill prevention. For information on wastes, see the waste management BMPs in this chapter.

### APPROACH

The following steps will help reduce the storm water impacts of leaks and spills:

#### Define "Significant Spill"

- Different materials pollute in different amounts. Make sure that each employee knows what a "significant spill" is for each material they use, and what is the appropriate response for "significant" and "insignificant" spills.

#### General Measures

- Hazardous materials and wastes should be stored in covered containers and protected from vandalism.
- Place a stockpile of spill cleanup materials where it will be readily accessible.
- Train employees in spill prevention and cleanup.
- Designate responsible individuals.

#### Cleanup

- Clean up leaks and spills immediately.
- On paved surfaces, clean up spills with as little water as possible. Use a rag for small spills, a damp mop for general cleanup, and absorbent material for larger spills. If the spilled material is hazardous, then the used cleanup materials are also hazardous and must be sent to either a certified laundry (rags) or disposed of as hazardous waste.
- Never hose down or bury dry material spills. Clean up as much of the material as possible and dispose of properly. See the waste management BMPs in this chapter for specific information.

#### Reporting

- Report significant spills to local agencies, such as the Fire Department; they can assist in cleanup.
- Federal regulations require that any significant oil spill into a water body or onto an adjoining shoreline be reported to the National Response Center (NRC) at 800-424-8802 (24 hour).

### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA12



Best Management Practices

## ACTIVITY: SPILL PREVENTION AND CONTROL (Continue)

Use the following measures related to specific activities:

### Vehicle and Equipment Maintenance

- If maintenance must occur on-site, use a designated area and/or a secondary containment, located away from drainage courses, to prevent the runoff of storm water and the runoff of spills.
- Regularly inspect on-site vehicles and equipment for leaks, and repair immediately.
- Check incoming vehicles and equipment (including delivery trucks, and employee and subcontractor vehicles) for leaking oil and fluids. Do not allow leaking vehicles or equipment on-site.
- Always use secondary containment, such as a drain pan or drop cloth, to catch spills or leaks when removing or changing fluids.
- Place drip pans or absorbent materials under paving equipment when not in use.
- Use adsorbent materials on small spills rather than hosing down or burying the spill. Remove the adsorbent materials promptly and dispose of properly.
- Promptly transfer used fluids to the proper waste or recycling drums. Don't leave full drip pans or other open containers lying around.
- Oil filters disposed of in trash cans or dumpsters can leak oil and pollute storm water. Place the oil filter in a funnel over a waste oil recycling drum to drain excess oil before disposal. Oil filters can also be recycled. Ask your oil supplier or recycler about recycling oil filters.
- Store cracked batteries in a non-leaking secondary container. Do this with all cracked batteries, even if you think all the acid has drained out. If you drop a battery, treat it as if it is cracked. Put it into the containment area until you are sure it is not leaking.

### Vehicle and Equipment Fueling

- If fueling must occur on-site, use designated areas, located away from drainage courses, to prevent the runoff of storm water and the runoff of spills.
- Discourage "topping-off" of fuel tanks.
- Always use secondary containment, such as a drain pan, when fueling to catch spills/leaks.

### REQUIREMENTS

- Costs (Capital, O&M)
  - Prevention of leaks and spills is inexpensive. Treatment and/or disposal of contaminated soil or water can be quite expensive.
- Maintenance
  - Keep ample supplies of spill control and cleanup materials on-site, near storage, unloading, and maintenance areas.
  - Update your spill prevention and control plan and stock cleanup materials as changes occur in the types of chemicals on-site.

### LIMITATIONS

- If necessary, use a private spill cleanup company.

### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

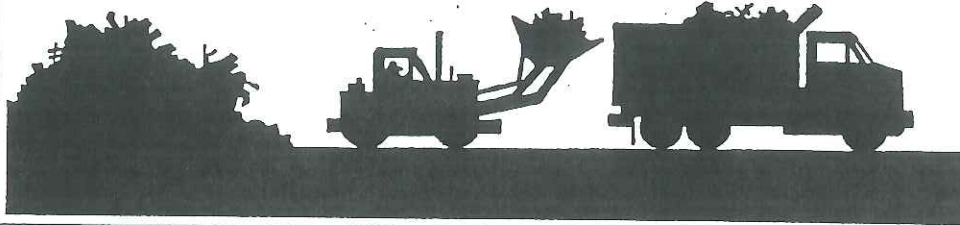
Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA12



## ACTIVITY: SOLID WASTE MANAGEMENT

Graphic: North Central Texas COG, 1993



### Objectives

Housekeeping Practices

Contain Waste

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from solid or construction waste by providing designated waste collection areas and containers, arranging for regular disposal, and training employees and subcontractors.

### APPROACH

Solid waste is one of the major pollutants resulting from construction. Construction debris includes:

- Solid waste generated from trees and shrubs removed during land clearing, demolition of existing structures (rubble), and building construction;
- Packaging materials including wood, paper and plastic;
- Scrap or surplus building materials including scrap metals, rubber, plastic, glass pieces, and masonry products; and
- Domestic wastes including food containers such as beverage cans, coffee cups, paper bags, and plastic wrappers, and cigarettes.

The following steps will help keep a clean site and reduce storm water pollution:

- Select designated waste collection areas on-site.
- Inform trash hauling contractors that you will accept only water-tight dumpsters for on-site use. Inspect dumpsters for leaks and repair any dumpster that is not water tight.
- Locate containers in a covered area and/or in a secondary containment.
- Provide an adequate number of containers with lids or covers that can be placed over the container to keep rain out or to prevent loss of wastes when it's windy.
- Plan for additional containers and more frequent pickup during the demolition phase of construction.
- Collect site trash daily, especially during rainy and windy conditions.
- Erosion and sediment control devices tend to collect litter. Remove this solid waste promptly.
- Make sure that toxic liquid wastes (used oils, solvents, and paints) and chemicals (acids, pesticides, additives, curing compounds) are not disposed of in dumpsters designated for construction debris.
- Salvage or recycle any useful material. For example, trees and shrubs from land clearing can be used as a brush barrier (see ESC53), or converted into wood chips, then used as mulch on graded areas (see ESC11).
- Do not hose out dumpsters on the construction site. Leave dumpster cleaning to trash hauling contractor.
- Arrange for regular waste collection before containers overflow.

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA20



## ACTIVITY: SOLID WASTE MANAGEMENT (Continue)

- If a container does spill, clean up immediately.
- Make sure that construction waste is collected, removed, and disposed of only at authorized disposal areas.
- Train employees and subcontractors in proper solid waste management.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Collect site trash daily.
  - Inspect construction waste area regularly.
  - Arrange for regular waste collection.

### LIMITATIONS

- There are no major limitations to this best management practice.

### REFERENCES

Best Management Practices and Erosion Control Manual for Construction Sites; Flood Control District of Maricopa County, AZ, September 1992.

Processes, Procedures, and Methods to Control Pollution Resulting from all Construction Activity; USEPA, 430/9-73-007, 1973.

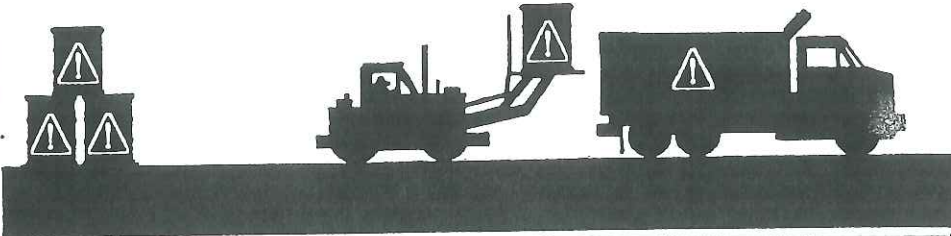
Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA20



## ACTIVITY: HAZARDOUS WASTE MANAGEMENT

Graphic: North Central Texas COG, 1993



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from hazardous waste through proper material use, waste disposal, and training of employees and subcontractors.

### APPROACH

Many of the chemicals used on-site can be hazardous materials which become hazardous waste upon disposal. These wastes may include:

- Paints and solvents;
- Petroleum products such as oils, fuels, and grease;
- Herbicides and pesticides;
- Acids for cleaning masonry; and
- Concrete curing compounds.

In addition, sites with existing structures may contain wastes which must be disposed of in accordance with Federal, State, and local regulations. These wastes include:

- Sandblasting grit mixed with lead-, cadmium-, or chromium-based paints;
- Asbestos; and
- PCBs (particularly in older transformers).

The following steps will help reduce storm water pollution from hazardous wastes:

#### Material Use

- Use all of the product before disposing of the container.
- Do not remove the original product label, it contains important safety and disposal information.
- Do not over-apply herbicides and pesticides. Prepare only the amount needed. Follow the recommended usage instructions. Over-application is expensive and environmentally harmful. Apply surface dressings in several smaller applications, as opposed to one large application, to allow time for infiltration and to avoid excess material being carried off-site by runoff. Do not apply these chemicals just before it rains. People applying pesticides must be certified in accordance with Federal and State regulations.
- Do not clean out brushes or rinse paint containers into the dirt, street, gutter, storm drain, or stream. "Paint out" brushes as much as possible. Rinse water-based paints to the sanitary sewer. Filter and re-use thinners and solvents. Dispose of excess oil-based paints and sludge as hazardous waste.

### Objectives

*Housekeeping Practices*

**Contain Waste**

*Minimize Disturbed Areas*

*Stabilize Disturbed Areas*

*Protect Slopes/Channels*

*Control Site Perimeter*

*Control Internal Erosion*

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA21





## ACTIVITY: HAZARDOUS WASTE MANAGEMENT (Continue)

### Waste Recycling/Disposal

- Select designated hazardous waste collection areas on-site.
- Hazardous materials and wastes should be stored in covered containers and protected from vandalism.
- Place hazardous waste containers in secondary containment.
- Do not mix wastes, this can cause chemical reactions, make recycling impossible, and complicate disposal.
- Recycle any useful material such as used oil or water-based paint.
- Make sure that toxic liquid wastes (used oils, solvents, and paints) and chemicals (acids, pesticides, additives, curing compounds) are not disposed of in dumpsters designated for construction debris.
- Arrange for regular waste collection before containers overflow.
- Make sure that hazardous waste (e.g. excess oil-based paint and sludges) is collected, removed, and disposed of only at authorized disposal areas.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### Training

- Train employees and subcontractors in proper hazardous waste management.
- Warning signs should be placed in areas recently treated with chemicals.
- Place a stockpile of spill cleanup materials where it will be readily accessible.
- If a container does spill, clean up immediately.

### **REQUIREMENTS**

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Inspect hazardous waste receptacles and area regularly.
  - Arrange for regular hazardous waste collection.

### **LIMITATIONS**

- Hazardous waste that cannot be reused or recycled must be disposed of by a licensed hazardous waste hauler.

### **REFERENCES**

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

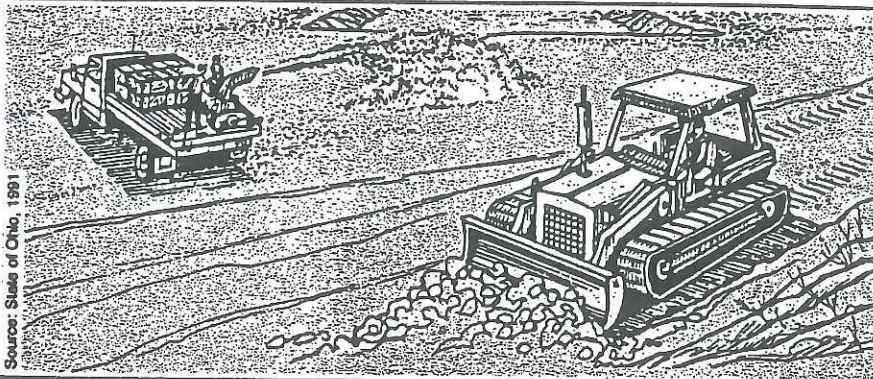
Processes, Procedures, and Methods to Control Pollution Resulting from all Construction Activity; USEPA, 430/9-73-007, 1973.

Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA21



## ACTIVITY: CONTAMINATED SOIL MANAGEMENT



### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from contaminated soil and highly acidic or alkaline soils by conducting pre-construction surveys, inspecting excavations regularly, and remediating contaminated soil promptly.

### APPROACH

Contaminated soils may occur on your site for several reasons including:

- Past site uses and activities;
- Detected or undetected spills and leaks; and
- Acid or alkaline solutions from exposed soil or rock formations high in acid or alkaline-forming elements.

Most developers conduct pre-construction environmental assessments as a matter of routine. Recent court rulings holding contractors liable for cleanup costs when they unknowingly move contaminated soil, highlight the need for contractors to confirm that a site assessment is completed before earth moving begins.

The following steps will help reduce storm water pollution from contaminated soil:

- Conduct thorough site planning including pre-construction geologic surveys.
- Look for contaminated soil as evidenced by discoloration, odors, differences in soil properties, abandoned underground tanks or pipes, or buried debris.
- Prevent leaks and spills to the maximum extent practicable. Contaminated soil can be expensive to treat and/or dispose of properly. However, addressing the problem before construction is much less expensive than after the structures are in place.
- Test suspected soils at a certified laboratory.
- If the soil is contaminated, work with the local regulatory agencies to develop options for treatment and/or disposal.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - Prevention of leaks and spills is inexpensive. Treatment and/or disposal of contaminated soil can be quite expensive.
- Maintenance
  - Inspect excavated areas daily for signs of contaminated soil.
  - Implement CA12, Spill Prevention and Control, to prevent leaks and spills as much as possible.

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA22



## ACTIVITY: CONTAMINATED SOIL MANAGEMENT (Continue)

### LIMITATIONS

- Contaminated soils that cannot be treated on-site must be disposed of off-site by a licensed hazardous waste hauler.
- The presence of contaminated soil may indicate contaminated water as well. See CA1 (Dewatering Operations) in this chapter for more information.

### REFERENCES

Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

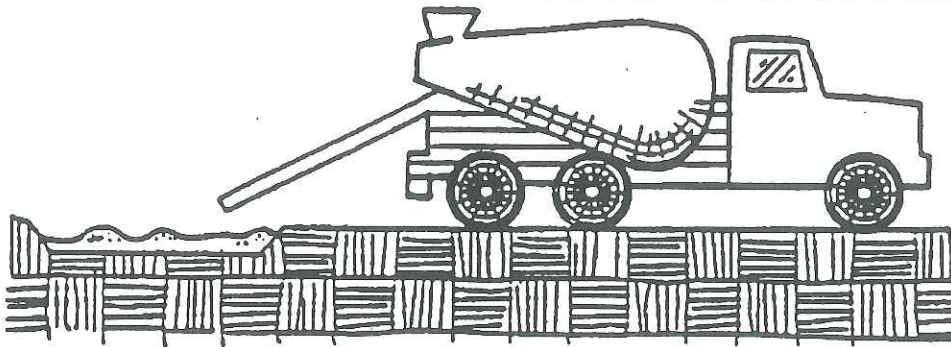
Processes, Procedures, and Methods to Control Pollution Resulting from all Construction Activity; USEPA, 430/9-73-007, 1973.

Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA22



## ACTIVITY: CONCRETE WASTE MANAGEMENT



### Objectives

Housekeeping Practices

**Contain Waste**

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from concrete waste by conducting washout off-site, performing on-site washout in a designated area, and training employees and subcontractors.

### APPROACH

The following steps will help reduce storm water pollution from concrete wastes:

- Store dry and wet materials under cover, away from drainage areas.
- Avoid mixing excess amounts of fresh concrete or cement on-site.
- Perform washout of concrete trucks off site or in designated areas only.
- Do not wash out concrete trucks into storm drains, open ditches, streets, or streams.
- Do not allow excess concrete to be dumped on-site, except in designated areas.
- For on-site washout:
  - locate washout area at least 50 feet from storm drains, open ditches, or water bodies. Do not allow runoff from this area by constructing a temporary pit or bermed area large enough for liquid and solid waste;
  - wash out wastes into the temporary pit where the concrete can set, be broken up, and then disposed of properly.
- When washing concrete to remove fine particles and expose the aggregate, avoid creating runoff by draining the water to a bermed or level area.
- Do not wash sweepings from exposed aggregate concrete into the street or storm drain. Collect and return sweepings to aggregate base stock pile, or dispose in the trash.
- Train employees and subcontractors in proper concrete waste management.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Inspect subcontractors to ensure that concrete wastes are being properly managed.
  - If using a temporary pit, dispose hardened concrete on a regular basis.

### LIMITATIONS

- Off-site washout of concrete wastes may not always be possible.

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA23



Best Management Practices

## ACTIVITY: CONCRETE WASTE MANAGEMENT (Continue)

### REFERENCES

Best Management Practices and Erosion Control Manual for Construction Sites; Flood Control District of Maricopa County, AZ, July 1992.

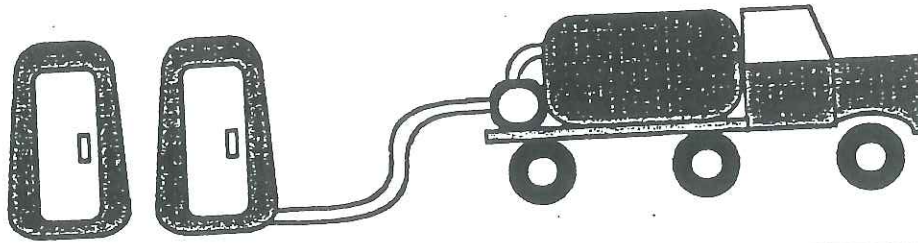
Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

CA23



## ACTIVITY: SANITARY/SEPTIC WASTE MANAGEMENT



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from sanitary/septic waste by providing convenient, well-maintained facilities, and arranging for regular service and disposal.

### APPROACH

Sanitary or septic wastes should be treated or disposed of in accordance with State and local requirements. These requirements may include:

- Locate sanitary facilities in a convenient location.
- Untreated raw wastewater should never be discharged or buried.
- Temporary septic systems should treat wastes to appropriate levels before discharging.
- If using an on-site disposal system (OSDS), such as a septic system, comply with local health agency requirements.
- Temporary sanitary facilities that discharge to the sanitary sewer system should be properly connected to avoid illicit discharges.
- If discharging to the sanitary sewer, contact the local wastewater treatment plant for their requirements.
- Sanitary/septic facilities should be maintained in good working order by a licensed service.
- Arrange for regular waste collection by a licensed hauler before facilities overflow.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Inspect facilities regularly.
  - Arrange for regular waste collection.

### LIMITATIONS

- There are no major limitations to this best management practice.

### REFERENCES

Best Management Practices and Erosion Control Manual for Construction Sites; Flood Control District of Maricopa County, AZ, September 1992.

Storm Water Management for Construction Activities, Developing Pollution Prevention Plans and Best Management Practices, EPA 832-R-92005; USEPA, April 1992.

### Objectives

- Housekeeping Practices
  - Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA24



March, 1993

# ACTIVITY: VEHICLE AND EQUIPMENT CLEANING

Graphic: North Central Texas COG, 1993



## Objectives

Housekeeping Practices

Contain Waste

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

## DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from vehicle and equipment cleaning by using off-site facilities, washing in designated, contained areas only, eliminating discharges to the storm drain by infiltrating or recycling the wash water, and/or training employees and subcontractors.

## APPROACH

- Use off-site commercial washing businesses as much as possible. Washing vehicles and equipment outdoors or in areas where wash water flows onto paved surfaces or into drainage pathways can pollute storm water. If you wash a large number of vehicles or pieces of equipment, consider conducting this work at an off-site commercial business. These businesses are better equipped to handle and dispose of the wash waters properly. Performing this work off-site can also be economical by eliminating the need for a separate washing operation at your site.
- If washing must occur on-site, use designated, bermed wash areas to prevent wash water contact with storm water, creeks, rivers, and other water bodies. The wash area can be sloped for wash water collection and subsequent infiltration into the ground.
- Use as little water as possible to avoid having to install erosion and sediment controls for the wash area.
- Use phosphate-free, biodegradable soaps.
- Educate employees and subcontractors on pollution prevention measures.
- Do not permit steam cleaning on-site. Steam cleaning can generate significant pollutant concentrations.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

## REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Minimal, some berm repair may be necessary.

## LIMITATIONS

- Even phosphate-free, biodegradable soaps have been shown to be toxic to fish before the soap degrades.
- Sending vehicles/equipment off-site should be done in conjunction with ESC24 (Stabilized Construction Entrance).

## REFERENCE

Swisher, R.D., 1987. Surfactant Biodegradation, Marcel Decker Corporation

## Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

## Implementation Requirements

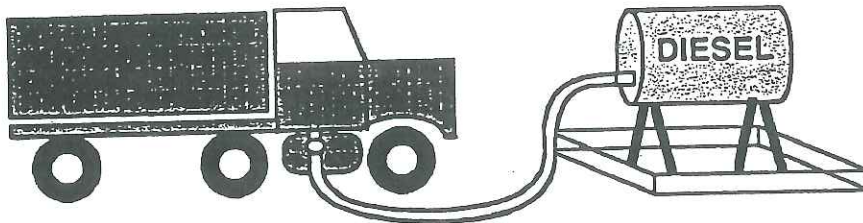
- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

**CA30**



## ACTIVITY: VEHICLE AND EQUIPMENT FUELING



### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### DESCRIPTION

Prevent fuel spills and leaks, and reduce their impacts to storm water by using off-site facilities, fueling in designated areas only, enclosing or covering stored fuel, implementing spill controls, and training employees and subcontractors.

### APPROACH

- Use off-site fueling stations as much as possible. Fueling vehicles and equipment outdoors or in areas where fuel may spill/leak onto paved surfaces or into drainage pathways can pollute storm water. If you fuel a large number of vehicles or pieces of equipment, consider using an off-site fueling station. These businesses are better equipped to handle fuel and spills properly. Performing this work off-site can also be economical by eliminating the need for a separate fueling area at your site.
- If fueling must occur on-site, use designated areas, located away from drainage courses, to prevent the runoff of storm water and the runoff of spills.
- Discourage "topping-off" of fuel tanks.
- Always use secondary containment, such as a drain pan or drop cloth, when fueling to catch spills/leaks.
- Place a stockpile of spill cleanup materials where it will be readily accessible.
- Use adsorbent materials on small spills rather than hosing down or burying the spill. Remove the adsorbent materials promptly and dispose of properly.
- Carry out all Federal and State requirements regarding stationary above ground storage tanks.
- Avoid mobile fueling of mobile construction equipment around the site; rather, transport the equipment to designated fueling areas. With the exception of tracked equipment such as bulldozers and perhaps forklifts, most vehicles should be able to travel to a designated area with little lost time.
- Train employees and subcontractors in proper fueling and cleanup procedures.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above measures are low cost, except for the capital costs of above ground tanks that meet all local environmental, zoning, and fire codes.
- Maintenance
  - Keep ample supplies of spill cleanup materials on-site.
  - Inspect fueling areas and storage tanks on a regular schedule.

### LIMITATIONS

- Sending vehicles/equipment off-site should be done in conjunction with ESC24 (Stabilized Construction Entrance).

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA31

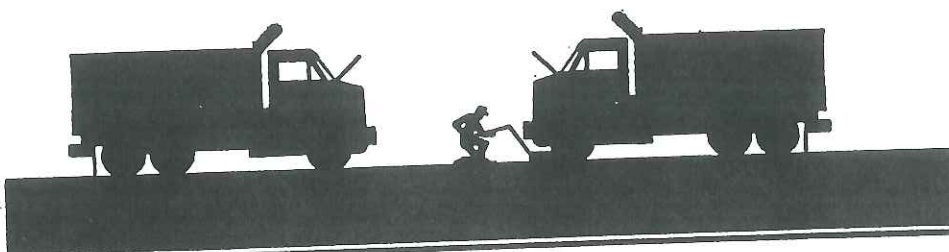


Best Management Practices



## ACTIVITY: VEHICLE AND EQUIPMENT MAINTENANCE

Graphic: North Central Texas COG, 1993



### DESCRIPTION

Prevent or reduce the discharge of pollutants to storm water from vehicle and equipment maintenance by running a "dry site". This involves using off-site facilities, performing work in designated areas only, providing cover for materials stored outside, checking for leaks and spills, containing and cleaning up spills immediately, and training employees and subcontractors.

### APPROACH

- Keep vehicles and equipment clean, don't allow excessive build-up of oil and grease.
- Use off-site repair shops as much as possible. Maintaining vehicles and equipment outdoors or in areas where vehicle or equipment fluids may spill or leak onto the ground can pollute storm water. If you maintain a large number of vehicles or pieces of equipment, consider using an off-site repair shop. These businesses are better equipped to handle vehicle fluids and spills properly. Performing this work off-site can also be economical by eliminating the need for a separate maintenance area.
- If maintenance must occur on-site, use designated areas, located away from drainage courses, to prevent the runoff of storm water and the runoff of spills.
- Always use secondary containment, such as a drain pan or drop cloth, to catch spills or leaks when removing or changing fluids.
- Place a stockpile of spill cleanup materials where it will be readily accessible.
- Use adsorbent materials on small spills rather than hosing down or burying the spill. Remove the adsorbent materials promptly and dispose of properly.
- Regularly inspect on-site vehicles and equipment for leaks, and repair immediately.
- Check incoming vehicles and equipment (including delivery trucks, and employee and subcontractor vehicles) for leaking oil and fluids. Do not allow leaking vehicles or equipment on-site.
- Segregate and recycle wastes, such as greases, used oil or oil filters, antifreeze, cleaning solutions, automotive batteries, hydraulic, and transmission fluids.
- Train employees and subcontractors in proper maintenance and spill cleanup procedures.
- For a quick reference on disposal alternatives for specific wastes, see Table 4.2, CA40, Employee/Subcontractor Training.

### REQUIREMENTS

- Costs (Capital, O&M)
  - All of the above are low cost measures.
- Maintenance
  - Keep ample supplies of spill cleanup materials on-site.
  - Inspect maintenance areas on a regular schedule.

### Objectives

#### Housekeeping Practices

- Contain Waste
- Minimize Disturbed Areas
- Stabilize Disturbed Areas
- Protect Slopes/Channels
- Control Site Perimeter
- Control Internal Erosion

### Targeted Pollutants

- Sediment
- Nutrients
- Toxic Materials
- Oil & Grease
- Floatable Materials
- Other Construction Waste

- Likely to Have Significant Impact
- Probable Low or Unknown Impact

### Implementation Requirements

- Capital Costs
- O&M Costs
- Maintenance
- Training
- Suitability for Slopes >5%

- High
- Low

## CA32



## ACTIVITY: VEHICLE AND EQUIPMENT MAINTENANCE (Continue)

### LIMITATIONS

- Sending vehicles/equipment off-site should be done in conjunction with ESC24 (Stabilized Construction Entrance).

Outdoor vehicle or equipment maintenance is a potentially significant source of storm water pollution. Activities that can contaminate storm water include engine repair and service, particularly changing or replacement of fluids, and outdoor equipment storage and parking (dripping engines). For further information on vehicle or equipment servicing, see CA30, Vehicle and Equipment Cleaning, and CA31, Vehicle and Equipment Fueling.

Listed below is further information if you must perform vehicle or equipment maintenance on-site.

### Waste Reduction

Parts are often cleaned using solvents such as trichloroethylene, 1,1,1-trichloroethane, or methylene chloride. Many of these parts cleaners are harmful and must be disposed of as a hazardous waste. Reducing the number of solvents makes recycling easier and reduces hazardous waste management costs. Often, one solvent can perform a job as well as two different solvents. Also, if possible, eliminate or reduce the amount of hazardous materials and waste by substituting non-hazardous or less hazardous materials. For example, replace chlorinated organic solvents (1,1,1-trichloroethane, methylene chloride, etc.) with non-chlorinated solvents. Non-chlorinated solvents like kerosene or mineral spirits are less toxic and less expensive to dispose of properly. Check list of active ingredients to see whether it contains chlorinated solvents. The "chlor" term indicates that the solvent is chlorinated. Also, try substituting a wire brush for solvents to clean parts.

### Recycling/Disposal

Separating wastes allows for easier recycling and may reduce disposal costs. Keep hazardous and non-hazardous wastes separate, do not mix used oil and solvents, and keep chlorinated solvents (like 1,1,1-trichloroethane) separate from non-chlorinated solvents (like kerosene and mineral spirits). Promptly transfer used fluids to the proper waste or recycling drums. Don't leave full drip pans or other open containers lying around.

Oil filters disposed of in trash cans or dumpsters can leak oil and contaminate storm water. Place the oil filter in a funnel over a waste oil recycling drum to drain excess oil before disposal. Oil filters can also be recycled. Ask your oil supplier or recycler about recycling oil filters.

Do not dispose of extra paints and coatings by dumping liquid onto the ground or throwing it into dumpsters. Allow coatings to dry or harden before disposal into covered dumpsters.

Store cracked batteries in a non-leaking secondary container. Do this with all cracked batteries, even if you think all the acid has drained out. If you drop a battery, treat it as if it is cracked. Put it into the containment area until you are sure it is not leaking.

Do not bury used tires.

### REFERENCES

Best Management Practices and Erosion Control Manual for Construction Sites; Flood Control District of Maricopa County, AZ, September 1992.

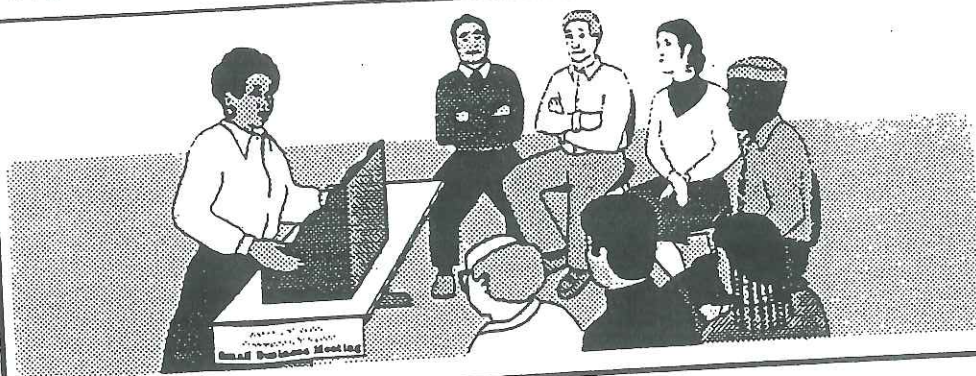
Blueprint for a Clean Bay-Construction-Related Industries: Best Management Practices for Storm Water Pollution Prevention; Santa Clara Valley Nonpoint Source Pollution Control Program, 1992.

Coastal Nonpoint Pollution Control Program: Program Development and Approval Guidance, Working Group Working Paper; USEPA, April 1992.

CA32



## ACTIVITY: EMPLOYEE/SUBCONTRACTOR TRAINING



### Objectives

Housekeeping Practices

Contain Waste

Minimize Disturbed Areas

Stabilize Disturbed Areas

Protect Slopes/Channels

Control Site Perimeter

Control Internal Erosion

### DESCRIPTION

Employee/subcontractor training, like maintenance or a piece of equipment, is not so much a best management practice as it is a method by which to implement BMPs. This fact sheet highlights the importance of training and of integrating the elements of employee/subcontractor training from the individual source controls into a comprehensive training program as part of a company's Storm Water Pollution Prevention Plan (SWPPP).

The specific employee/subcontractor training aspects of each of the source controls are highlighted in the individual fact sheets. The focus of this fact sheet is more general, and includes the overall objectives and approach for assuring employee/subcontractor training in storm water pollution prevention. Accordingly, the organization of this fact sheet differs somewhat from the other fact sheets in this chapter.

### OBJECTIVES

Employee/subcontractor training should be based on four objectives:

- Promote a clear identification and understanding of the problem, including activities with the potential to pollute storm water;
- Identify solutions (BMPs);
- Promote employee/subcontractor ownership of the problems and the solutions; and
- Integrate employee/subcontractor feedback into training and BMP implementation.

### APPROACH

- Integrate training regarding storm water quality management with existing training programs that may be required for your business by other regulations such as: the Illness and Injury Prevention Program (IIPP) (SB 198) (California Code of Regulations Title 8, Section 3203), the Hazardous Waste Operations and Emergency Response (HAZWOPER) standard (29 CFR 1910.120), the Spill Prevention Control and Countermeasure (SPCC) Plan (40 CFR 112), and the Hazardous Materials Management Plan (Business Plan) (California Health and Safety Code, Section 6.95).
- Businesses, particularly smaller ones that may not be regulated by Federal, State, or local regulations, may use the information in this Handbook to develop a training program to reduce their potential to pollute storm water.
- Use the quick reference on disposal alternatives (Table 4.2) to train employee/subcontractors in proper and consistent methods for disposal.

# CA40



March, 1993

## ACTIVITY: EMPLOYEE/SUBCONTRACTOR TRAINING (Continue)

- Consider posting the quick reference table around the job site or in the on-site office trailer to reinforce training.
- Train employee/subcontractors in standard operating procedures and spill cleanup techniques described in the fact sheets. Employee/subcontractors trained in spill containment and cleanup should be present during the loading/unloading and handling of materials.
- Personnel who use pesticides should be trained in their use. The California Department of Pesticide Regulation and county agricultural commissioners license pesticide dealers, certify pesticide applicators, and conduct on-site inspections.
- Proper education of off-site contractors is often overlooked. The conscientious efforts of well trained employee/subcontractors can be lost by unknowing off-site contractors, so make sure they are well informed about what they are expected to do on-site.

CA40



TABLE 4.2 QUICK REFERENCE - DISPOSAL ALTERNATIVES  
(Adopted from Santa Clara County Nonpoint Source Pollution Control Program - December 1992)

All of the waste products on this chart are prohibited from discharge to the storm drain system. Use this matrix to decide which alternative disposal strategies to use.  
**ALTERNATIVES ARE LISTED IN PRIORITY ORDER.**

Key: HHW Household hazardous waste (Government-sponsored drop-off events)  
 POTW Publically Owned Treatment Plant  
 Reg.Bd. Regional Water Quality Control Board (Oakland)  
 "Dispose to sanitary sewer" means dispose into sink, toilet, or sanitary sewer clean-out connection.  
 "Dispose as trash" means dispose in dumpsters or trash containers for pickup and/or eventual disposal in landfill.  
 "Dispose as hazardous waste" for business/commercial means contract with a hazardous waste hauler to remove and dispose.

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
<b>General Construction and Painting; Street and Utility Maintenance</b>			
Excess paint (oil-based)	1. Recycle/reuse. 2. Dispose as hazardous waste.		1. Recycle/reuse. 2. Take to HHW drop-off.
Excess paint (water-based)	1. Recycle/reuse. 2. Dry residue in cans, dispose as trash. 3. If volume is too much to dry, dispose as hazardous waste.		1. Recycle/reuse. 2. Dry residue in cans, dispose as trash. 3. If volume is too much to dry, take to HHW drop-off
Paint cleanup (oil-based)	Wipe paint out of brushes, then: 1. Filter & reuse thinners, solvents. 2. Dispose as hazardous waste.		Wipe paint out of brushes, then: 1. Filter & reuse thinners, solvents. 2. Take to HHW drop-off.
Paint cleanup (water-based)	Wipe paint out of brushes, then: 1. Rinse to sanitary sewer.		Wipe paint out of brushes, then: 1. Rinse to sanitary sewer.
Empty paint cans (dry)	1. Remove lids, dispose as trash.		1. Remove lids, dispose as trash.
Paint stripping (with solvent)	1. Dispose as hazardous waste.		1. Take to HHW drop-off.
Building exterior cleaning (high-pressure water)	1. Prevent entry into storm drain and remove offsite 2. Wash onto dirt area, spade in 3. Collect (e.g. mop up) and discharge to sanitary sewer	POTW	
Cleaning of building exteriors which have HAZARDOUS MATERIALS (e.g. mercury, lead) in paints	1. Use dry cleaning methods 2. Contain and dispose washwater as hazardous waste (Suggestion: dry material first to reduce volume)		

Table 4.1 (Continued)  
Page 2

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
<b>General Construction and Painting; Street and Utility Maintenance (cont'd)</b>			
Non-hazardous paint scraping/sand blasting	1. Dry sweep, dispose as trash		1. Dry sweep, dispose as trash
<b>HAZARDOUS</b> paint scraping/sand blasting (e.g. marine paints or paints containing lead or tributyl tin)	1. Dry sweep, dispose as hazardous waste		1. Dry sweep, take to HHW drop-off
Soil from excavations during periods when storms are forecast	1. Should not be placed in street or on paved areas 2. Remove from site or backfill by end of day 3. Cover with tarpaulin or surround with hay bales, or use other runoff controls 4. Place filter mat over storm drain Note: Thoroughly sweep following removal of dirt in all four alternatives.		
Soil from excavations placed on paved surfaces during periods when storms are not forecast	1. Keep material out of storm conveyance systems and thoroughly remove via sweeping following removal of dirt		
Cleaning streets in construction areas	1. Dry sweep and minimize tracking of mud 2. Use silt ponds and/or similar pollutant reduction techniques when flushing pavement		
Soil erosion, sediments	1. Cover disturbed soils, use erosion controls, block entry to storm drain. 2. Seed or plant immediately.		
Fresh cement, grout, mortar	1. Use/reuse excess 2. Dispose to trash		1. Use/reuse excess 2. Dispose as trash
Washwater from concrete/mortar (etc.) cleanup	1. Wash onto dirt area, spade in 2. Pump and remove to appropriate disposal facility 3. Settle, pump water to sanitary sewer	POTW	1. Wash onto dirt area, spade in 2. Pump and remove to appropriate disposal facility 3. Settle, pump water to sanitary sewer
Aggregate wash from driveway/patio construction	1. Wash onto dirt area, spade in 2. Pump and remove to appropriate disposal facility		1. Wash onto dirt area, spade in 2. Pump and remove to appropriate disposal facility

Table 4.1 (Continued)  
Page 3

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
<b>General Construction and Painting; Street and Utility Maintenance (cont'd)</b>			
Rinsewater from concrete mixing trucks	<ol style="list-style-type: none"> <li>1. Return truck to yard for rinsing into pond or dirt area</li> <li>2. At construction site, wash into pond or dirt area</li> </ol>		
Non-hazardous construction and demolition debris	<ol style="list-style-type: none"> <li>1. Recycle/reuse (concrete, wood, etc.)</li> <li>2. Dispose as trash</li> </ol>		<ol style="list-style-type: none"> <li>1. Recycle/reuse (concrete, wood, etc.)</li> <li>2. Dispose as trash</li> </ol>
Hazardous demolition and construction debris (e.g. asbestos)	<ol style="list-style-type: none"> <li>1. Dispose as hazardous waste</li> </ol>		<ol style="list-style-type: none"> <li>1. Do not attempt to remove yourself. Contact asbestos removal service for safe removal and disposal</li> <li>2. Very small amounts (less than 5 lbs) may be double-wrapped in plastic and taken to HHW drop-off</li> </ol>
Saw-cut slurry	<ol style="list-style-type: none"> <li>1. Use dry cutting technique and sweep up residue</li> <li>2. Vacuum slurry and dispose off-site.</li> <li>3. Block storm drain or berm with low weir as necessary to allow most solids to settle. Shovel out gutters; dispose residue to dirt area, construction yard or landfill.</li> </ol>		
Construction dewatering (Nonturbid, uncontaminated groundwater)	<ol style="list-style-type: none"> <li>1. Recycle/Reuse</li> <li>2. Discharge to storm drain</li> </ol>		
Construction dewatering (Other than nonturbid, uncontaminated groundwater)	<ol style="list-style-type: none"> <li>1. Recycle/reuse</li> <li>2. Discharge to sanitary sewer</li> <li>3. As appropriate, treat prior to discharge to storm drain</li> </ol>	POTW Reg. Bd.	
Portable toilet waste	<ol style="list-style-type: none"> <li>1. Leasing company shall dispose to sanitary sewer at POTW</li> </ol>	POTW	
Leaks from garbage dumpsters	<ol style="list-style-type: none"> <li>1. Collect, contain leaking material. Eliminate leak, keep covered, return to leasing company for immediate repair</li> <li>2. If dumpster is used for liquid waste, use plastic liner</li> </ol>		

Table 4.1 (Continued)  
Page 4

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
<b>General Construction and Painting; Street and Utility Maintenance (cont'd)</b>			
Leaks from construction debris bins	1. Insure that bins are used for dry nonhazardous materials only (Suggestion: Fencing, covering help prevent misuse)		
Dumpster cleaning water	1. Clean at dumpster owner's facility and discharge waste through grease interceptor to sanitary sewer 2. Clean on site and discharge through grease interceptor to sanitary sewer	POTW POTW	
Cleaning driveways, paved areas * (Special Focus = Restaurant alleys Grocery dumpster areas)  * Note: Local drought ordinances may contain additional restrictions	1. Sweep and dispose as trash (Dry cleaning only). 2. For vehicle leaks, restaurant/grocery alleys, follow this 3-step process: a. Clean up leaks with rags or absorbents. b. Sweep, using granular absorbent material (cat litter). c. Mop and dispose of mopwater to sanitary sewer (or collect rinsewater and pump to the sanitary sewer). 3. Same as 2 above, but with rinsewater (2c)(no soap) discharged to storm drain.		1. Sweep and dispose as trash (Dry cleaning only). 2. For vehicle leaks, follow this 3-step process: a. Clean up leaks with rags or absorbents; dispose as hazardous waste. b. Sweep, using granular absorbent material (cat litter). c. Mop and dispose of mopwater to sanitary sewer.
Steam cleaning of sidewalks, plazas *	1. Collect all water and pump to sanitary sewer. 2. Follow this 3-step process: a. Clean oil leaks with rags or absorbents b. Sweep (Use dry absorbent as needed) c. Use no soap, discharge to storm drain		
Potable water/line flushing Hydrant testing	1. Deactivate chlorine by maximizing time water will travel before reaching creeks		
Super-chlorinated (above 1 ppm) water from line flushing	1. Discharge to sanitary sewer 2. Complete dechlorination required before discharge to storm drain		



DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
Landscape/Garden Maintenance			
Pesticides	<ol style="list-style-type: none"> <li>Use up. Rinse containers use rinsewater as product. Dispose rinsed containers as trash</li> <li>Dispose unused pesticide as hazardous waste</li> </ol>		<ol style="list-style-type: none"> <li>Use up. Rinse containers, use rinsewater as pesticide. Dispose rinsed container as trash.</li> <li>Take unused pesticide to HHW drop-off</li> </ol>
Garden clippings	<ol style="list-style-type: none"> <li>Compost</li> <li>Take to Landfill</li> </ol>		<ol style="list-style-type: none"> <li>Compost</li> <li>Dispose as trash.</li> </ol>
Tree trimming	<ol style="list-style-type: none"> <li>Chip if necessary, before composting or recycling</li> </ol>		<ol style="list-style-type: none"> <li>Chip if necessary, before composting or recycling</li> </ol>
Swimming pool, spa, fountain water (emptying)	<ol style="list-style-type: none"> <li>Do not use metal-based algicides (i.e. Copper Sulfate)</li> <li>Recycle/reuse (e.g. irrigation)</li> <li>Determine chlorine residual = 0, wait 24 hours and then discharge to storm drain.</li> </ol>	POTW	<ol style="list-style-type: none"> <li>Do not use metal-based algicides (i.e. Copper Sulfate)</li> <li>Recycle/reuse (e.g. irrigation)</li> <li>Determine chlorine residual = 0, wait 24 hours and then discharge to storm drain.</li> </ol>
Acid or other pool/spa/fountain cleaning	<ol style="list-style-type: none"> <li>Neutralize and discharge to sanitary sewer</li> </ol>	POTW	
Swimming pool, spa filter backwash	<ol style="list-style-type: none"> <li>Reuse for irrigation</li> <li>Dispose on dirt area</li> <li>Settle, dispose to sanitary sewer</li> </ol>		<ol style="list-style-type: none"> <li>Use for landscape irrigation</li> <li>Dispose on dirt area</li> <li>Settle, dispose to sanitary sewer</li> </ol>
Vehicle Wastes			
Used motor oil	<ol style="list-style-type: none"> <li>Use secondary containment while storing, send to recycler.</li> </ol>		<ol style="list-style-type: none"> <li>Put out for curbside recycling pickup where available</li> <li>Take to Recycling Facility or auto service facility with recycling program</li> <li>Take to HHW events accepting motor oil</li> </ol>
Antifreeze	<ol style="list-style-type: none"> <li>Use secondary containment while storing, send to recycler.</li> </ol>		<ol style="list-style-type: none"> <li>Take to Recycling Facility</li> </ol>
Other vehicle fluids and solvents	<ol style="list-style-type: none"> <li>Dispose as hazardous waste</li> </ol>		<ol style="list-style-type: none"> <li>Take to HHW event</li> </ol>
Automobile batteries	<ol style="list-style-type: none"> <li>Send to auto battery recycler</li> <li>Take to Recycling Center</li> </ol>		<ol style="list-style-type: none"> <li>Exchange at retail outlet</li> <li>Take to Recycling Facility or HHW event where batteries are accepted</li> </ol>
Motor home/construction trailer waste	<ol style="list-style-type: none"> <li>Use holding tank. Dispose to sanitary sewer</li> </ol>		<ol style="list-style-type: none"> <li>Use holding tank, dispose to sanitary sewer.</li> </ol>

Table 4.1 (Continued)  
Page 6

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities		Approval	RESIDENTIAL Disposal Priorities
Vehicle Wastes (cont'd)				
Vehicle Washing	<ol style="list-style-type: none"> <li>1. Recycle</li> <li>2. Discharge to sanitary sewer, never to storm drain</li> </ol>	POTW	<ol style="list-style-type: none"> <li>1. Take to Commercial Car Wash.</li> <li>2. Wash over lawn or dirt area</li> <li>3. If soap is used, use a bucket for soapy water and discharge remaining soapy water to sanitary sewer.</li> </ol>	
Mobile Vehicle Washing	<ol style="list-style-type: none"> <li>1. Collect washwater and discharge to sanitary sewer.</li> </ol>	POTW		
Rinsewater from dust removal at new car fleets	<ol style="list-style-type: none"> <li>1. Discharge to sanitary sewer</li> <li>2. If rinsing dust from exterior surfaces from appearance purposes, use no soap (water only); discharge to storm drain.</li> </ol>	POTW		
Vehicle leaks at Vehicle Repair Facilities	<p>Follow this 3-step process:</p> <ol style="list-style-type: none"> <li>1. Clean up leaks with rags or absorbents</li> <li>2. Sweep, using granular absorbent material (cat litter)</li> <li>3. Mop and dispose of mopwater to sanitary sewer.</li> </ol>			
Other Wastes			POTW	1. Dispose to sanitary sewer
Carpet cleaning solutions & other mobile washing services				
Roof drains	<ol style="list-style-type: none"> <li>1. Dispose to sanitary sewer</li> <li>1. If roof is contaminated with industrial waste products, discharge to sanitary sewer</li> <li>2. If no contamination is present, discharge to storm drain</li> </ol>			
Cooling water Air conditioning condensate	<ol style="list-style-type: none"> <li>1. Recycle/reuse</li> <li>2. Discharge to sanitary sewer</li> </ol>	POTW		
Pumped groundwater, infiltration/foundation drainage (contaminated)	<ol style="list-style-type: none"> <li>1. Recycle/reuse (landscaping, etc.)</li> <li>2. Treat if necessary; discharge to sanitary sewer</li> <li>3. Treat and discharge to storm drain</li> </ol>	Reg. Bd. POTW Reg. Bd.		
Fire fighting flows	<p>If contamination is present, Fire Dept. will attempt to prevent flow to stream</p>			

Table 4.1 (Continued)  
Page 7

DISCHARGE/ACTIVITY	BUSINESS/COMMERCIAL Disposal Priorities	Approval	RESIDENTIAL Disposal Priorities
Other Wastes (cont'd) Kitchen Grease	<ol style="list-style-type: none"> <li>1. Provide secondary containment, collect, send to recycler.</li> <li>2. Provide secondary containment, collect, send to POTW via hauler.</li> </ol>	POTW	1. Collect, solidify, dispose as trash
Restaurant cleaning of floor mats, exhaust filters, etc.	<ol style="list-style-type: none"> <li>1. Clean inside building with discharge through grease trap to sanitary sewer.</li> <li>2. Clean outside in container or bermed area with discharge to sanitary sewer.</li> </ol>		
Clean-up wastewater from sewer back-up	<ol style="list-style-type: none"> <li>1. Follow this procedure:               <ol style="list-style-type: none"> <li>a. Block storm drain, contain, collect, and return spilled material to the sanitary sewer.</li> <li>b. Block storm drain, rinse remaining material to collection point and pump to sanitary sewer. (no rinse-water may flow to storm drain)</li> </ol> </li> </ol>		



**APPENDIX D - HYDROLOGY DESIGN STANDARDS, LAKE COUNTY**

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# HYDROLOGY DESIGN STANDARDS

## LAKE COUNTY

Lake County Department of Public Works  
Water Resources Division  
255 N. Forbes Street  
Lakeport, CA 95453  
(707)263-2341

Adopted \_\_\_\_\_, 1999

*DRAFT*  
*4/28/99*





These Standards provide design criteria and the methodology used to estimate peak flows for drainages within Lake County.

These Standards are based on information provided by the National Weather Service, the USDA Natural Resources Conservation Service, the California Department of Water Resources, and the California Department of Transportation.

It is the intent that these Standards be utilized for estimating flows in minor waterways (less than one square mile) with time of concentrations of less than two hours. For larger drainage areas, we recommend the use of more detailed calculations and/or models, such as TR20, TR-55, HEC-1 and HEC-HMS.

### WATERWAY DESIGN CRITERIA

A "waterway" is defined as being a natural or artificial channel or depression in the surface of the earth or an underground conduit system which provides a course for water flowing as a consequence of storm water runoff.

For the purposes of design criteria contained herein, waterways are divided into three classifications:

1. Major Waterways: having a tributary drainage area of four square miles or more; shall require a design frequency of re-occurrence of one in 100 years. This frequency would only apply to design in urban and suburban areas and not, for instance, agricultural channel design.
2. Secondary Waterways: having a tributary drainage area of between one and four square miles; shall require a design frequency of re-occurrence of once in 25 years.
3. Minor Waterways: having a tributary drainage area less than one square mile; shall require a design frequency of re-occurrence of once in 10 years.

Commercial sites, industrial sites, residential subdivisions, and manufactured home parks or subdivisions shall be designed to carry the 10-year storm in the storm drain system, and the 100-year storm within the confines of the streets. Secondary and major waterways passing through the site shall be designed to their respective design flows. All new building pads should be designed such that they are not inundated by a 100-year flood event from local drainage facilities. Flooding from regional sources will be considered on a case-by-case basis.

Best Management Practices (BMPs), such as filter strips and sedimentation basins, are usually designed for the 2-year event. BMP's designed for the 2-year event will properly treat over 90% of the flow during its life. Design criteria, such as included in the California Storm Water Best Management Practice Handbooks should be used.

Open channels should be designed with a minimum of six inches of freeboard at the design flow. Closed conduit systems should be designed with no surcharging at the design flow. Culvert inlets may be surcharged to efficiently use the culvert. To reduce routine maintenance, facilities should be designed with a self-cleansing velocity of 3 feet per second. Erosive velocities in unlined channels and culvert outlets should be minimized, or erosion resistant lining provided.

### ROADWAY DESIGN CRITERIA

Roadway drainage design is a matter of properly balancing technical principles and data with the environment giving due consideration to other factors such as safety and economics. Drainage features to remove runoff from the roadway and to convey surface and stream waters originating upstream of the roadway to the downstream side should be designed to accomplish these functions without causing objectionable backwater, excessive velocities or unduly affecting traffic safety. Chapters 800 to 890 of

the CALTRANS Highway Design Manual should be used for drainage design of public roadways within Lake County. The following minimum design standards apply to Lake County:

**Bridges/Major Culverts:** Design in conformance with Chapter 820. For Major Waterways and streams that are included in the Flood Insurance Study (FIS), a 100-year flood should be used for design purposes. Bridges over streams included in the FIS may not increase the base flood elevation more than one foot. If a floodway is present, the bridge may not encroach on the floodway or must be designed with no increase the base flood elevation.

**Arterial and Collector Roadways:** Cross culverts should be designed for a 25-year flood event with headwater six inches below the edge of the traveled way. A 100-year event should be used if the drainage is defined as a Major Waterway.

Drainage along the roadway, i.e. gutter flow, should be designed for a 25-year event with flow contained within the shoulder or parking lane. Roadside ditches should be designed for a 25-year flood event with six inches of freeboard. The 100-year event should be contained within the roadway.

**Local Roadways:** Cross culverts must be designed for a 10-year flood event with headwater six inches below the edge of the traveled way. Secondary and Major Waterways should be designed for the corresponding recurrence interval.

Drainage along the roadway, i.e. gutter flow, should be designed for a 10-year event with flow contained within the shoulder or parking lane. Roadside ditches should be designed for a 10-year flood event with six inches of freeboard. The 100-year event should be contained within the roadway.

In the event of sheet flooding occurring in the area of a bridge or culvert, exceptions to the above standards will be considered on a case-by-case basis.

## HYDROLOGIC DESIGN

Estimation of flood flows from minor waterways and for drainage areas that have significant areas of urban development should be through use of the Rational Formula. Secondary and major waterways should have the flood flows estimated from detailed calculations and/or models. Design shall be based on the assumption that all upstream areas are fully developed, consistent with zoning at the time of project approval.

### Rational Formula

Design discharge for minor waterways and urban areas shall be determined by use of the rational formula:

$$Q = C I A K$$

Where:

Q = design discharge in cubic feet per second, cfs

C = runoff coefficient based on full development

I = rainfall intensity in inches per hour

A = drainage area in acres

K = coefficient of intensity

#### Runoff Coefficient:

The runoff coefficient for undeveloped areas is selected from Table 1. For developed areas, the runoff coefficient is calculated based on the runoff coefficient from Table 1 and the percentage of area that is covered by impermeable surfaces. Table 2 provides some typical ranges for the area covered by impermeable surfaces for different levels of development. Table 3 provides some typical runoff coefficients for different types of development. The runoff coefficient is calculated as follows:

$$C_t = (A_p/A_t)(C_p) + (A_v/A_t)(C_v)$$

Where:

$A_p$  = area covered by impermeable surfaces, such as paving and buildings

$A_v$  = area planted or vegetated

$A_t$  = total area

$C_p$  = coefficient of runoff of paved area, usually 0.95

$C_v$  = coefficient of runoff for planted or vegetated areas, from Table 1

$C_t$  = coefficient adjusted for vegetated area

#### Rainfall Intensity:

Rainfall Duration-Intensity Curves are included in Figure 1. Proper determination of the time of concentration has the greatest effect on the rainfall intensity. The time of concentration is the time required for water from the most remote point of the drainage area to travel to the point of interest. Because the flow velocity is dependent on the characteristics of the flow route, the route should be divided into segments where the route characteristics change (i.e. roughness, slope, wetted perimeter, channel slope, etc.) and the individual times added together to get the time of concentration. Figure 2 provides a relationship of slope, cover type and overland flow velocity. The flow velocities for natural channels can be estimated using Manning's equation. Because the depth of flow increases with higher intensity rainfall, the time of concentration will decrease as the storm intensity increases. Add 10 minutes to the calculated time of travel to obtain the time of concentration for the design rainfall intensity.

K: The "K" factor is determined by obtaining the mean annual precipitation for the drainage basin from Figure 3, and dividing it by 35.

#### General:

The Rational Method is based on the following assumptions:

1. All areas of the drainage basin contribute to the peak flow.
2. Rainfall falls at a uniform rate over the entire drainage basin.
3. The runoff coefficient is the same for storms of various frequencies.
4. The runoff coefficient is the same for all storms in a given watershed.
5. The frequency of peak discharge is the same as that of the rainfall intensity for the given time of concentration.
6. The base flow is negligible compared to the flood flow.

Because of these assumptions, use of the Rational Formula should be limited to small, simple watersheds. Diverse watersheds should be divided into homogenous subareas and the resultant flows accumulated based on the entire watershed's time of concentration. If a large amount of storage exists within the basin, development of a hydrograph and flood routing may be required.

**Table 1: Runoff Coefficients For Undeveloped Areas**

	Watershed Types			
	Extreme	High	Normal	Low
Relief	0.28-0.35 Steep Rugged terrain with average slopes above 30%	0.20-0.28 Hilly, with average slopes of 10 to 30%	0.14-0.20 Rolling with average slopes of 5 to 10%	0.08-0.14 Relatively flat land, with average slopes of 0 to 5%
Soil infiltration	0.12-0.16 No effective soil cover, either rock or thin soil mantle of negligible infiltration capacity	0.08-0.12 Slow to take up water, clay or shallow loam soils of low soil infiltration capacity, imperfectly or poorly drained	0.06-0.08 Normal, well drained light or medium textured soils, sandy loams, silt and silt loams	0.04-0.06 High, deep sand or other soil that takes up water readily, very light well drained soils
Vegetal Cover	0.12-0.16 No effective plant cover, bare or very sparse cover	0.08-0.12 Poor to fair; clean cultivation crops, or poor natural cover, less than 20% of drainage area over good cover	0.06-0.08 Fair to good; about 50% of area in good grassland or woodland, not more than 50% of area in cultivated crops	0.04-0.06 Good to excellent; about 90% of drainage area in good grassland, woodland or equivalent cover
Surface Storage	0.10-0.12 Negligible surface storage, depressions few and shallow; drainageways steep and small, no marshes	0.08-0.10 Low; well defined system of small drainageways; no ponds or marshes	0.06-0.08 Normal; considerable surface depression storage; lakes and pond marshes	0.04-0.06 High; surface storage high; drainage system not sharply defined; large floodplain storage or large number of ponds and marshes
Given: An undeveloped watershed consisting of 1) rolling terrain with average slopes of 5%, 2) clay type soils, 3) good grassland area, and 4) normal surface depressions Find: The runoff coefficient, C, for the above watershed			Solution: Relief      0.14 Soil Infiltration    0.08 Vegetal Cover     0.04 Surface Storage   0.06 C = 0.32	

**Table 2: Typical Ranges of Impermeable Area**

Development Type	Low, %	High, %
Suburban Residential (SR)	5	15
Single-Family Residential (R1)	45	65
Two-Family Residential (R2)	50	70
Multi-Family Residential (R3)	50	75
Commercial	50	100

**Table 3: Typical Runoff Coefficients for Developed Areas**

Type of Drainage Area	Runoff Coefficient	Type of Drainage Area	Runoff Coefficient
Business:		Residential	
Downtown Areas	0.70-0.95	Single Family Areas	0.30-0.50
Neighborhood Areas	0.50-0.70	Multi-units, detached	0.40-0.60
Industrial		Multi-units, attached	0.60-0.75
Light industrial areas	0.50-0.80	Suburban	0.25-0.40
Heavy industrial areas	0.60-0.90	Apartment dwelling areas	0.50-0.70
Parks, cemeteries	0.10-0.25	Playgrounds	0.20-0.40

Example:

Calculate the design flow for a subdivision in Kelseyville which has flow from 35 acres of adjacent, rolling, pasture land (zoned AG) and 15 acres of subdivision (zoned R1). The average slope of the agricultural land is 8 percent. The average slope within the subdivision is 3 percent. The soil is a normal Lake County loam.

Example Drainage Area

Calculate I:

The drainage area is less than 1 square mile, therefore, design for the 10-year event

$T_c = 10 \text{ minutes} + \text{Overland Flow time} + \text{Channel Flow time}$

Overland Flow: Pasture; 500 feet, slope of 10%, good grass cover

From Figure 2, the flow velocity is 0.8 feet per second

$T_{of} = (500/0.8)/60 = 10.4 \text{ minutes}$

Channel Flow: Pasture: 1200 feet of natural channel at 1.5%

Use Manning's equation to estimate velocity

$V = (1.49/0.035)(0.5)^{2/3} \times (0.015)^{1/2}$

$V = 3.3 \text{ fps}$

$T_c = (1200/3.3)/60 = 6.1 \text{ minutes}$

Subdivision: 800 feet of culvert at 1.25 %

$$V = (1.49/0.013)(0.5)^{2/3} \times (.0125)^{1/2}$$

$$V = 8 \text{ fps}$$

$$T_c = (800/8)/60 = 1.7 \text{ minutes}$$

Design Time of Concentration

$$T_c = 10 + 10.4 + 6.1 + 1.7 = 28.2 \text{ minutes, Use 30 minutes}$$

Using Figure 1 for the 10-year event, the rainfall intensity is 0.96 inches/hour

Determine K

Using Figure 3, the average annual precipitation for Kelseyville is 26 inches/year

$$K = 26/35 = 0.74$$

$$Q = (0.47)(0.96)(50)(0.74) = 16.7 \text{ cfs}$$

Design Drainage Facilities for 17 cfs

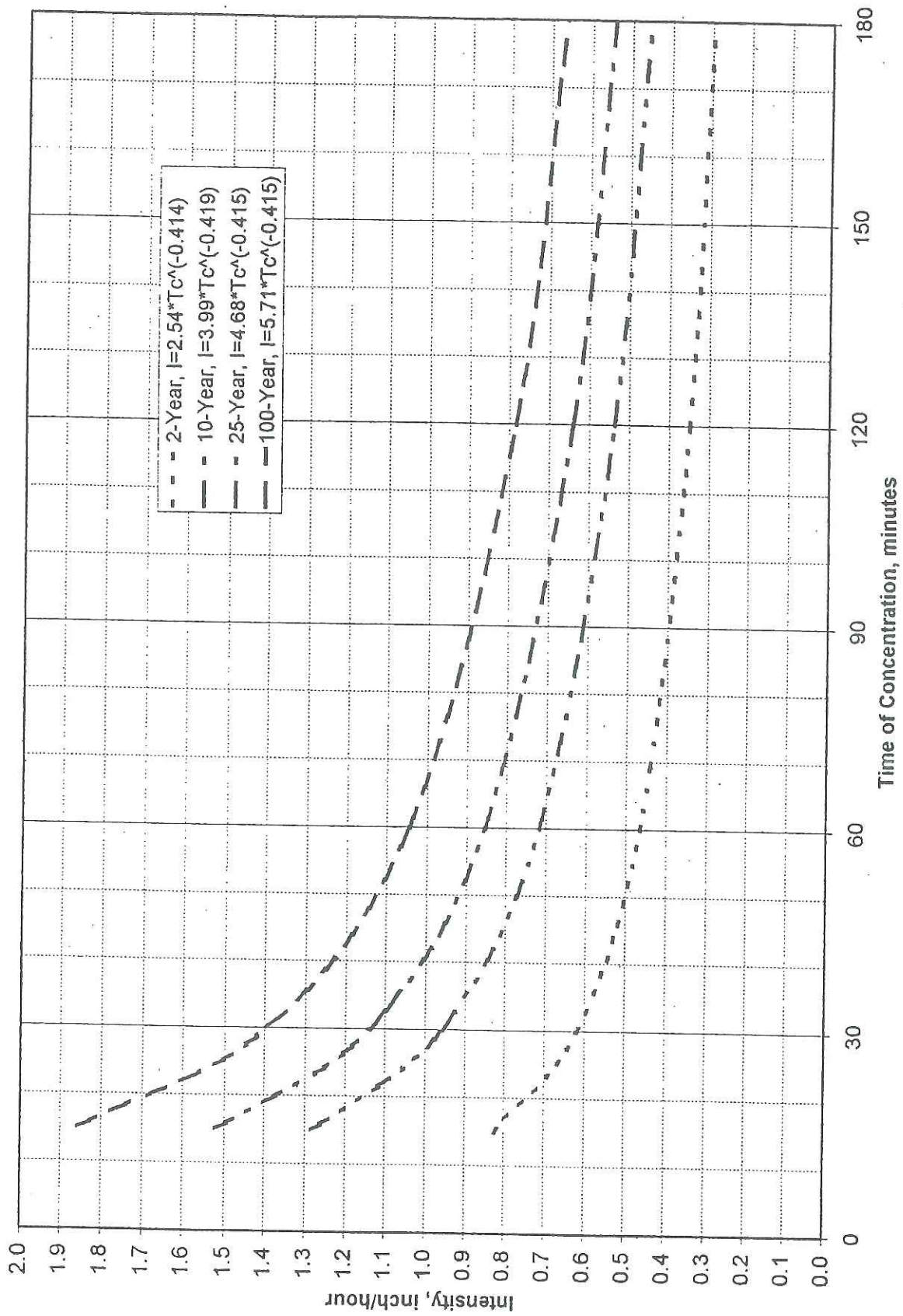


Figure 1: Rainfall Duration-Intensity Curves

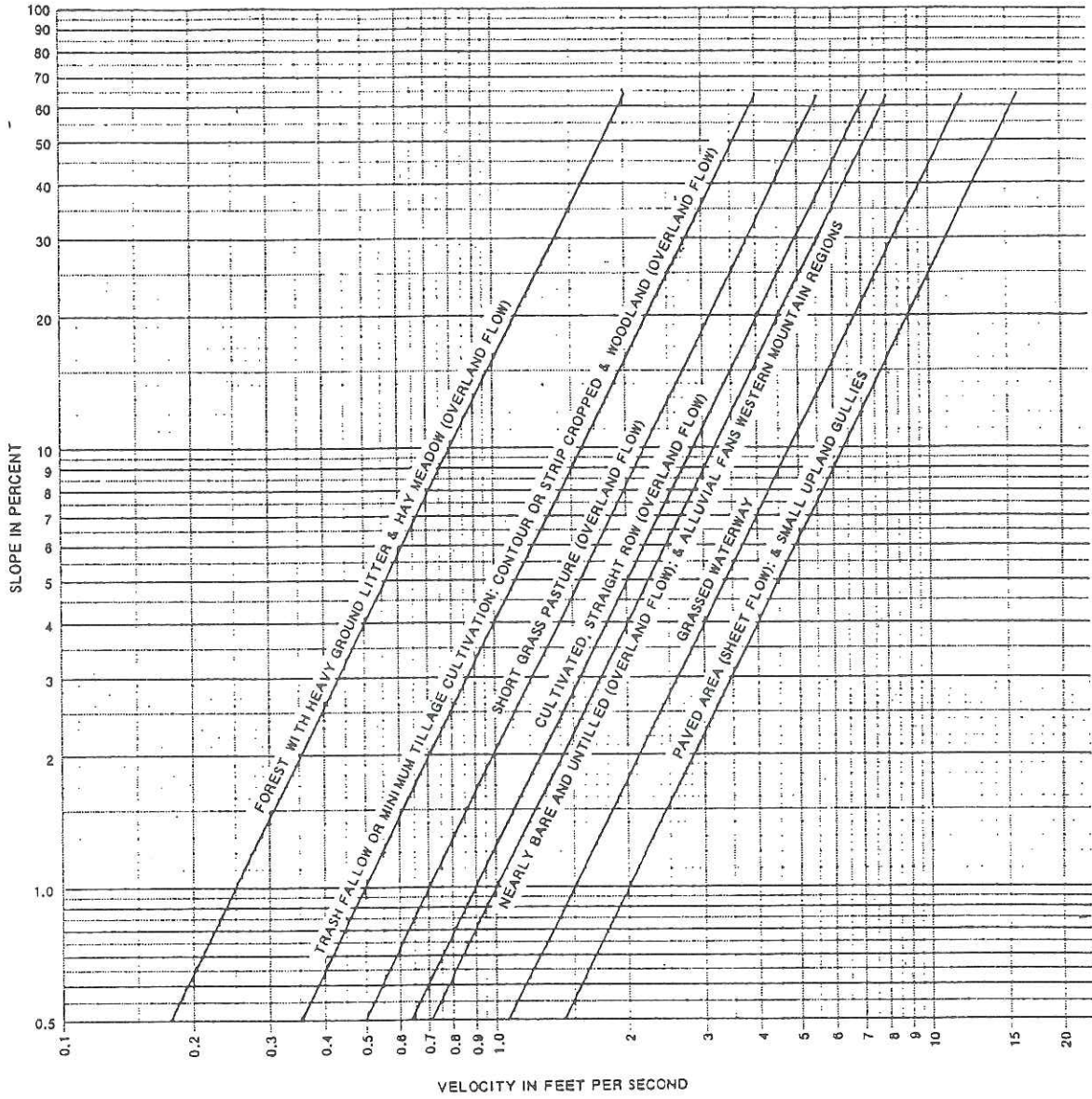


Figure 2: Overland Flow Velocities

From: USDA Soil Conservation Service, National Engineering Handbook, Section 4, Hydrology, March 1985, p. 15-8



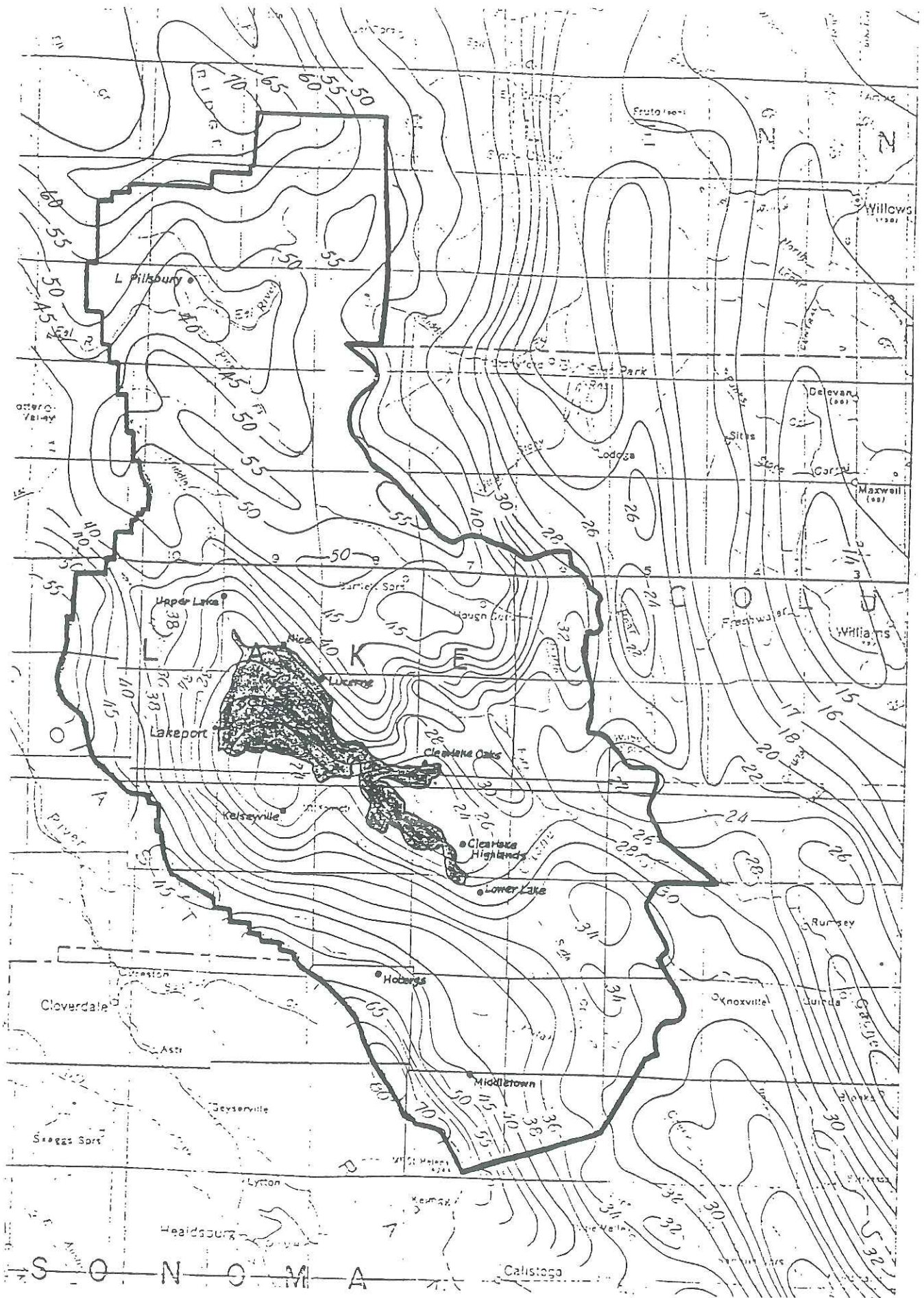


Figure 3: Average Annual Precipitation for Lake County

From: Calif. Department of Water Resources, Lines of Average Yearly Precipitation in the Central Valley, April 1966

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